

Modeling plastics in LS-DYNA

Part 1 - isotropic Modeling of Thermoplastics

Part 2 - anisotropic Modeling of Fiber-reinforced Thermoplastics

P. Reithofer, B. Hirschmann, H. Pothukuchi, St. Riemelmoser (4a engineering GmbH),

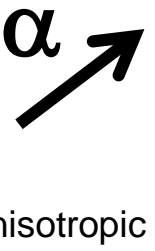
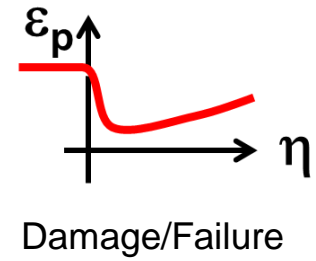
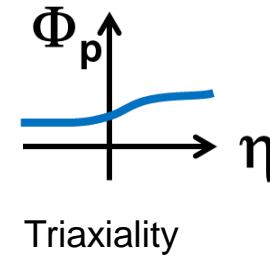
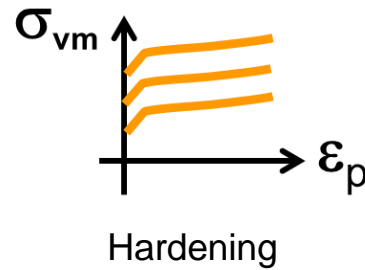
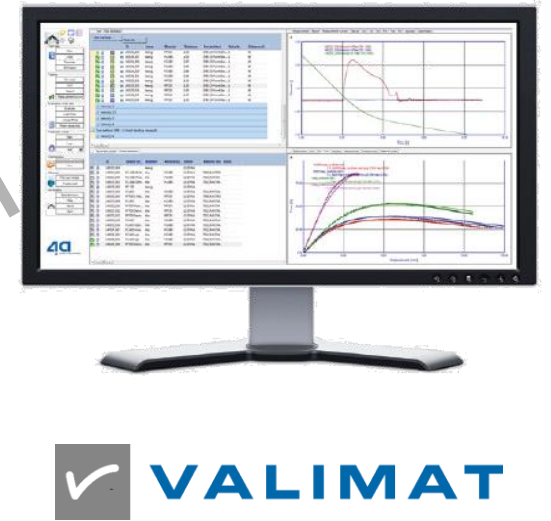
contact: peter.reithofer@4a.at

***DYNAMore Express** 19th & 26th June 2020*

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Outline

- [Introduction](#)
- [Thermoplastic materials](#)
- [Summary Part 1: Isotropic](#)
- [SFRT & LFRT](#)
[short and long fiber reinforced thermoplastics](#)
- [Composites](#)
- [Summary Part 2: Anisotropic](#)
- [Appendix – IMPETUS® & VALIMAT® details](#)

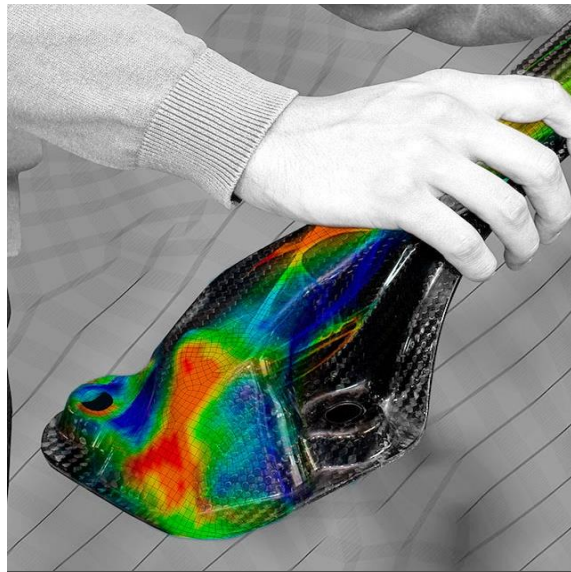


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excellence in
plastics&simulation
testing equipment
lightweight products



4a business units



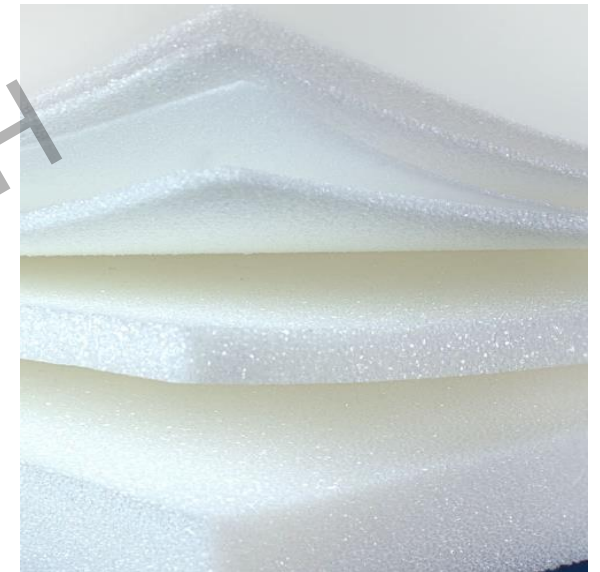
4a engineering
Engineering and simulation for plastic products and composites



Impetus
Testing equipment generating material data for the dynamic simulation of plastics



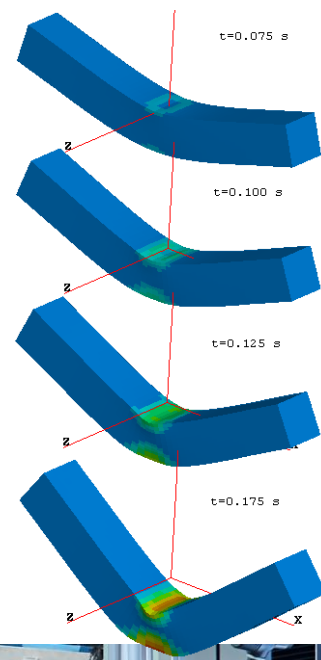
4activeSystems
Dummies and testing facilities for active vehicle safety



4a manufacturing
Specialized thin foams and multi layer materials

Material characterization - services

- efficient high-dynamic testing
- dynamic material behaviour
- plastics, foams, composites, ...
- **validated material cards ready to use for your crash-simulation**



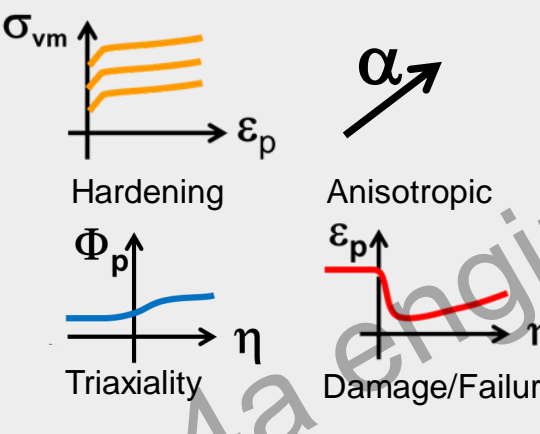
Intelligent reliable solutions for plastics, composites, metals, foams, ...

IMPETUS



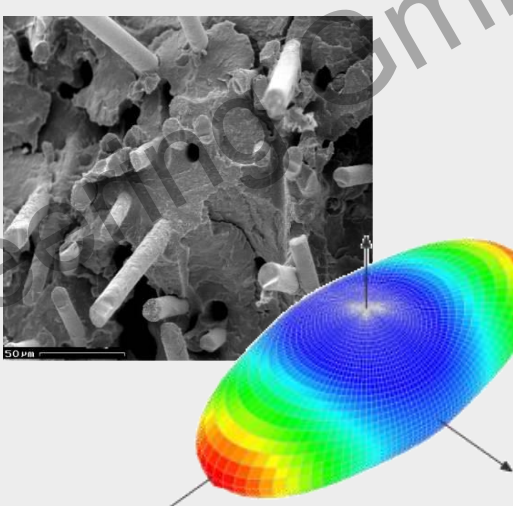
efficient dynamic testing

VALIMAT



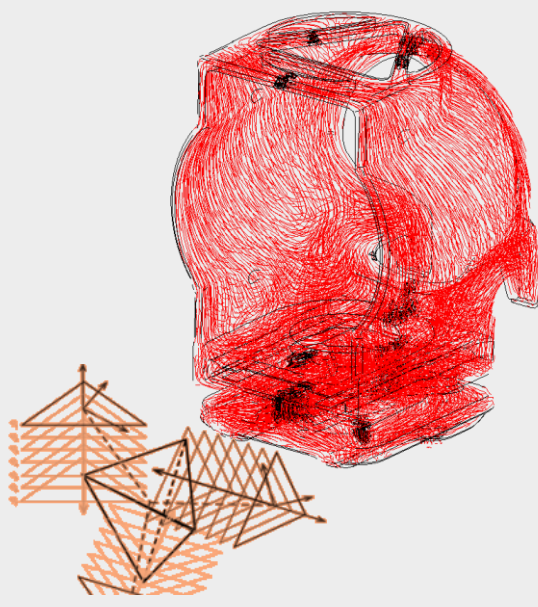
from test to validated material cards

MICROMECH



3D anisotropic material cards

FIBERMAP



individual mapping process information



4a summer-school - webinar and training
Material characterization with
VALIMAT® and IMPETUS®

SAVE THE DATE

The webinars will be completely free of charge and
will be held from 9 - 11 a.m. CET

<https://www.4a-engineering.at/news>

1st week - Introduction and outlook

- 07. July** - Introduction to VALIMAT®
from test to material card
- 08. July** - Efficient dynamic testing with IMPETUS®
- 09. July** - Material card generation: vonMises plasticity
(*MAT_024), simple failure, setting up our
Autofit
- 10. July** - Summary: Lessons learned, outlook and
upcoming feature

2nd week - Advanced topics

- 14. July** - Evaluating and checking test data -
interpretation of typical results
- 15. July** - Material card generation: general yield surface
(*MAT_187) and other material models, failure
approaches and comprehensive Autofit setup
- 16. July** - Material card generation: Fiber reinforced
plastics and their modelling approach: an
extensive guide
- 17. July** - Python: a powerful tool with VALIMAT®, user
defined material cards/specimen,

Intelligent reliable solutions for plastics, composites, metals, foams, ...

◀ **IMPETUS**

✓ **VALIMAT**

◉ **MICROMECH**

➔ **FIBERMAP**

Foams

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

Metals

efficient
dynamic testing

from test to validated
material cards

3D anisotropic
material cards

individual mapping
process information

Intelligent reliable solutions for plastics, composites, metals, foams, ...

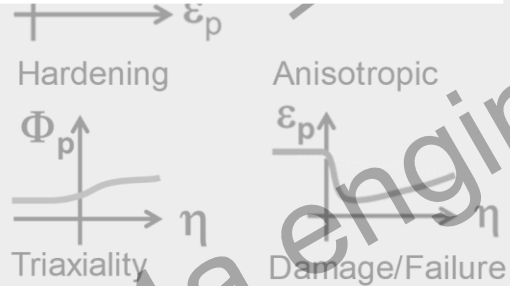
IMPETUS

Thermoplastics



efficient
dynamic testing

VALIMAT



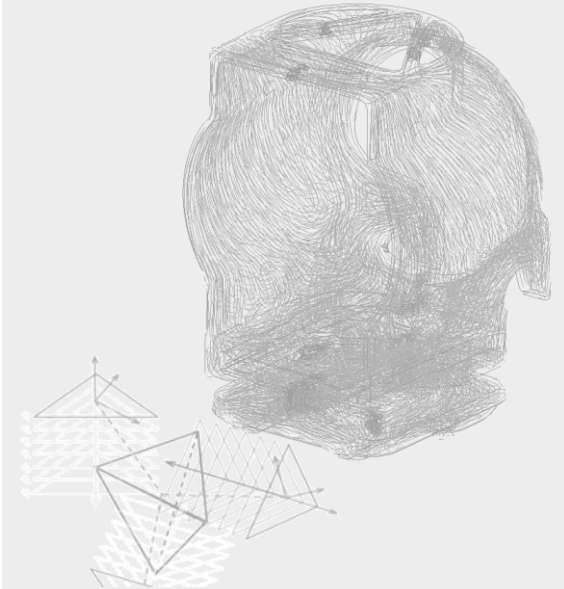
from test to validated
material cards

MICROMECH



3D anisotropic
material cards

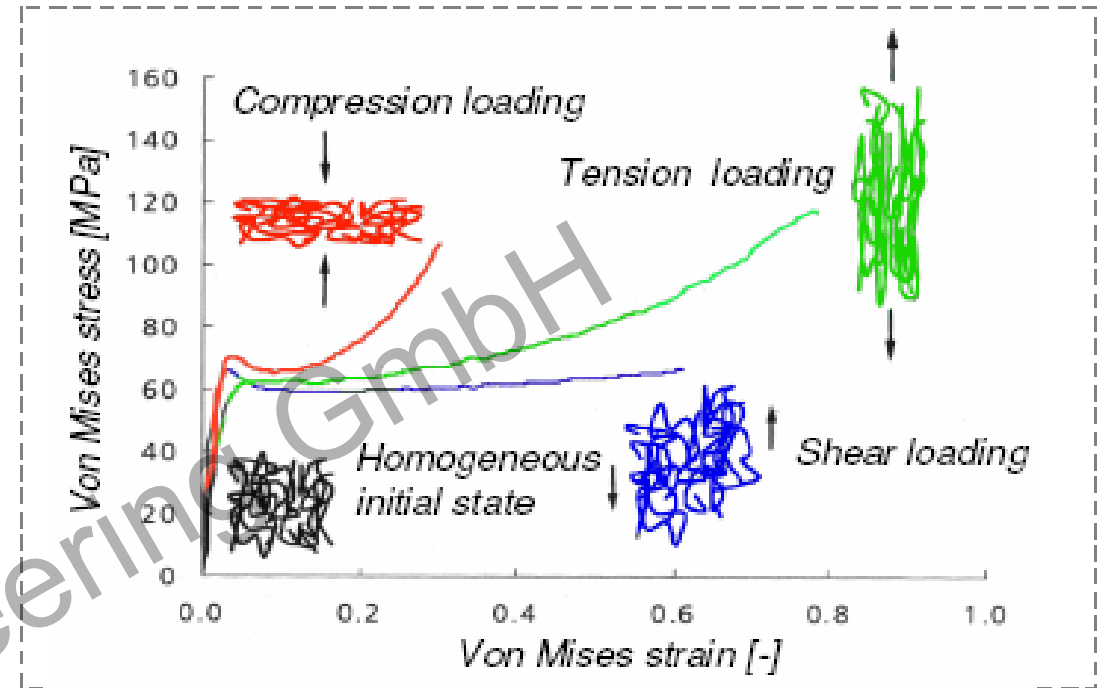
FIBERMAP



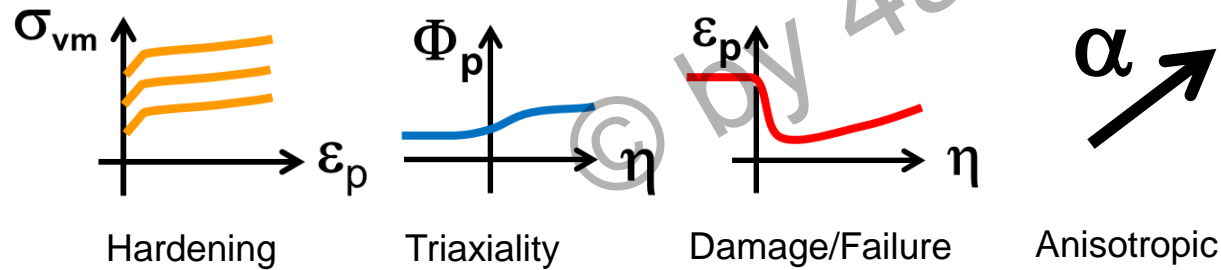
individual mapping
process information

Thermoplastic materials

- Motivation
- Material behavior
- Material characterization
 - IMPETUS™ - dynamic impact tensile testing
 - typical test results PP T10
- Material and failure models
- First validation results

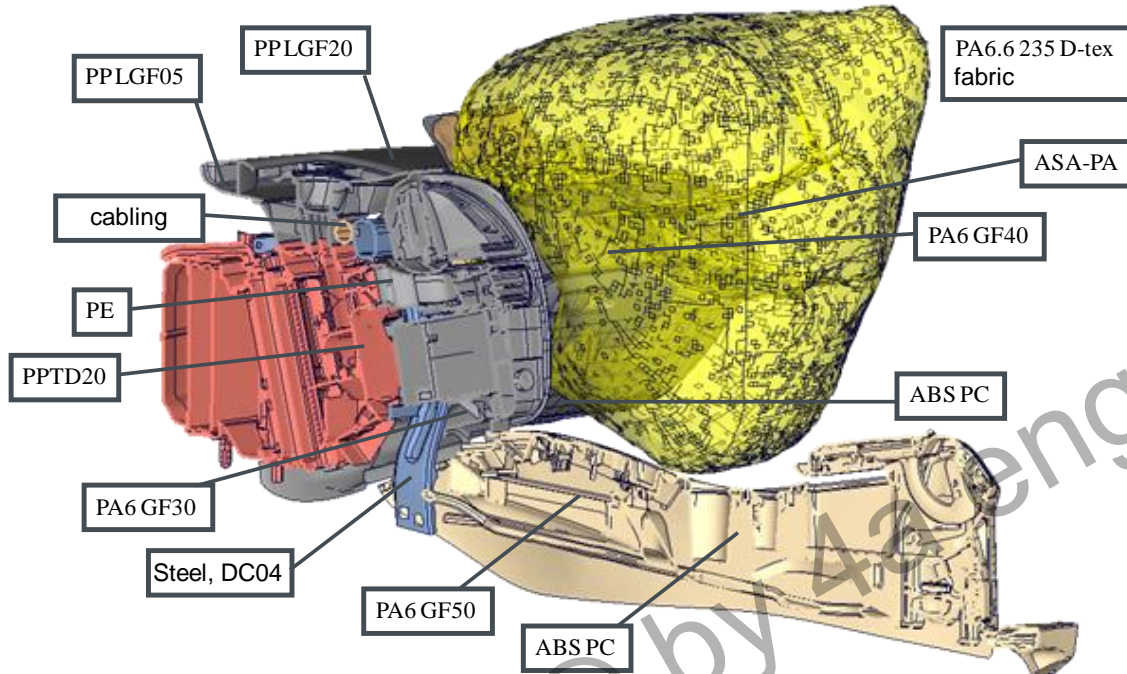


Source: Mechanik der Kunststoffe W. Retting, Hanser Verlag 1991



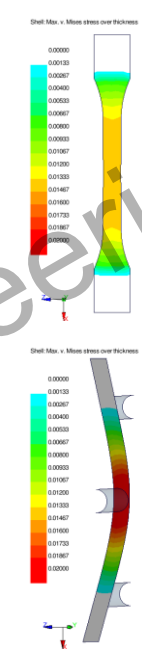
Motivation

material variety



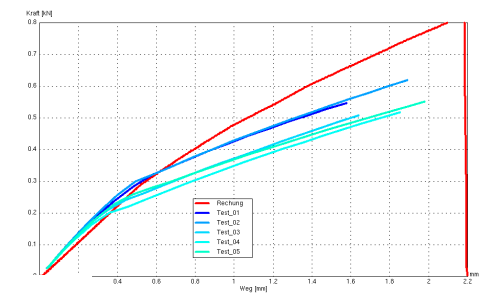
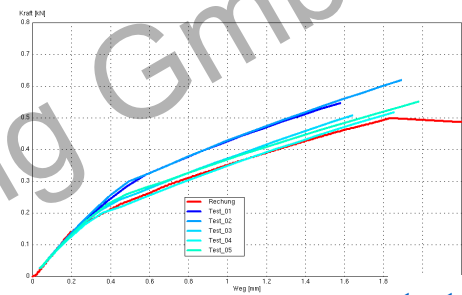
Source: R. Luijckx - *Kunststoffmaterialien in der Interieur Funktionsauslegung bei Audi AG*, 4a Technologietag 2010

bending load case

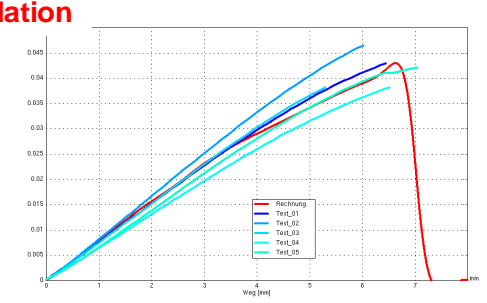
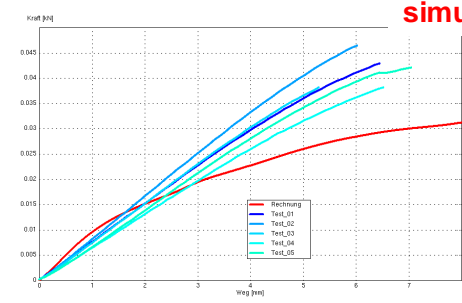


original test curve tension

scaling 1.25

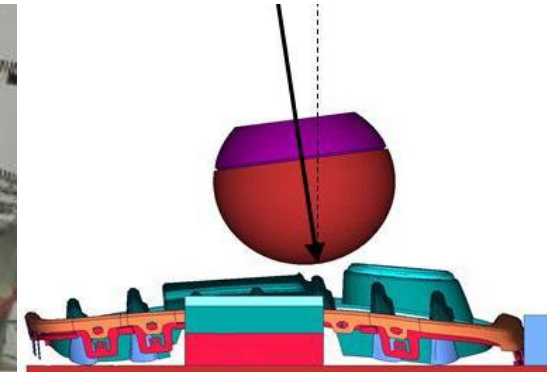
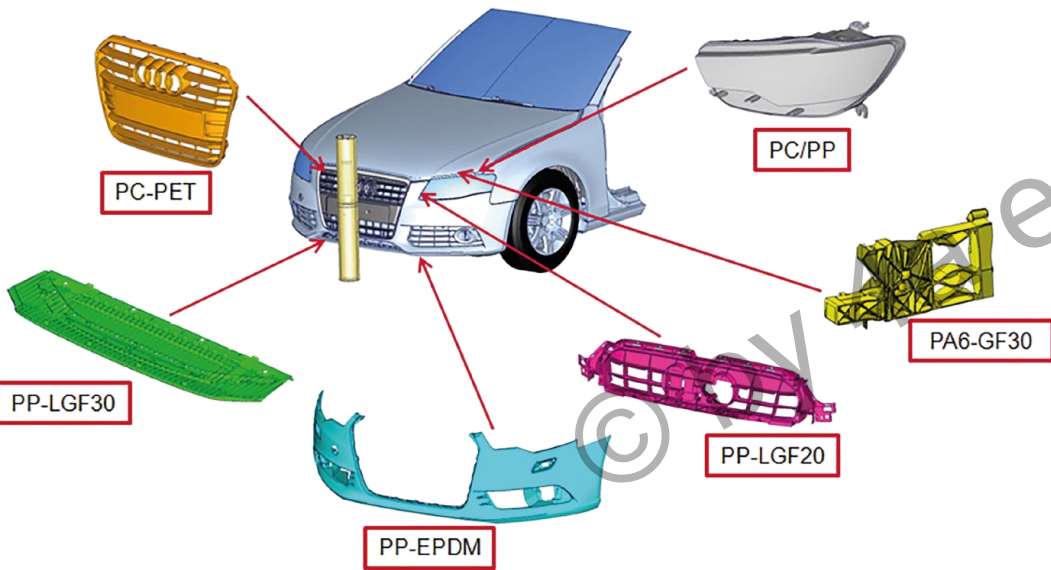
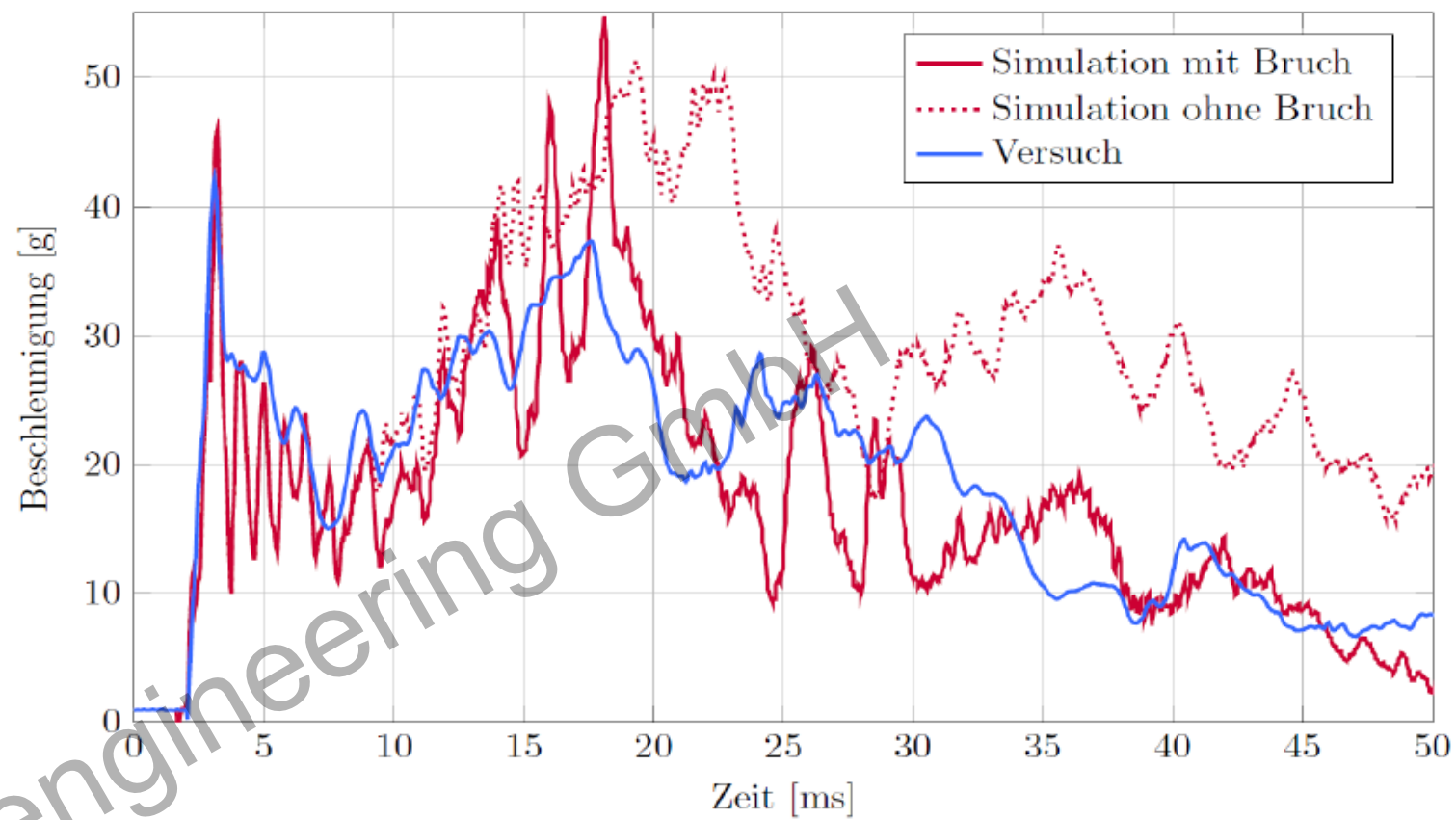
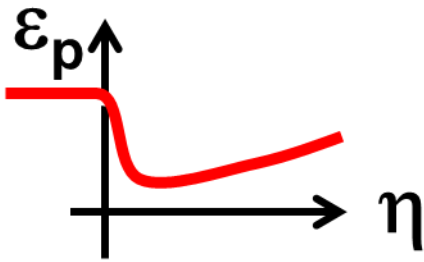


test simulation



Motivation

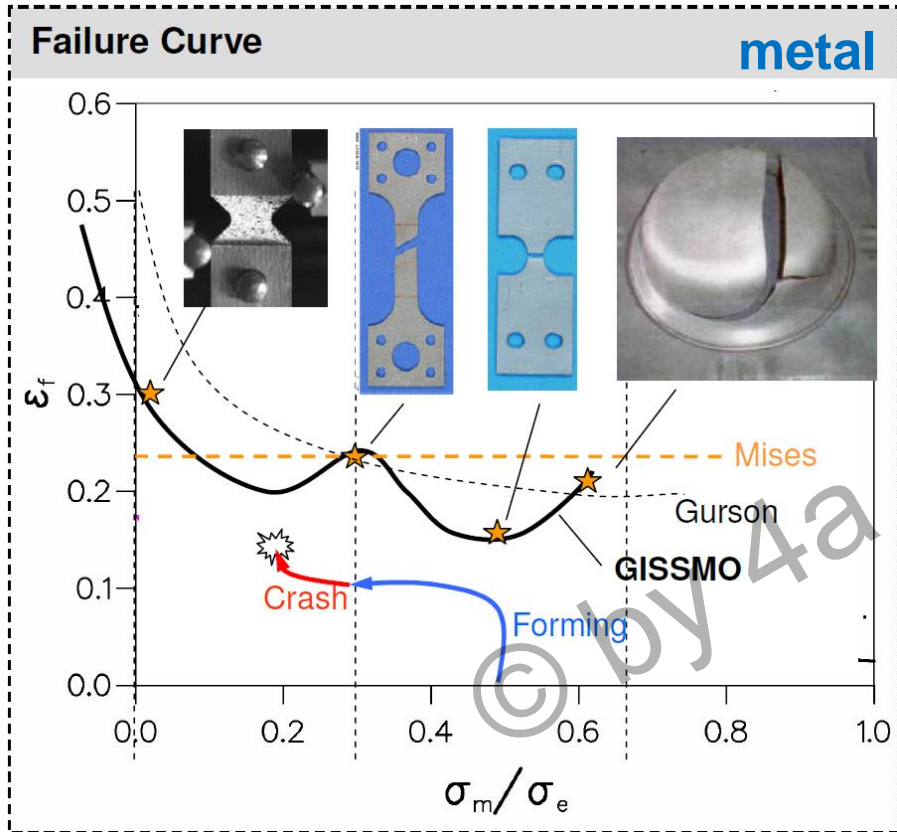
Damage/Failure



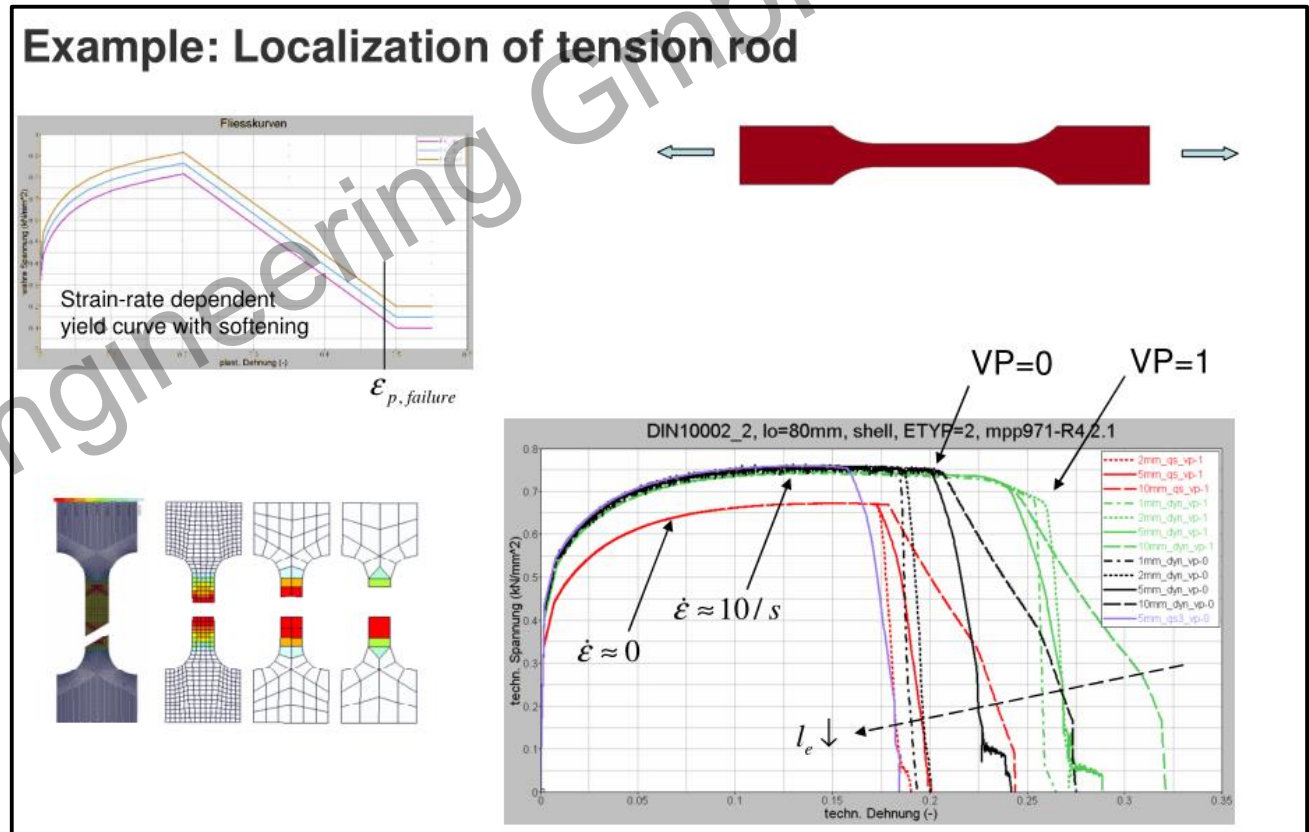
Source: H. Staack, Audi AG: Anforderungsgerechte Material- und Bruchmodellierung für die Fahrzeugsicherheit, TT16 Schladming

Motivation

- typical customers request for plastics
 → **GISSMO with *MAT_024**



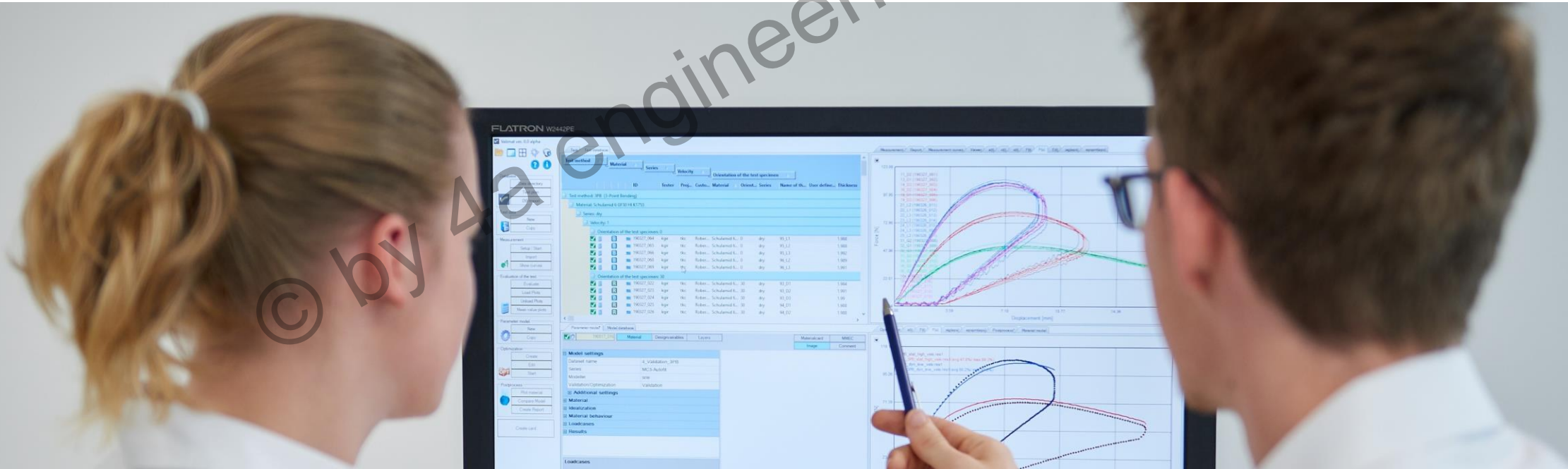
source: F. Neukamm – GISSMO – Material modeling with a sophisticated failure criteria, LS-Dyna Developer Forum 2011, Stuttgart



source: Damage and Failure Models in LS-DYNA; M. Feucht; A. Haufe ;(2009)

Available material and failure models!

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Material Model Selection

LS-DYNA has many material models implemented currently 265 materials (01.07.2020)
most of them won't fit in our use case

The most used material model is ***MAT_024**.

Other interesting material models for thermoplastic polymers are ***MAT_124** and ***MAT_187**.

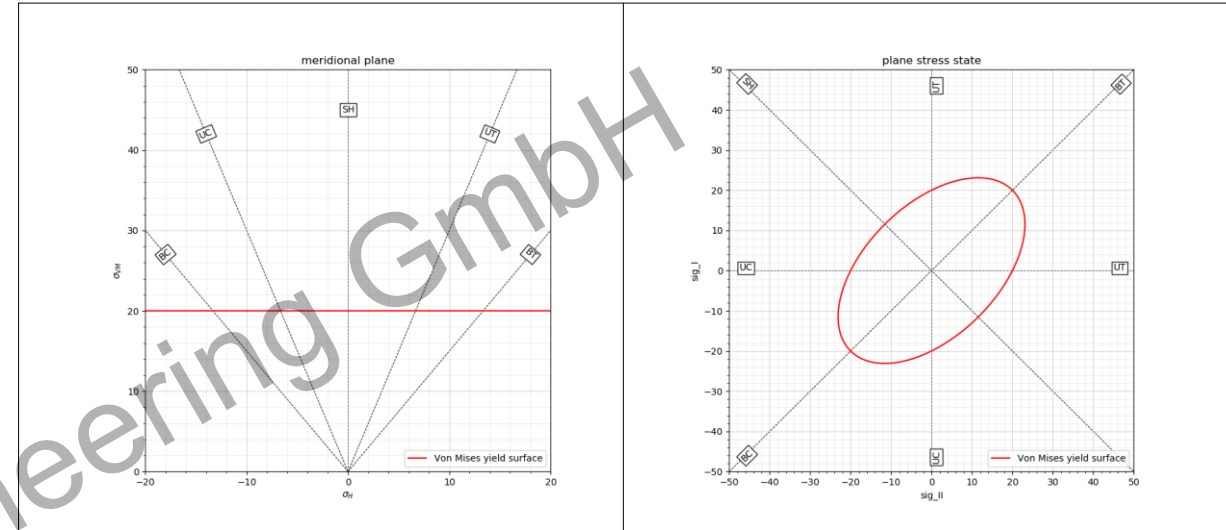
Table: number of available material models for subset of filters
<http://www.lstc.com/dynamat/> (01.7.2020)

Element	Material family	Nr. of material models
Any element	Any family	265
Shell element	Any family	23
Solid element	Any family	179
Any element	Plastics	33
Shell element	Plastics	23
Solid element	Plastics	29

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Commonly Used Material Models For Plastics

- ***MAT_024 - The workhorse**
 (*MAT_081, *MAT_089, *MAT_123, ...)

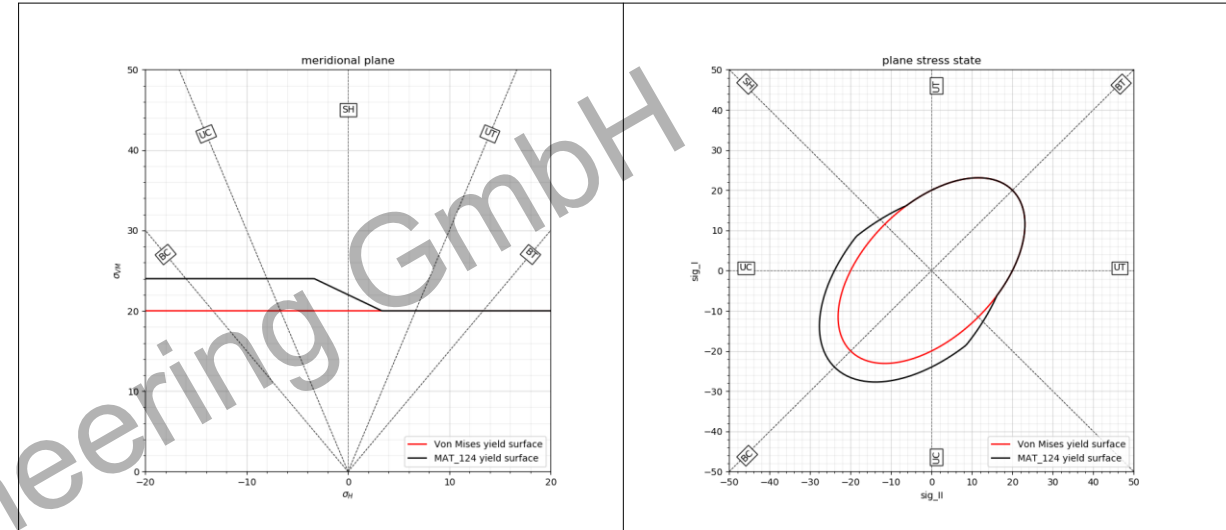


Material model	yield surface	Visco-elasticity	Visco-plasticity	Comp./tension asymmetry	plastic Poisson's ratio
*MAT_024	von Mises	x	✓	x	0.5

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Commonly Used Material Models For Plastics

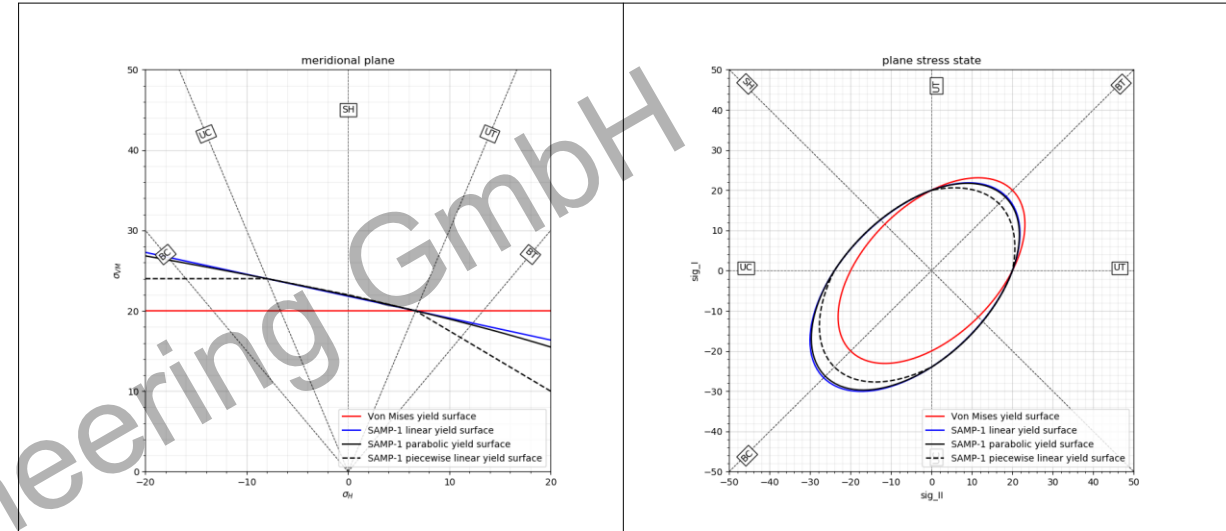
- ***MAT_024 - The workhorse**
(***MAT_081, *MAT_089, *MAT_123, ...**)
- ***MAT_124 - The hidden**



Material model	yield surface	Visco-elasticity	Visco-plasticity	Comp./tension asymmetry	plastic Poisson's ratio
*MAT_024	von Mises	✗	✓	✗	0.5
*MAT_124	2x von Mises	✓ Pronyseries	✓	✓	0.5

Commonly Used Material Models For Plastics

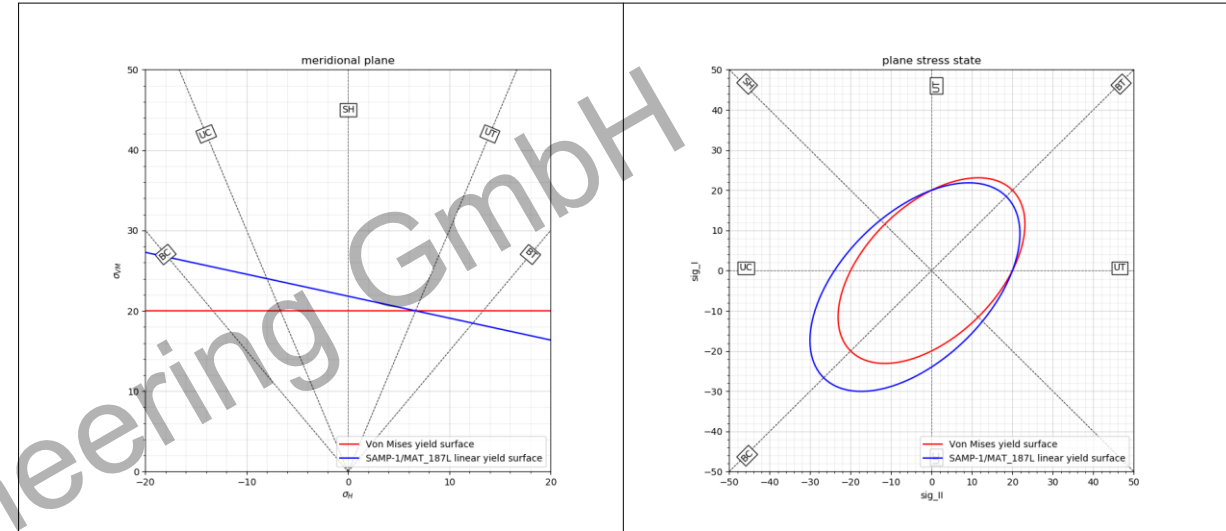
- ***MAT_024 - The workhorse**
(***MAT_081, *MAT_089, *MAT_123, ...**)
- ***MAT_124 - The hidden**
- ***MAT_187 - The plastic expert**



Material model	yield surface	Visco-elasticity	Visco-plasticity	Comp./tension asymmetry	plastic Poisson's ratio
*MAT_024	von Mises	✗	✓	✗	0.5
*MAT_124	2x von Mises	✓ Pronyseries	✓	✓	0.5
*MAT_187	linear; parabolic; piecewise linear	✓ $E(\dot{\epsilon})$	✓	✓	✓ $\nu_p(\epsilon)$

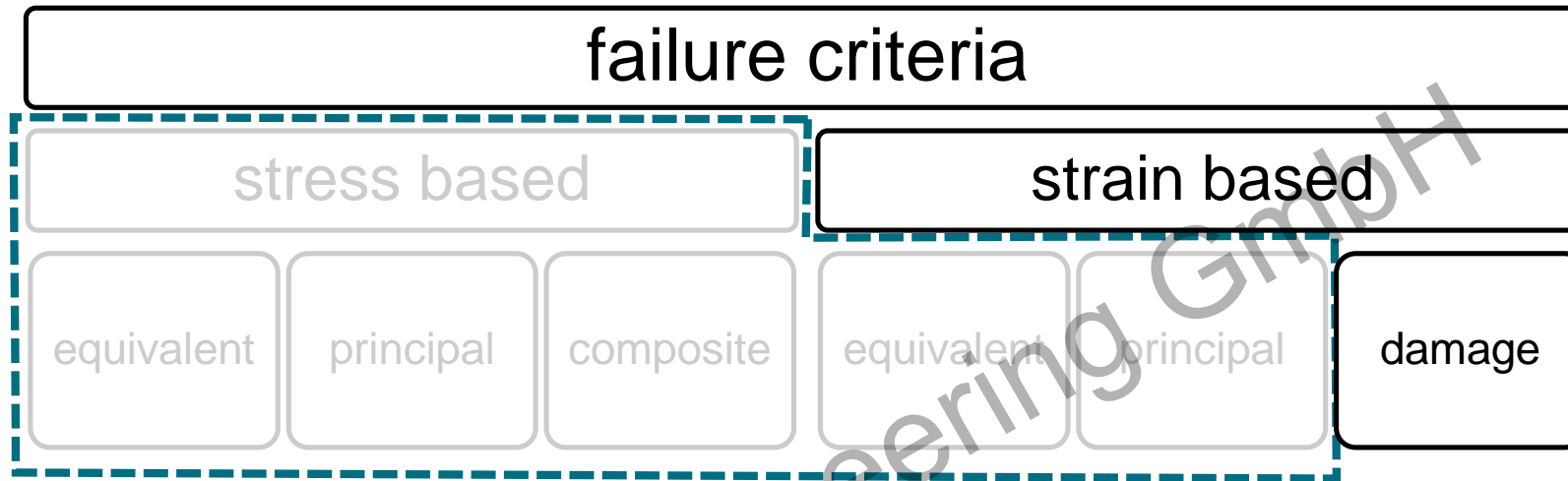
Commonly Used Material Models For Plastics

- ***MAT_024 - The workhorse**
(***MAT_081, *MAT_089, *MAT_123, ...**)
- ***MAT_124 - The hidden**
- ***MAT_187 - The plastic expert**
- ***MAT_187L – efficient version (R12)**



Material model	yield surface	Visco-elasticity	Visco-plasticity	Comp./tension asymmetry	plastic Poisson's ratio
*MAT_024	von Mises	✗	✓	✗	0.5
*MAT_124	2x von Mises	✓ Pronyseries	✓	✓	0.5
*MAT_187	linear; parabolic; piecewise linear	✓ $E(\dot{\epsilon})$	✓	✓	✓ $\nu_p(\epsilon)$
*MAT_187L	linear	✓ $E(\dot{\epsilon})$	✓	✓	✓ $\nu_p(\epsilon)$

Available failure models in LS-DYNA®



additional failure models

***MAT_ADD_EROSION**

strain damage based

- *before R11 optional DIEM / GISSMO*
- *since R11 *MAT_ADD_DAMAGE_DIEM*
- *since R11 *MAT_ADD_DAMAGE_GISSMO*

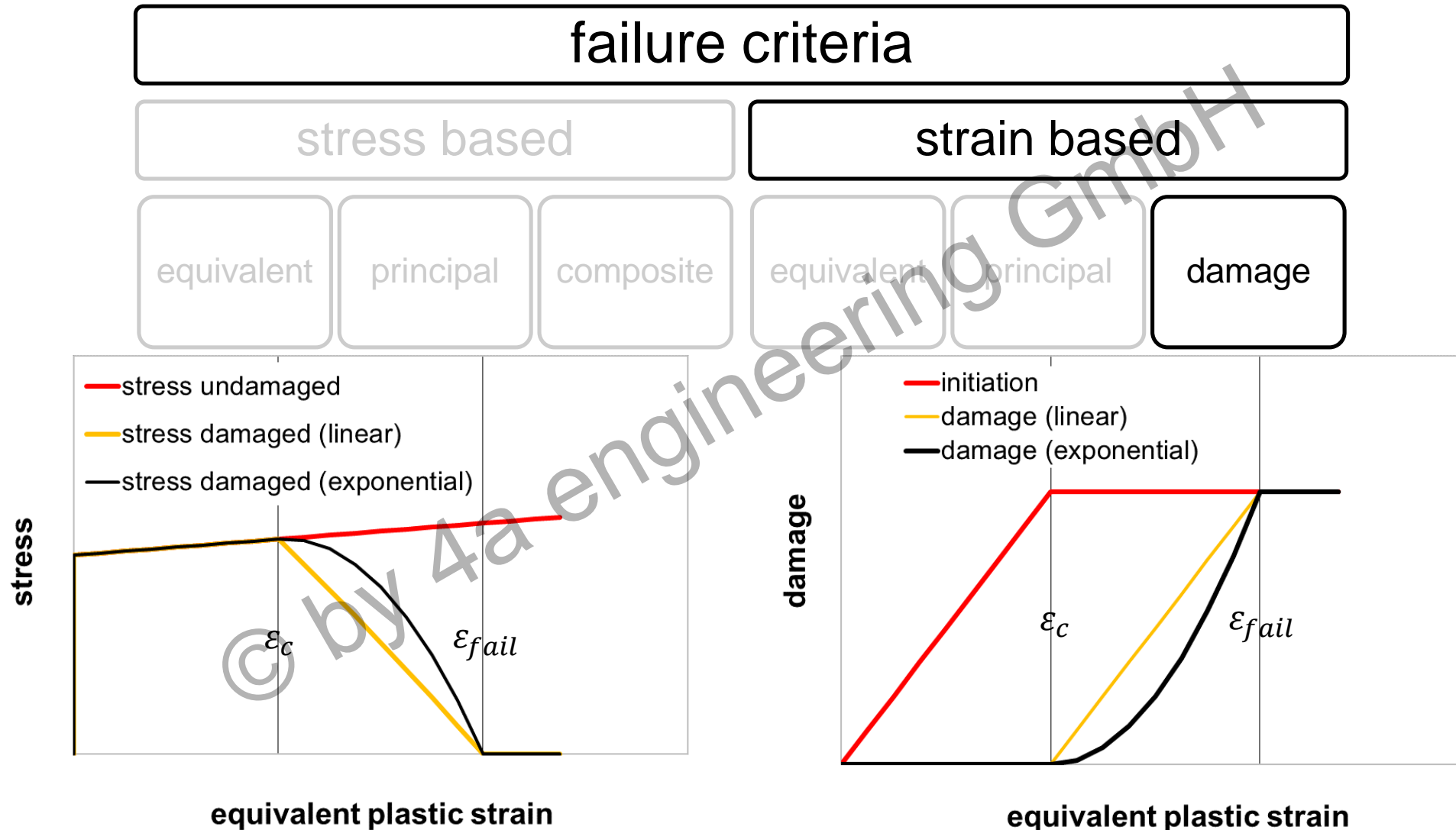
Included eq. pl. strain

***MAT_024**

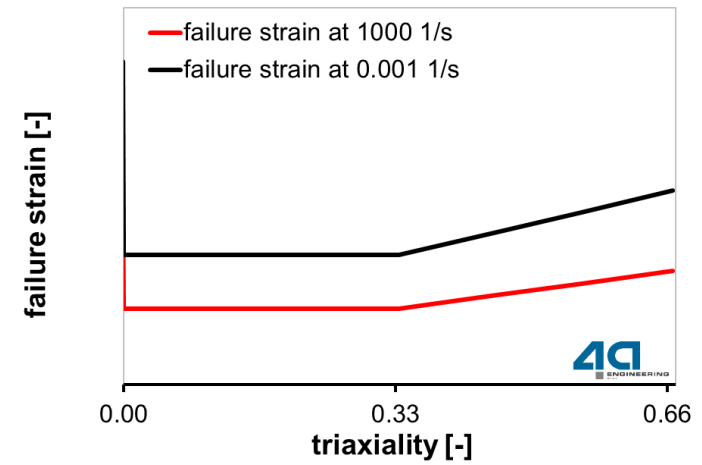
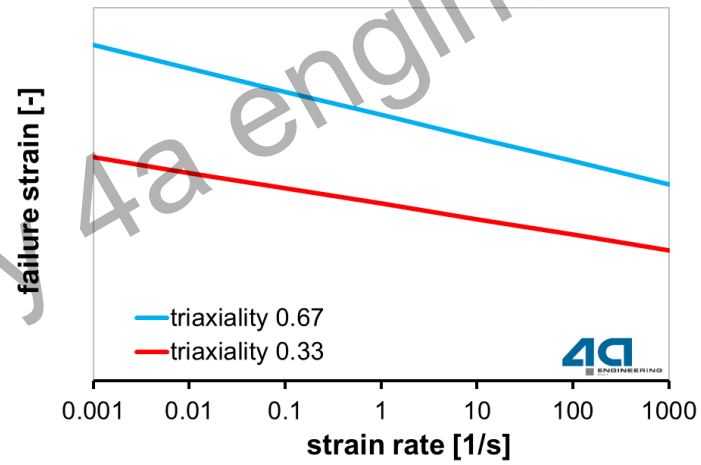
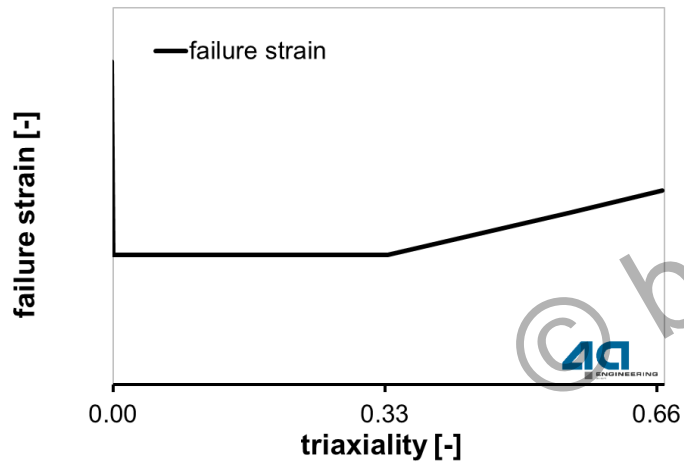
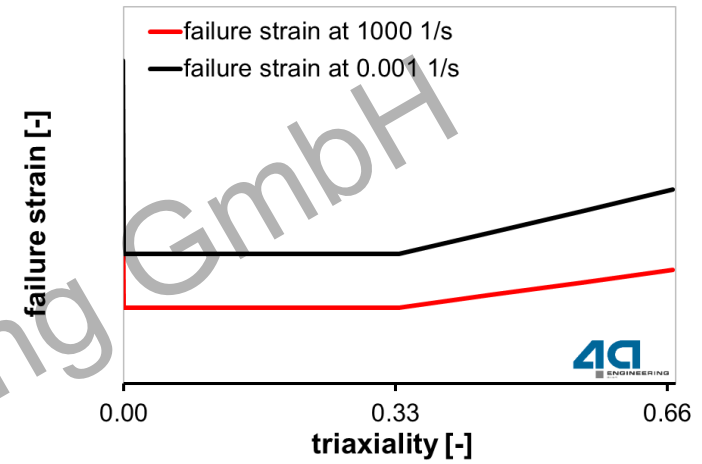
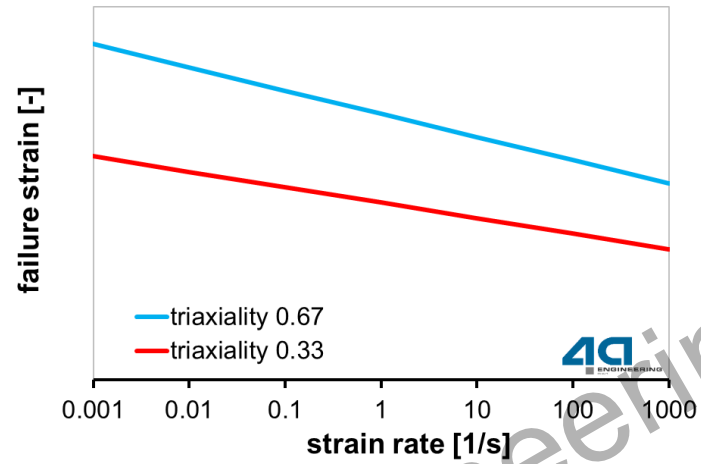
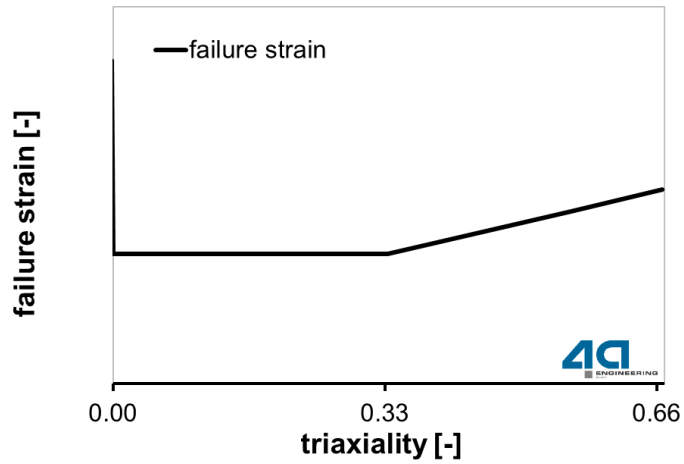
included damage model in

***MAT_SAMP-1(GISSMO like)**

Available failure models – incremental damage formulation



Comparison DIEM-GISSMO visualized

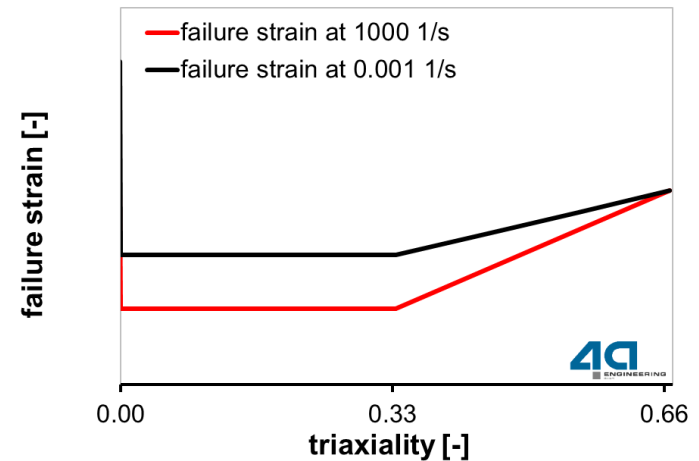
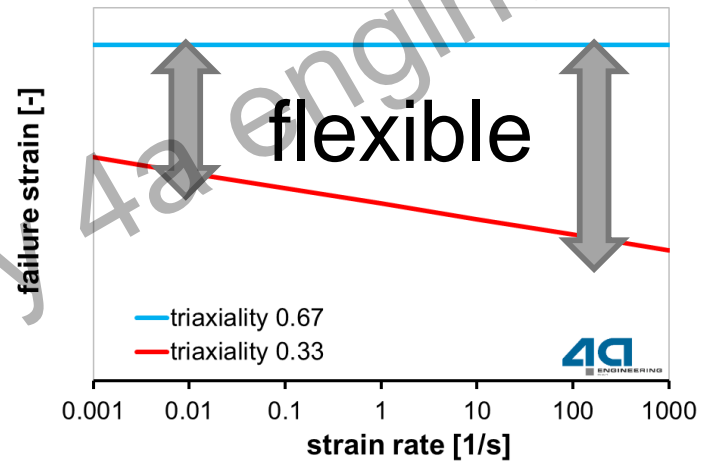
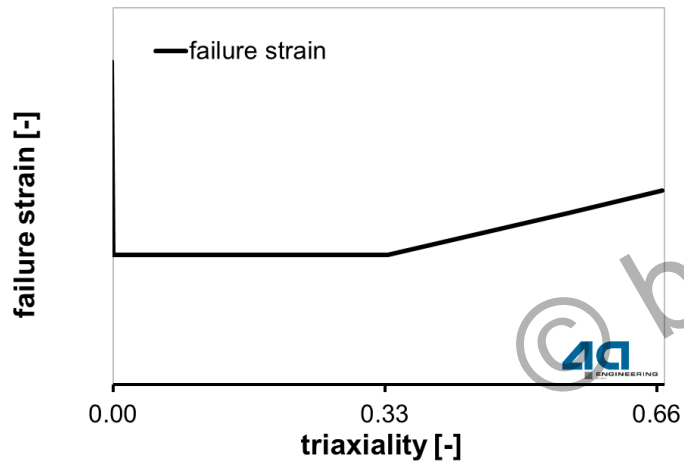
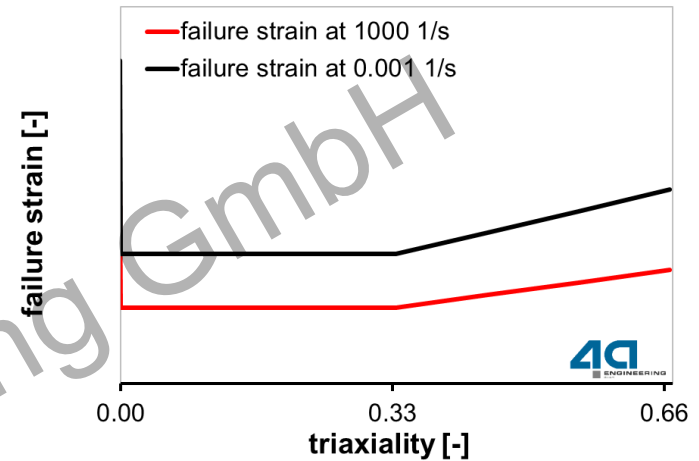
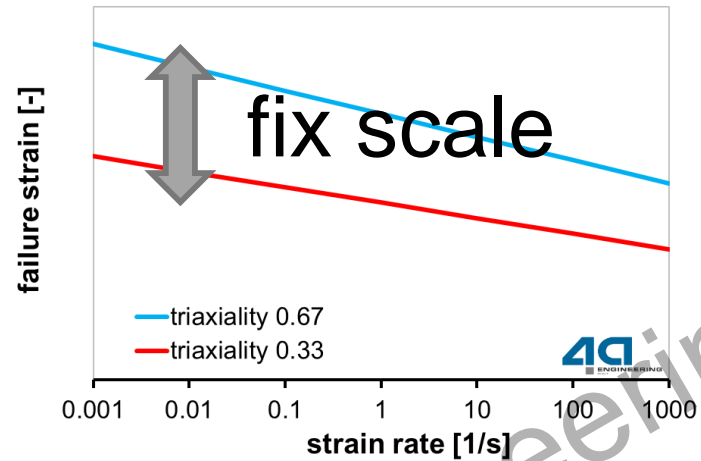
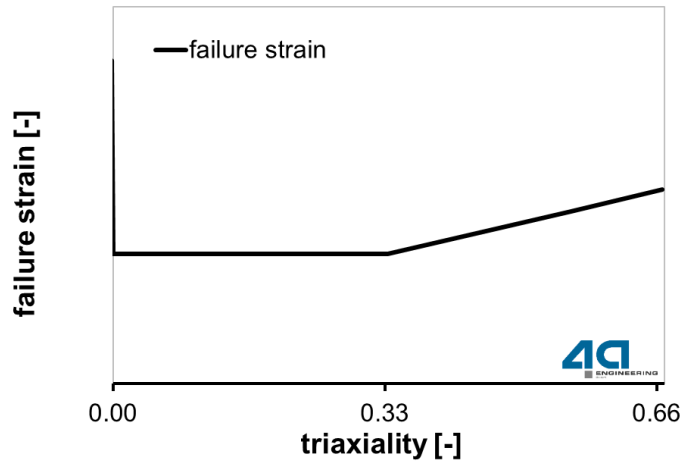


GISSMO

DIEM

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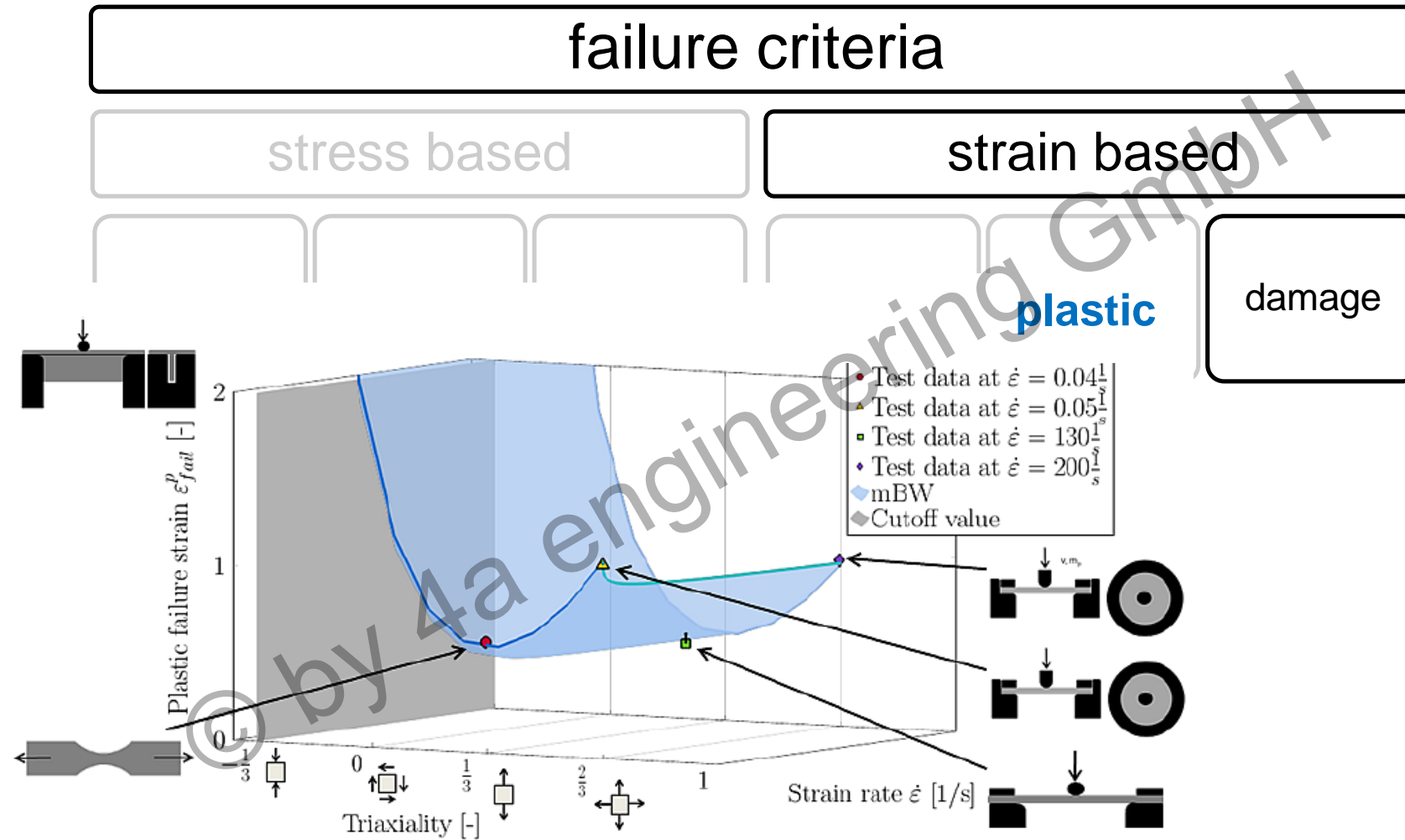
Comparison DIEM-GISSMO visualized



GISSMO

DIEM

Available failure models – typical curves

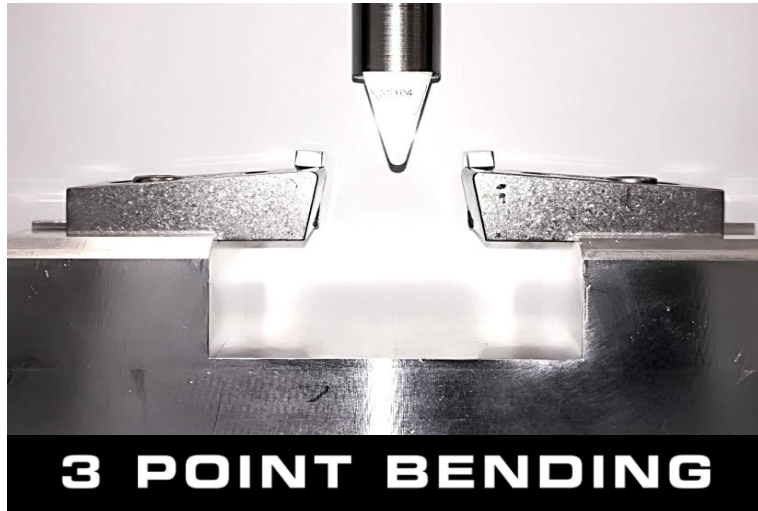


source: H. Staack, - Application oriented failure modeling and characterization for polymers in automotive pedestrian protection, COMPLAS 2015, Barcelona

Let's take a closer look on the plastic!



Static Testing



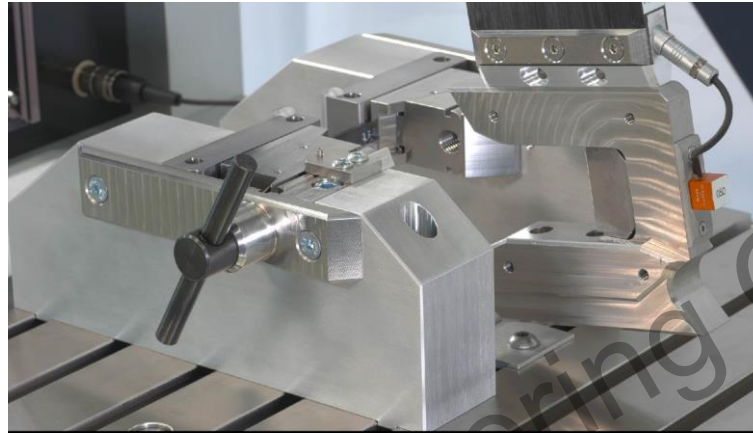
static ~ 1mm/s

© by 4a engineering GmbH

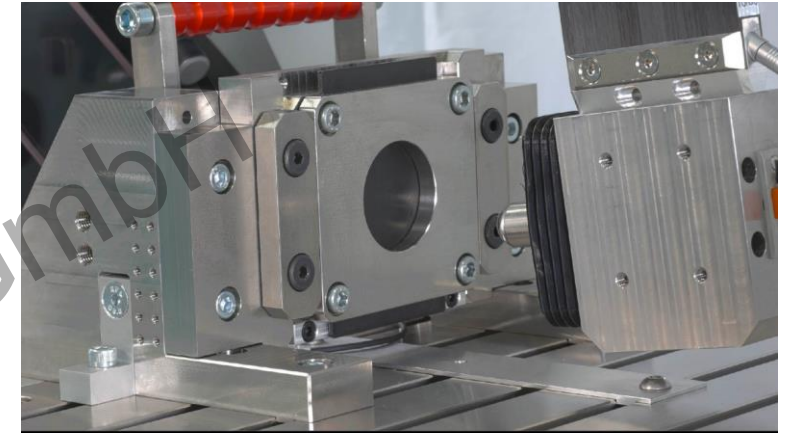
IMPETUS® - efficient dynamic testing



3 POINT BENDING

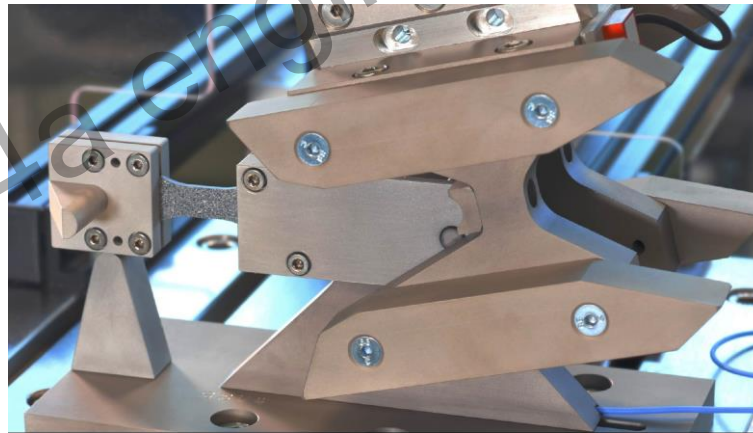


TENSION BENDING



PUNCTURE TEST

IMPETUS® ~ 3 m/s



TENSION TEST

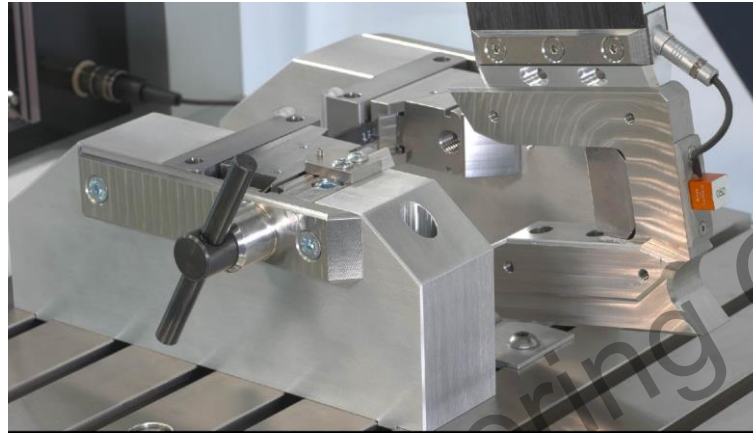


YOUTUBE CHANNEL

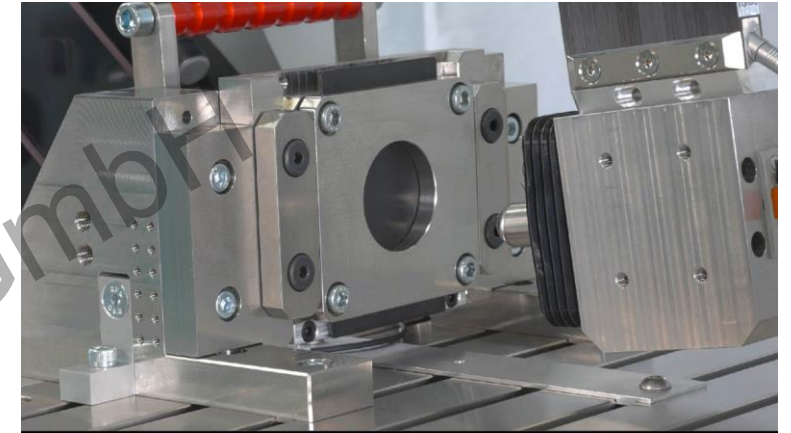
IMPETUS® - efficient dynamic testing



3 POINT BENDING

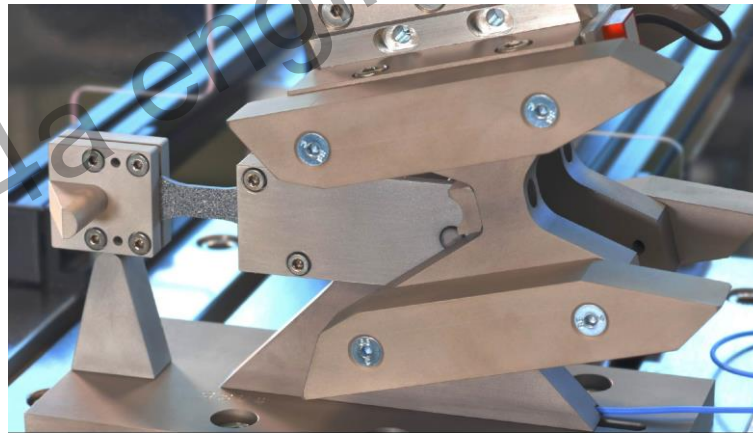


TENSION BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



TENSION TEST

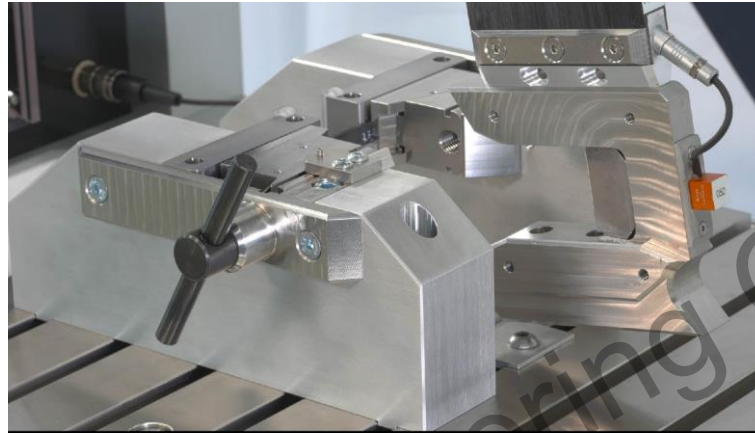


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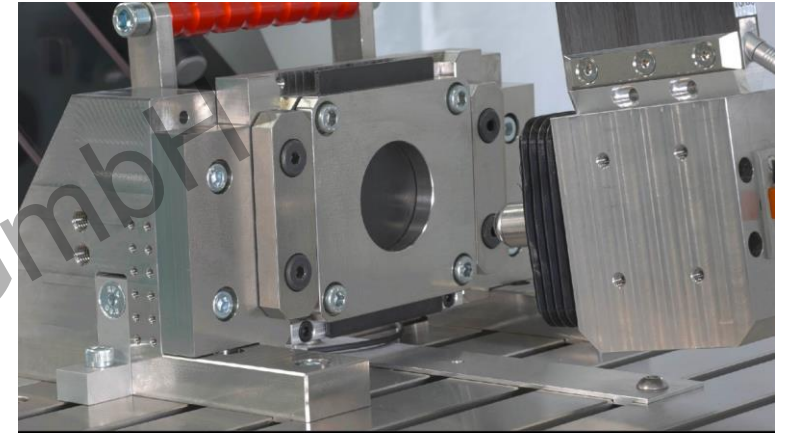
IMPETUS® - efficient dynamic testing



3 POINT BENDING

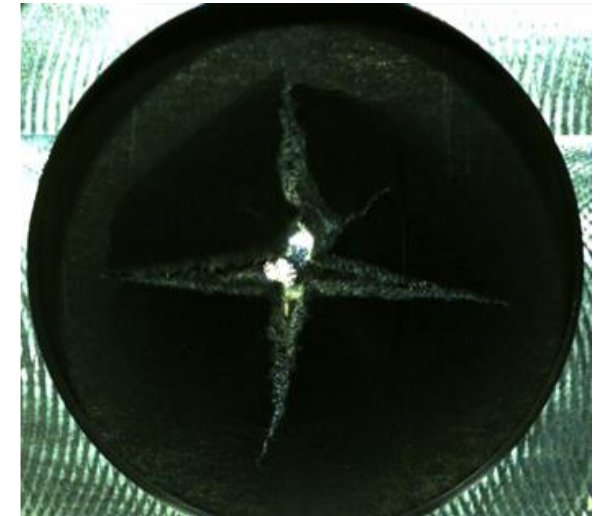
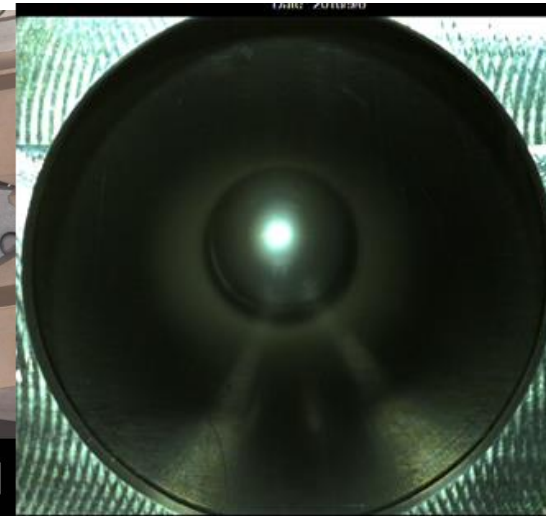


TENSION BENDING

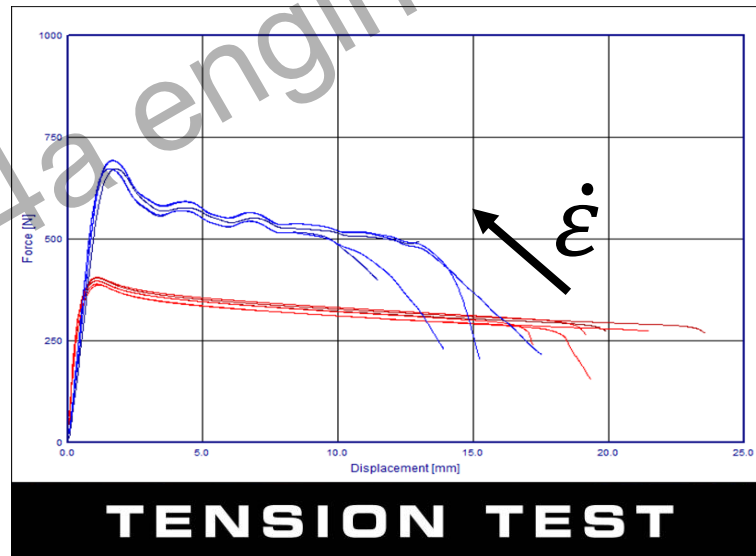
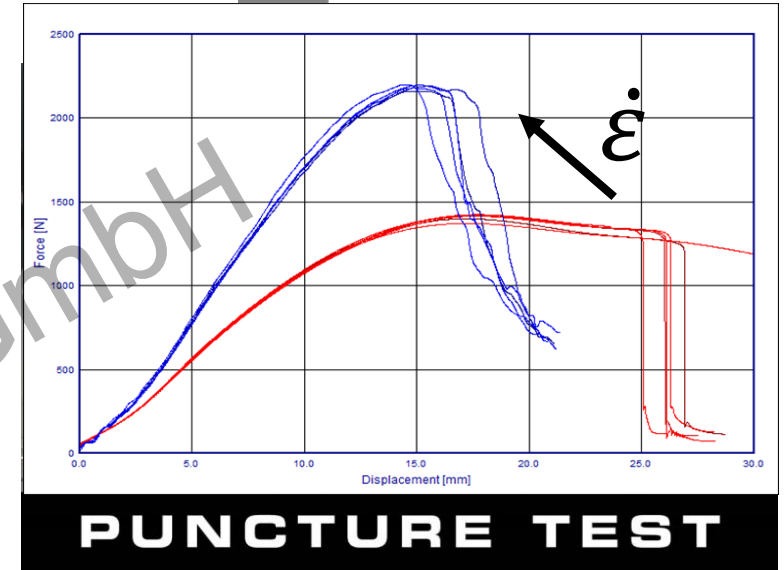
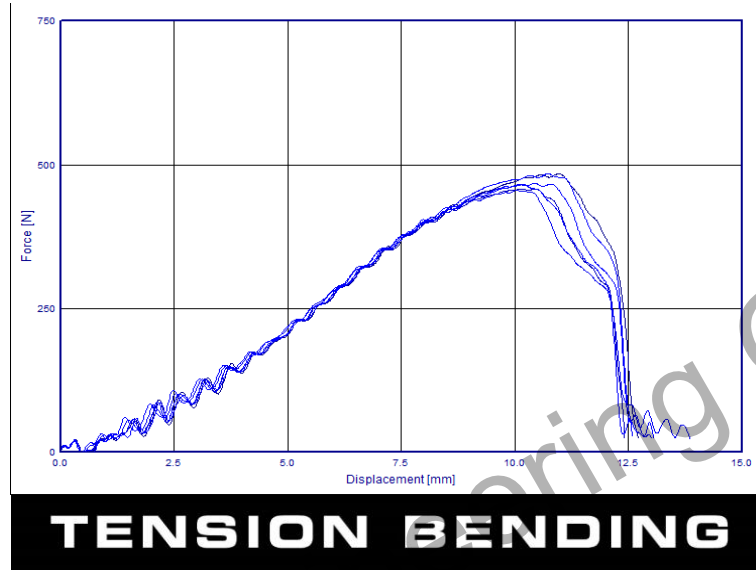
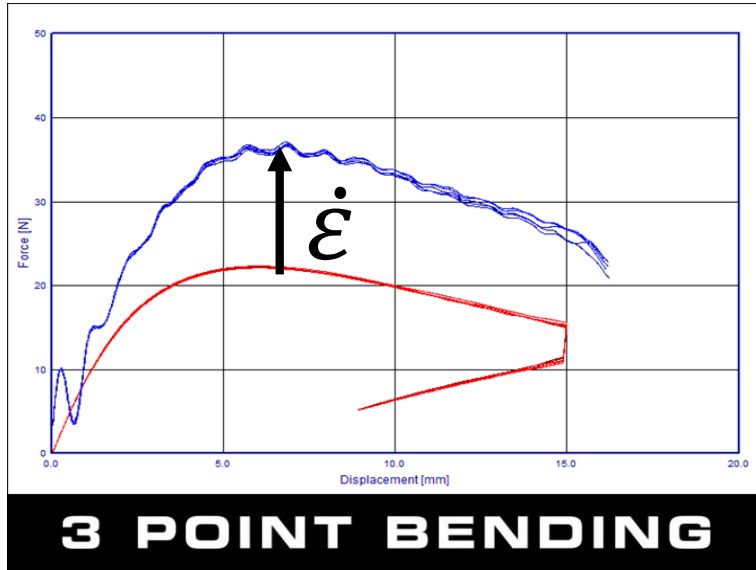


PUNCTURE TEST

IMPETUS™ ~ 3 m/s

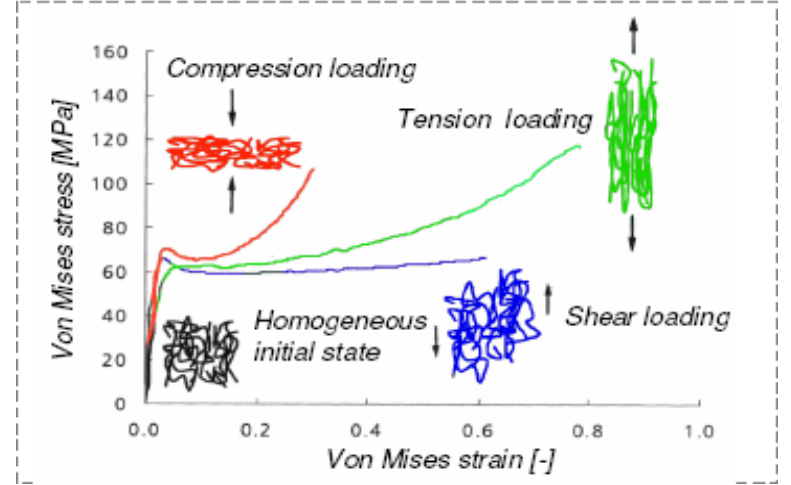
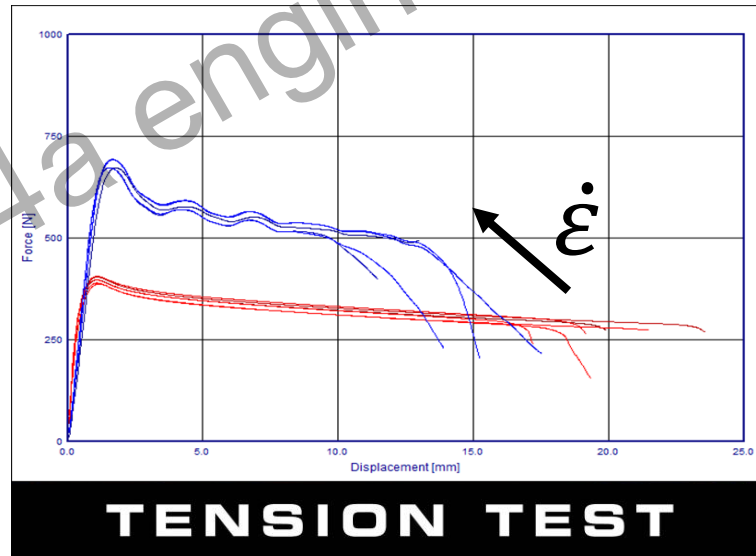
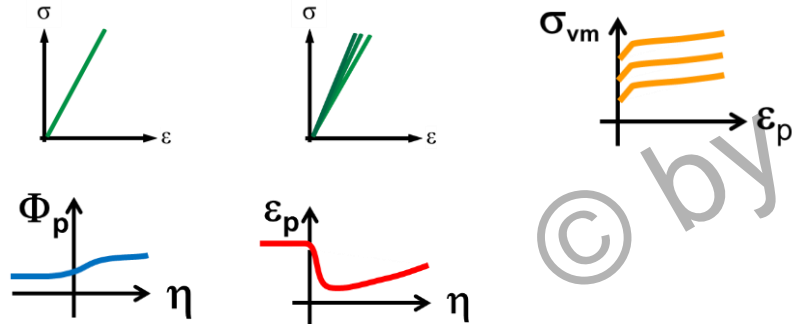
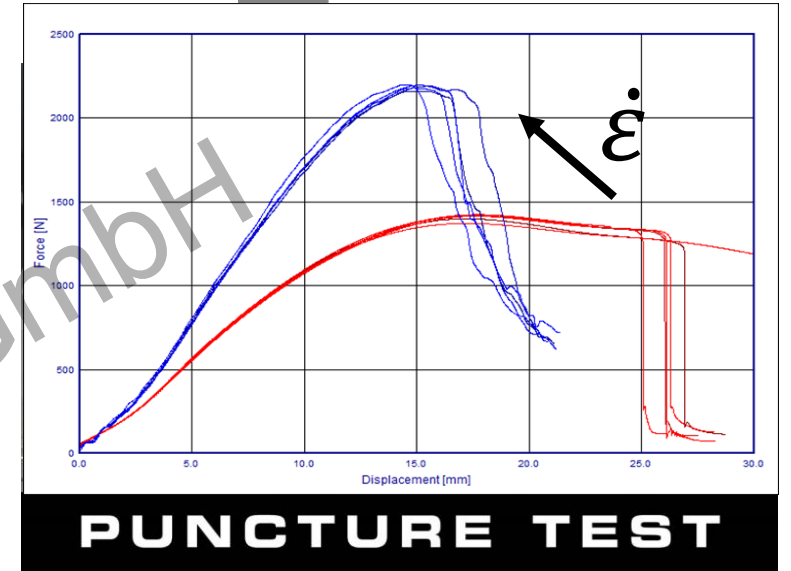
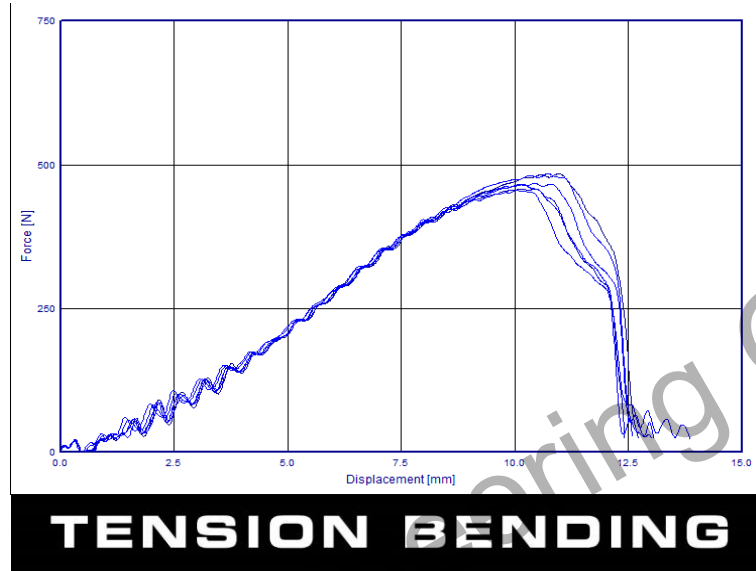
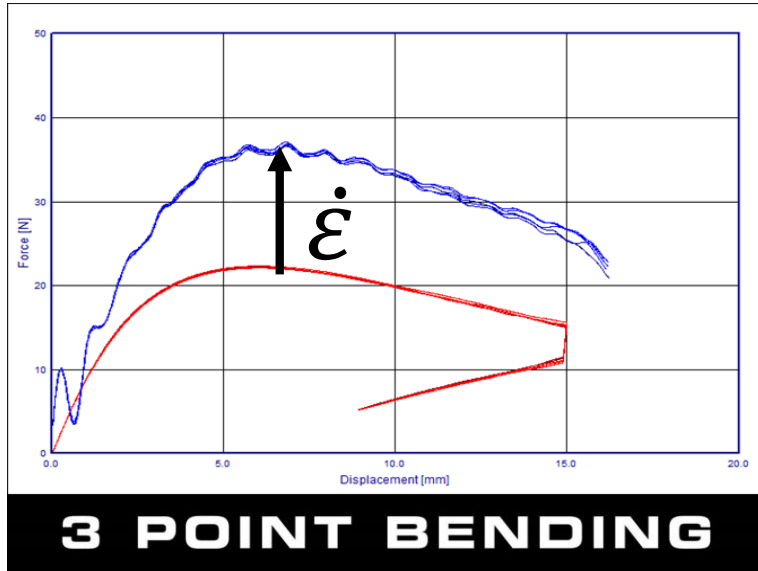


Measurement Results



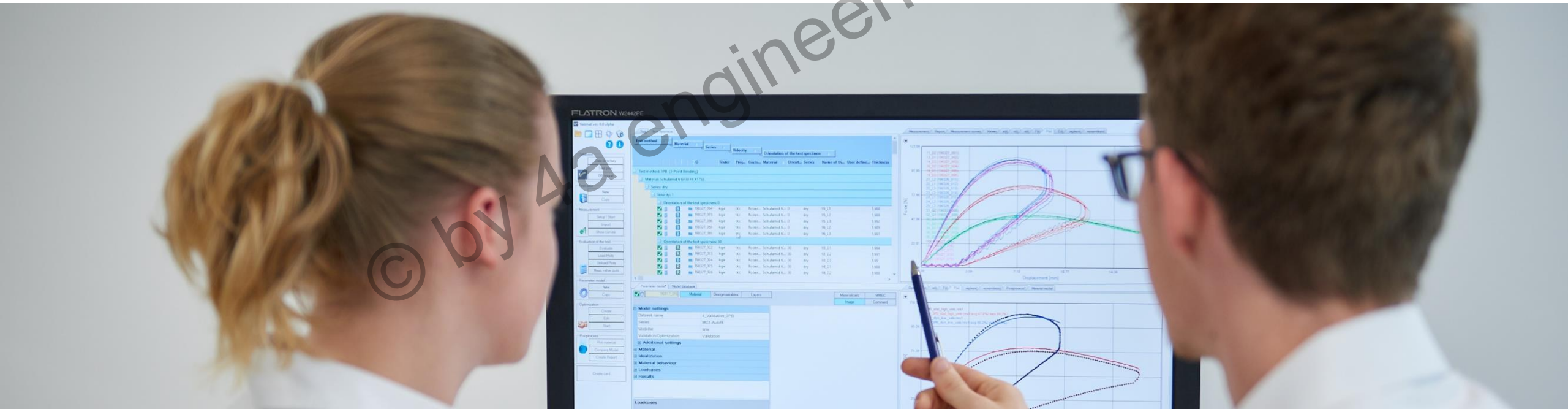
IMPETUS® ~ 3 m/s
static ~ 1 mm/s

Measurement Results → Material Model



Source: Mechanik der Kunststoffe W. Retting, Hanser Verlag 1991

From test to material card

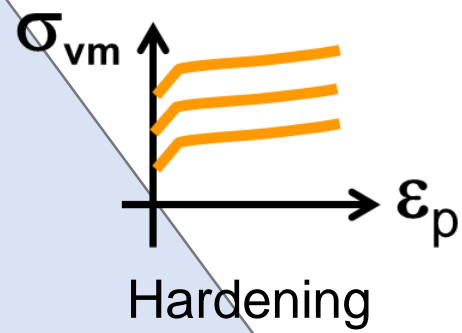
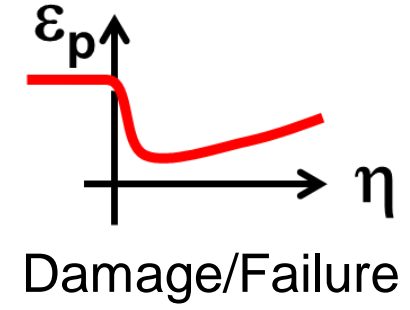
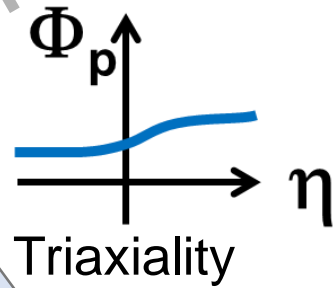
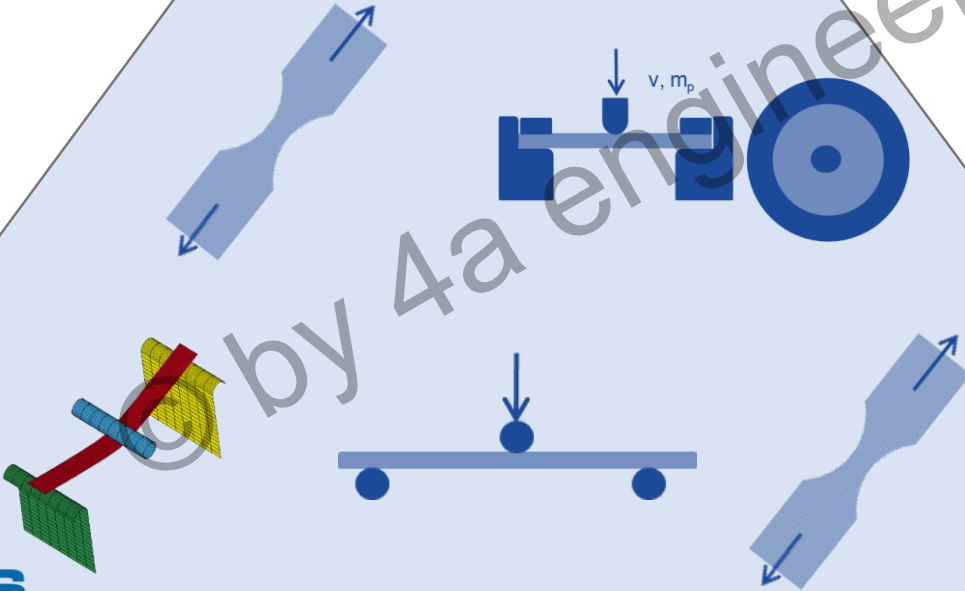
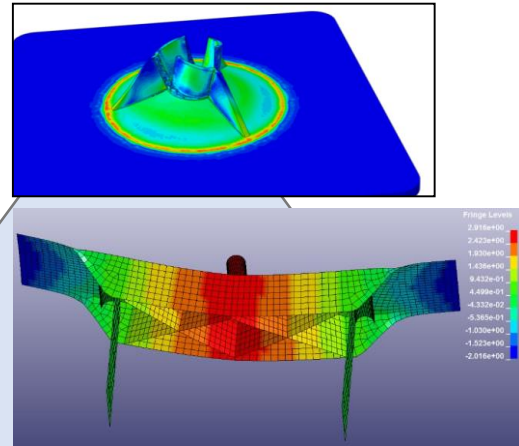


© by 4a engineering GmbH

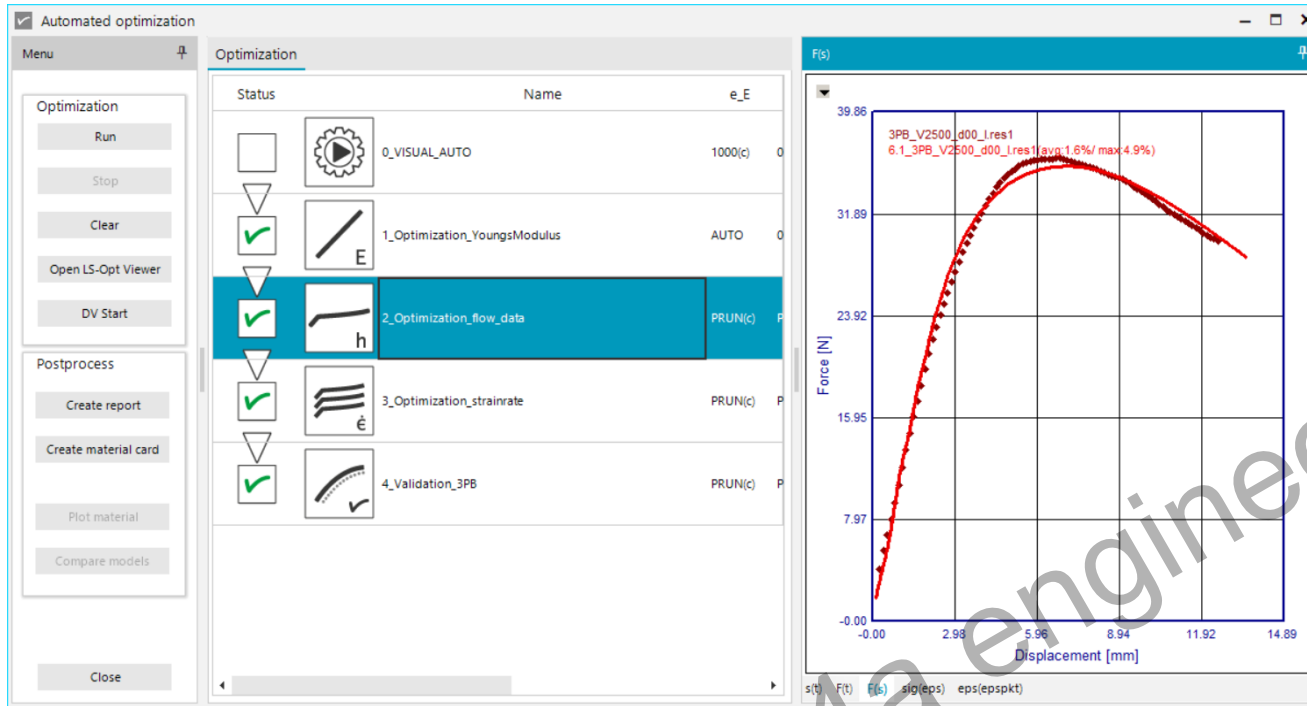
From test to material card



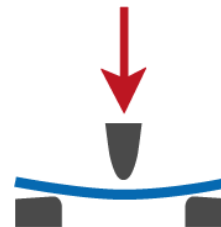
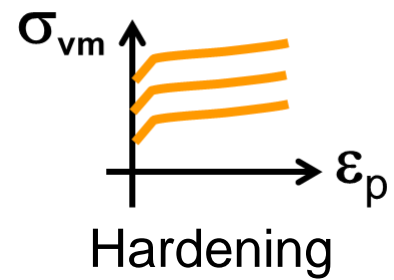
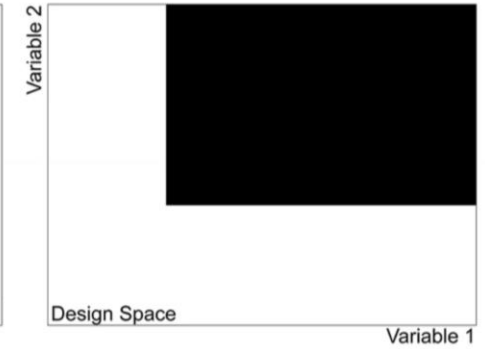
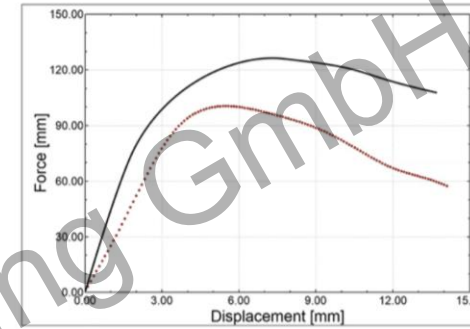
Deformation → Failure
 Creep → Static → Crash
 ISOTROPIC → ANISOTROPIC



Workflow for Material Card Generation - AUTOFIT

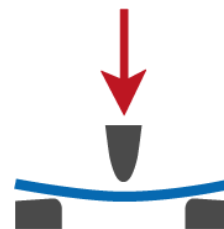
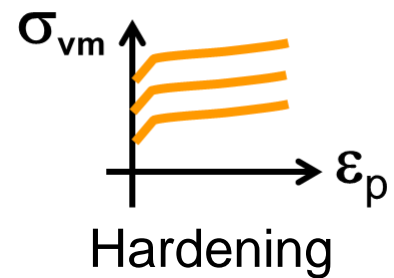
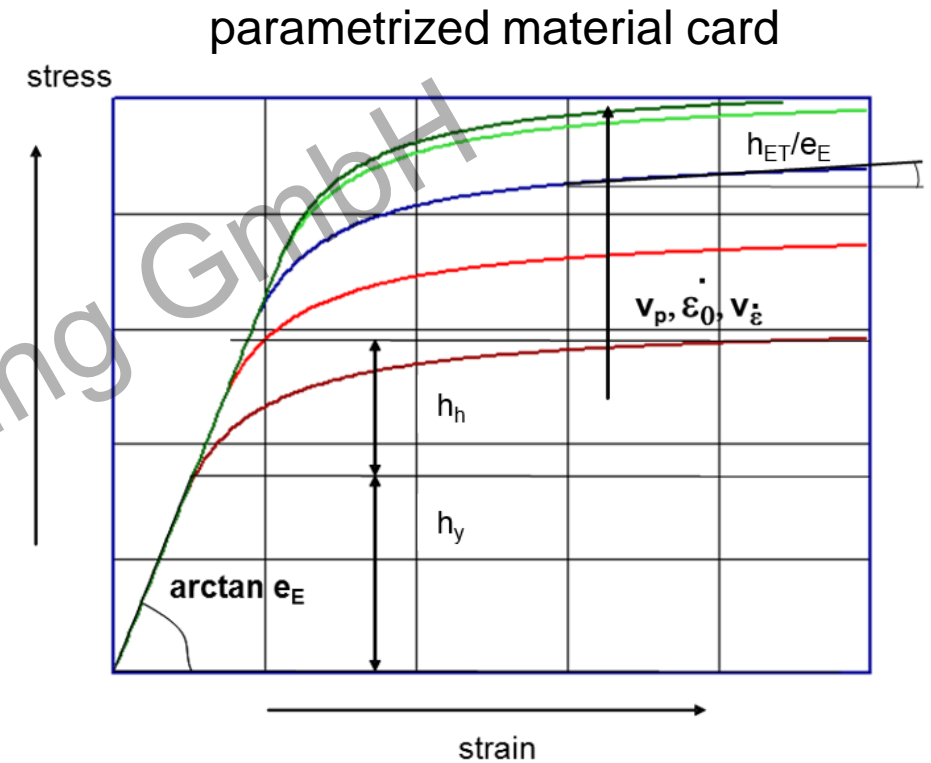
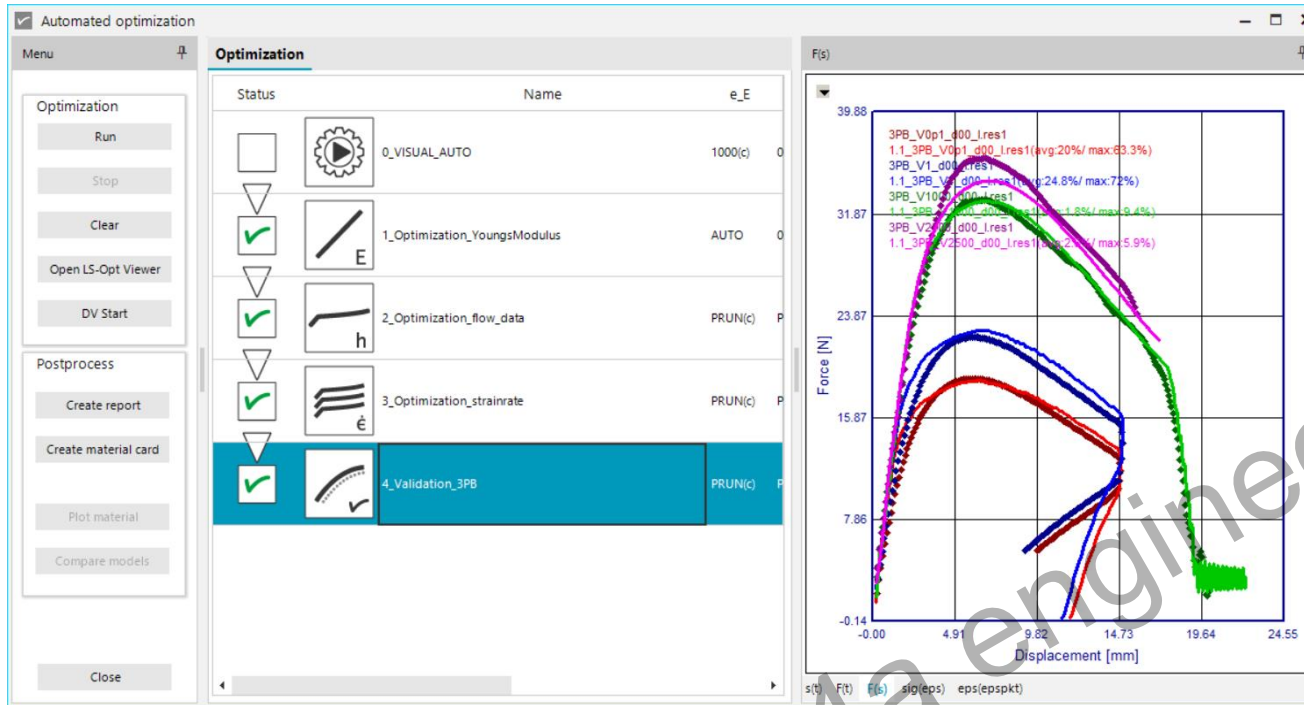


optimization – successive response surface method



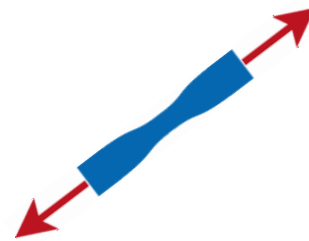
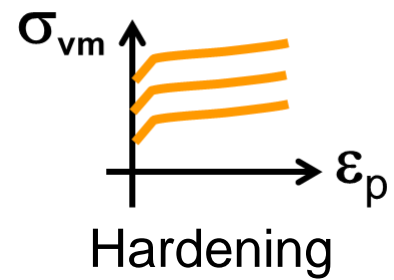
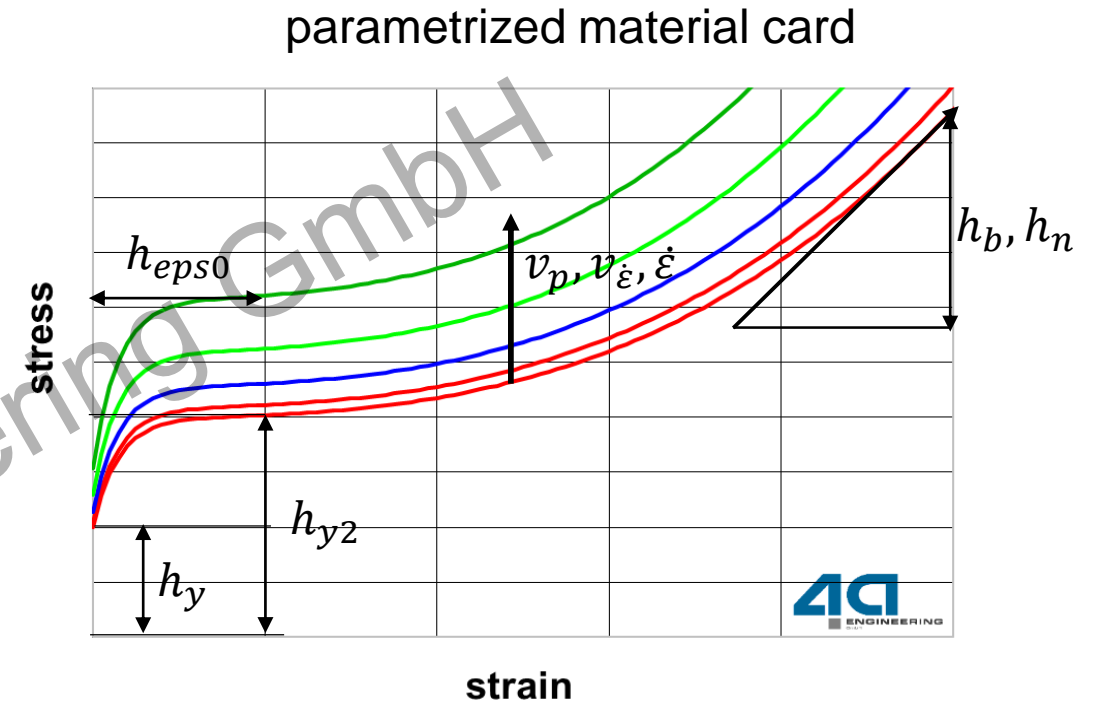
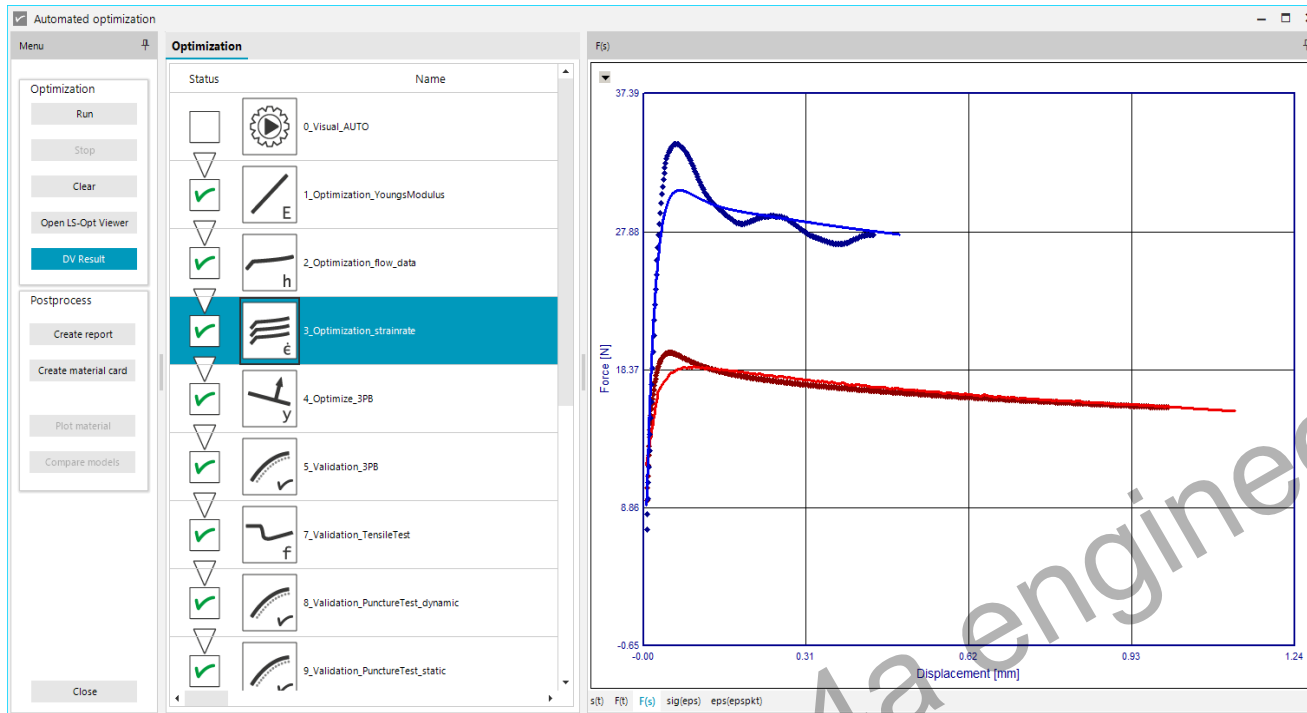
© by 4a engineering GmbH

Workflow for Material Card Generation - AUTOFIT



© by 4a engineering GmbH

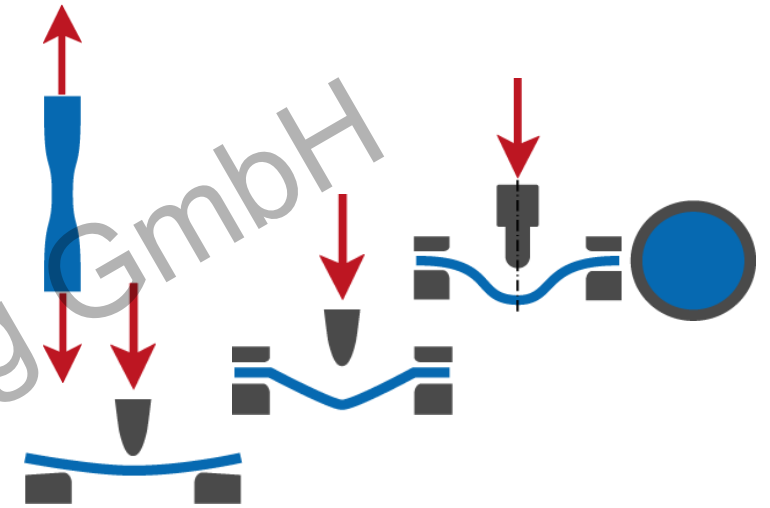
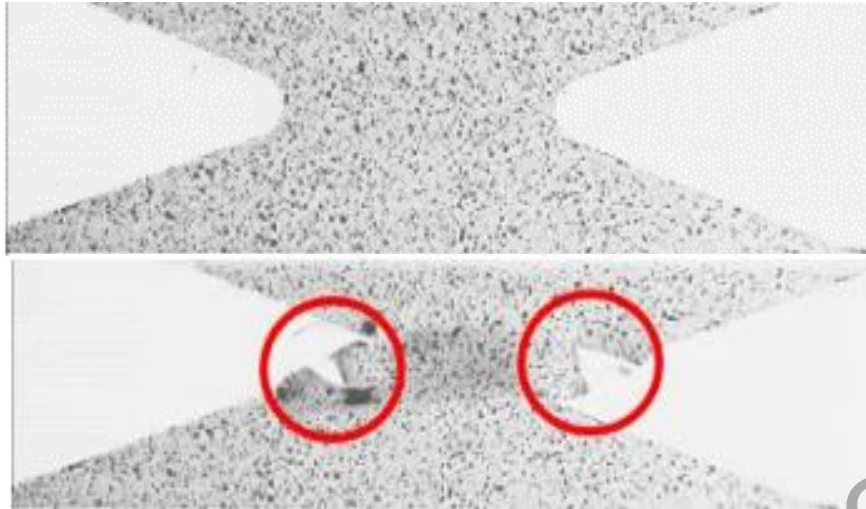
Workflow for Material Card Generation - AUTOFIT



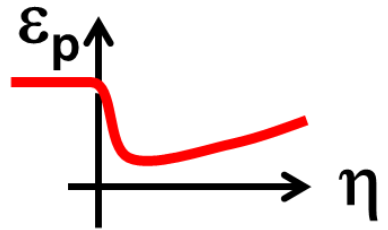
© by 4a engineering GmbH



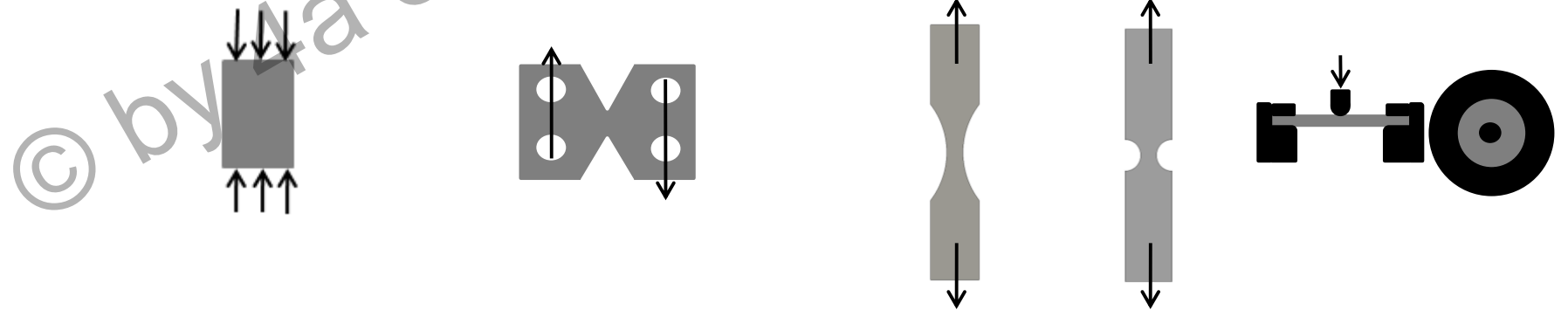
From test to material card



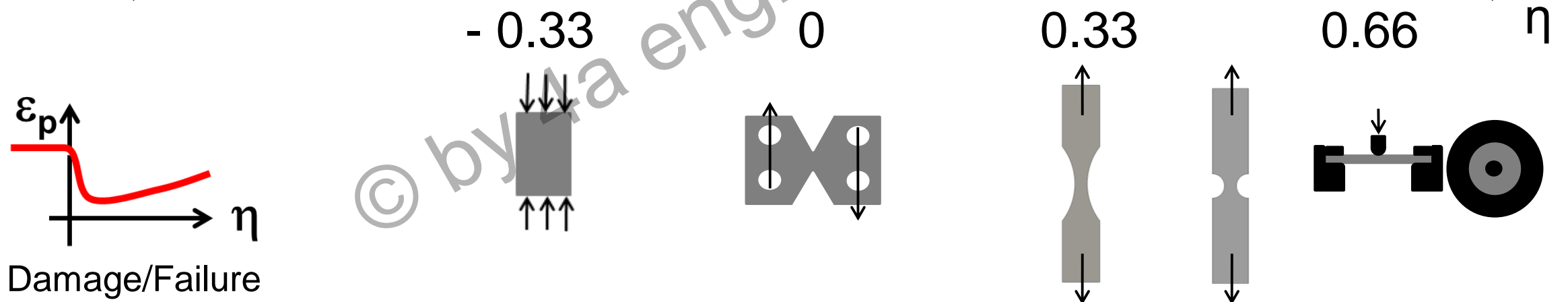
- 0.33 0 0.33 0.66 η



Damage/Failure



From test to material card



© by 4a engineering GmbH

Fracture models → *MAT_ADD_EROSION



Parameter model* Model database

170503_024 Material Designvariables Layers

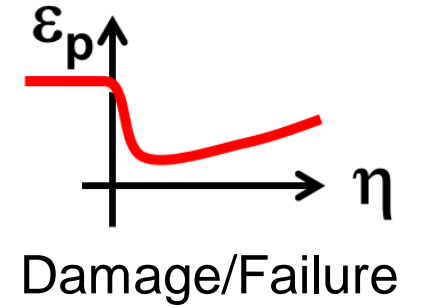
Materialcard MMEC
Image Comment

- Material behaviour
 - Material source
 - Elasticity
 - Plasticity
 - Failure/Damage
 - Material card
 - Materialcardcase
 - Damage/Failurecase
 - Materialcard id
 - Density
 - Plasticity
 - Function (Hardening, Elastic curve form)
 - Curve 1
 - Curve 2
 - Strain range upto
 - Sampling points
 - Bias factor
 - Strain rate dependency
 - Strain rate dependency
 - Fracture
 - Ductile Damage Settings
 - lower triax value
 - upper triax value
 - step size triax
 - Shear Damage Settings
 - FLC Damage Settings
 - Strainrate Settings
 - Postfracture
 - Loadcases
 - Results

Density	-1
Plasticity	vonMISES
Function (Hardening, Elastic cur	
Strain rate dependency	Table
Fracture	Damage
Ductile Damage Settings	Johnson Cook
Shear Damage Settings	None
FLC Damage Settings	plastic equivalent strain
Strainrate Settings	simple criteria
Postfracture	4a picewise linear
Loadcases	Johnson Cook
Casename	mod Xue-Wierzbicki
Tests	Xue-Wierzbicki
Settings optimization	Mohr-Coulomb
Weighting case	1

Ductile Damage Settings

	0.33	Johnson Cook
	None	mod Xue-Wierzbicki
	None	Xue-Wierzbicki
	Johnson Cook	Mohr-Coulomb
	Fracture Energy (TRIAx)	



Materialcard MMEC
Image Comment

$f_{dJCD1} + f_{dJCD2} \cdot e^{-f_{dJCD3} \cdot \eta}$

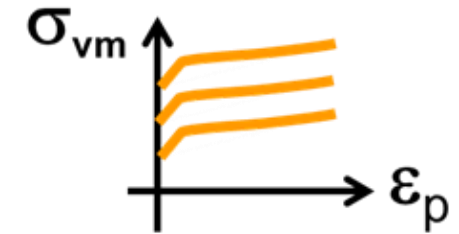
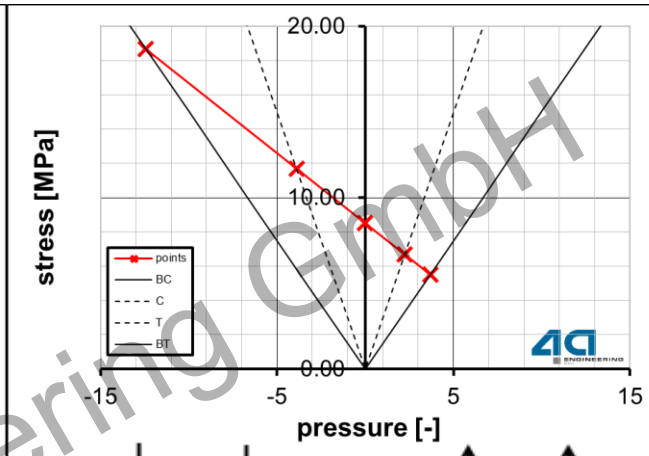
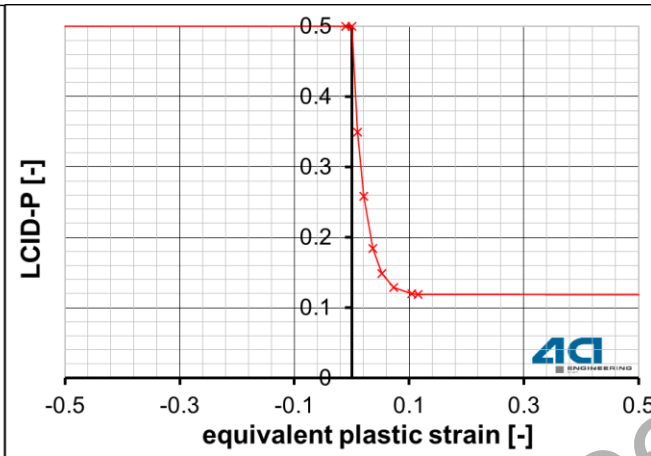
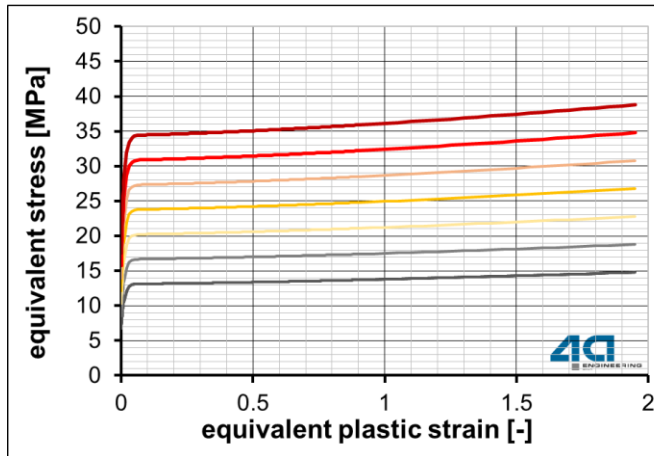
failure strain [-]

triaxiality [-]

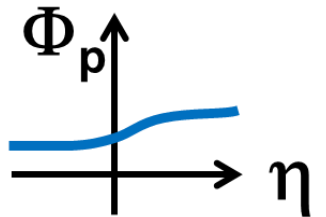
4a



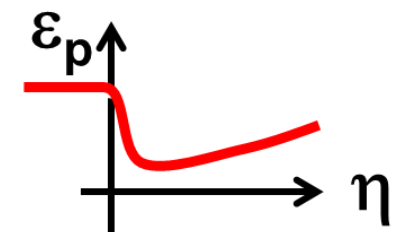
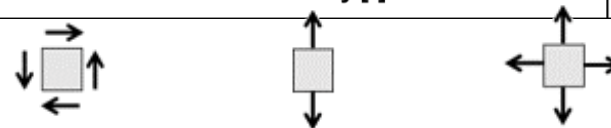
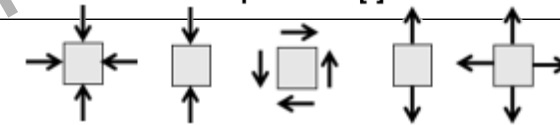
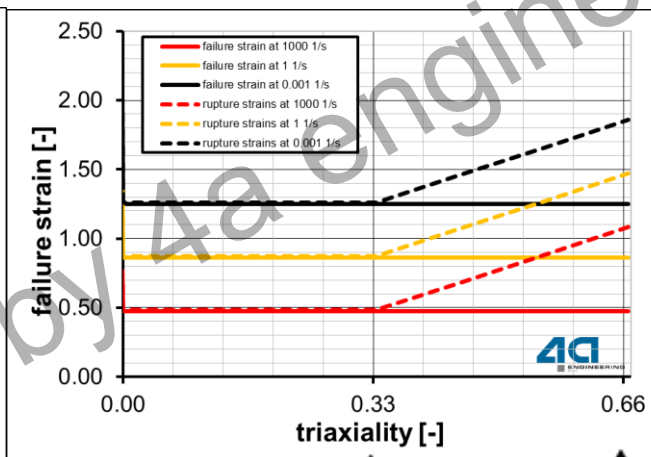
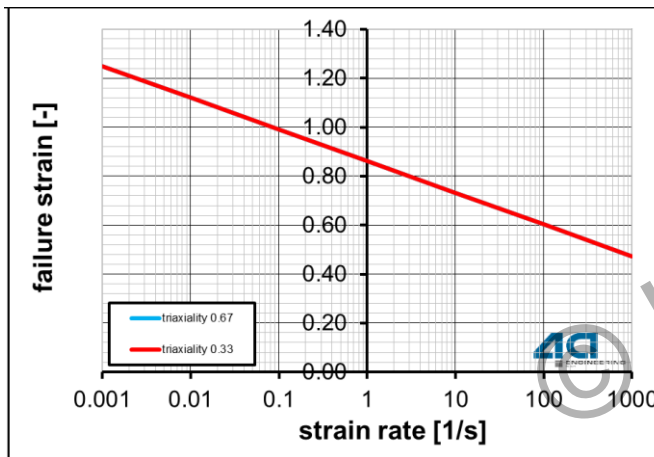
Workflow Result: *MAT_SAMP-1 with internal FM - AUTOFIT



Hardening



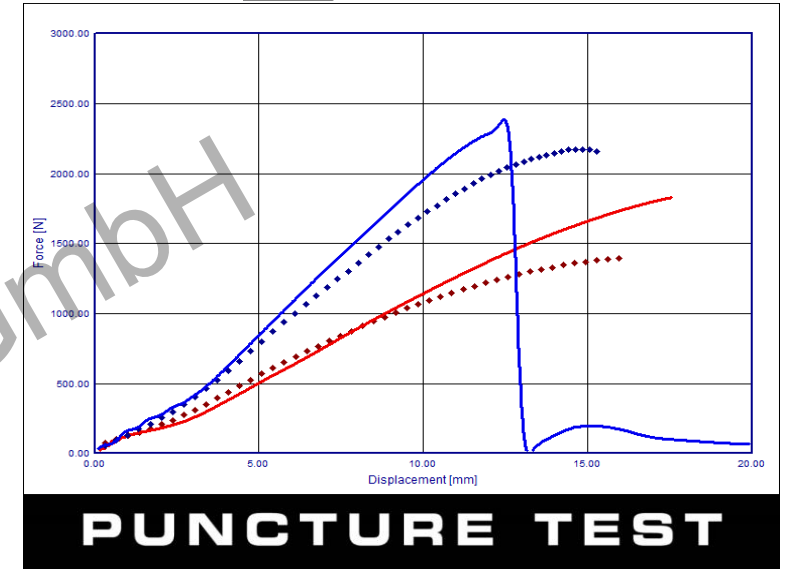
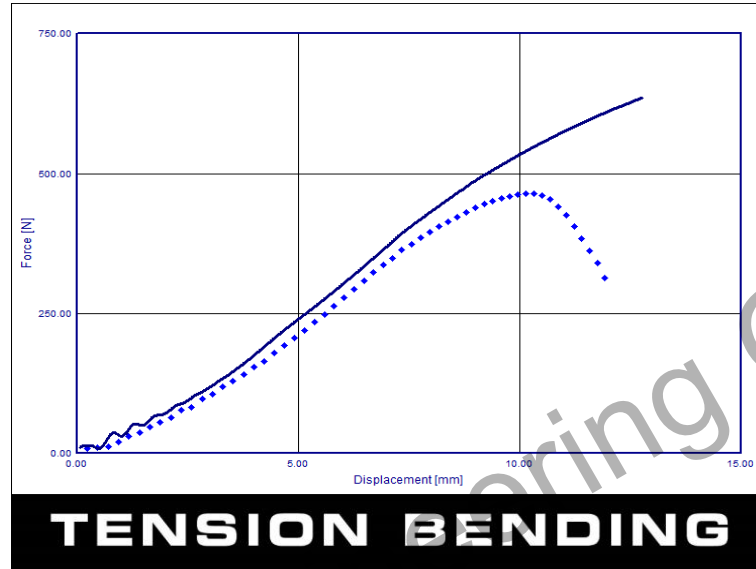
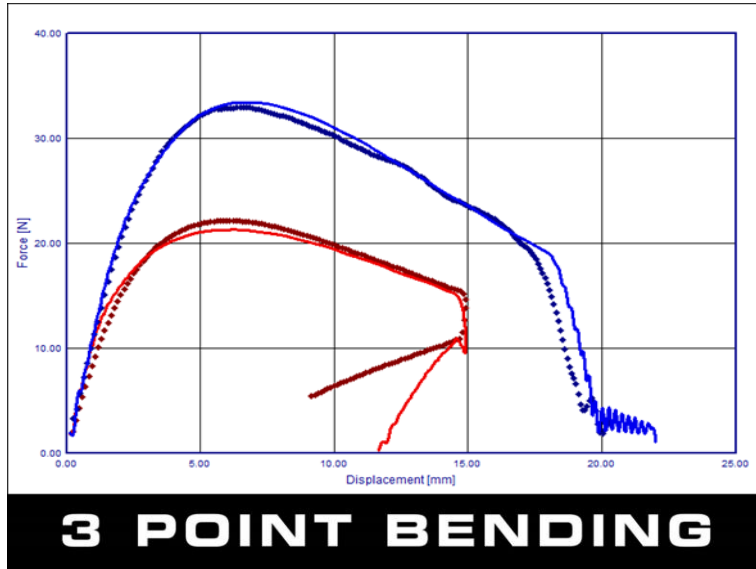
Triaxiality



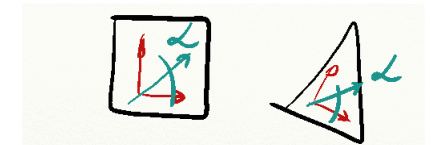
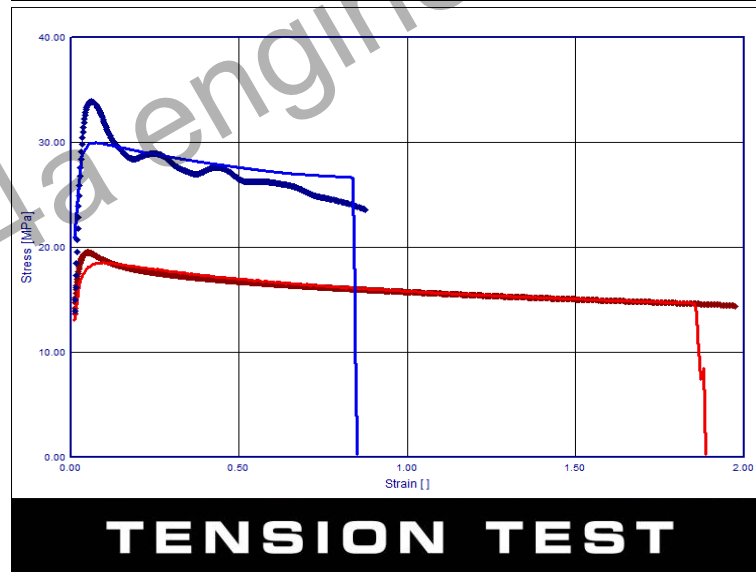
Damage/Failure

source: Benjamin Hirschmann, master thesis





IMPETUS® ~ 3 m/s
static ~ 1 mm/s



..... averaged test curves
— result of simulation

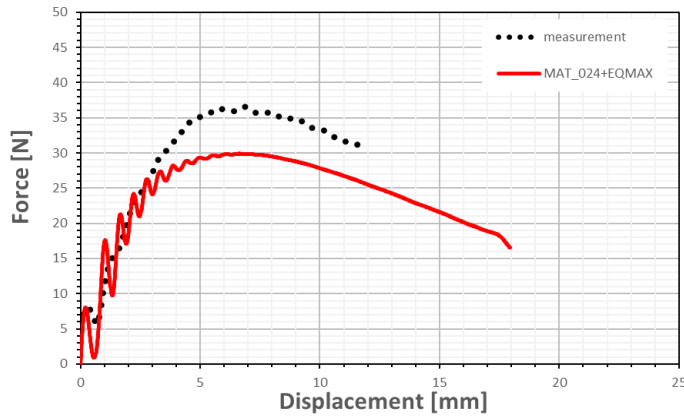
source: Benjamin Hirschmann, master thesis

Comparison different material models

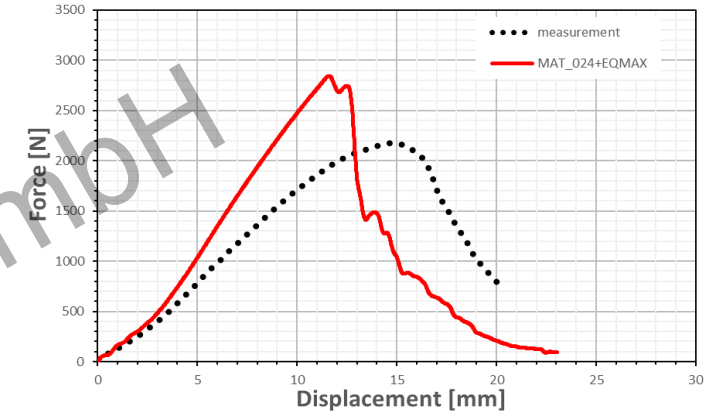
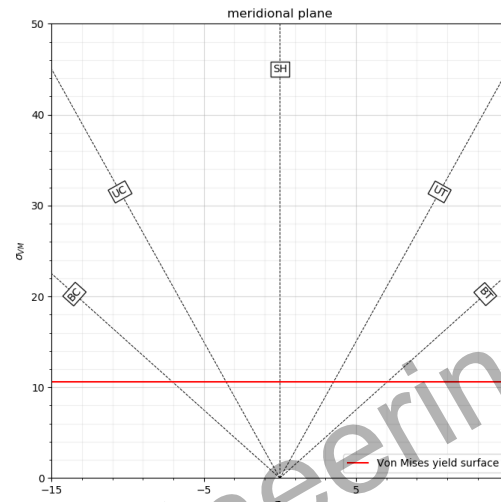
- stability
- numerical cost
 - number of operations in material model → Translation into simulation model (localization, load path,...)
 - relative numerical cost of the material model (measurement model comparison)
- accuracy



Relative Numerical Cost of the Material Model – MAT_024

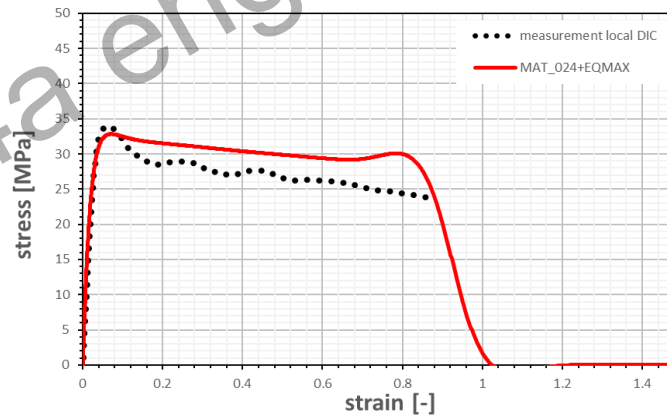


3 POINT BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



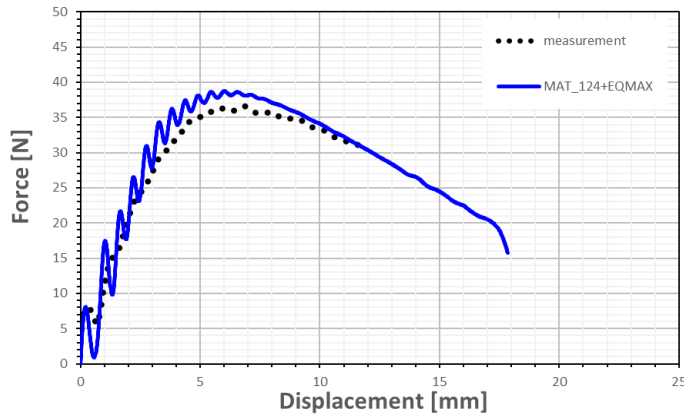
TENSION TEST

..... averaged test curves
 — result of simulation

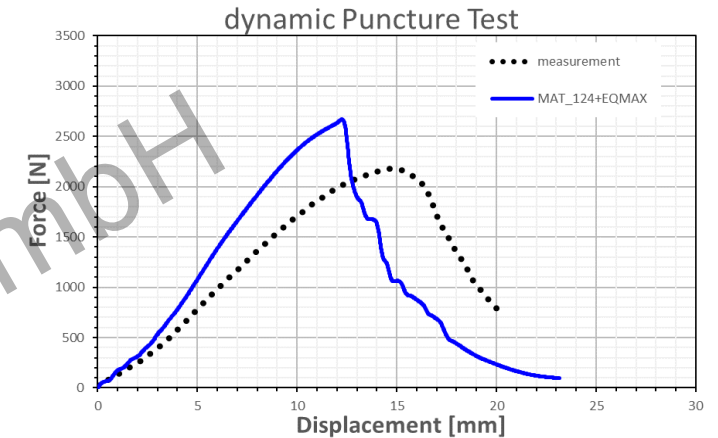
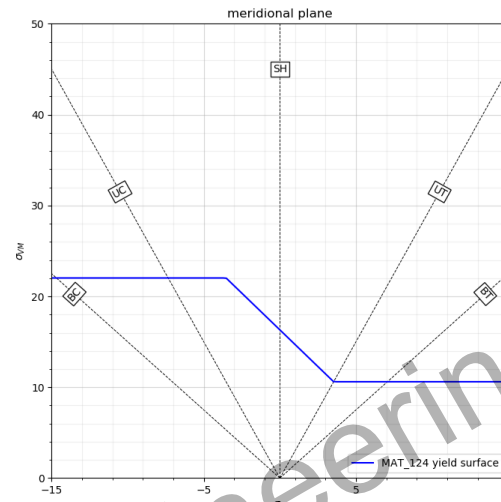
source: Benjamin Hirschmann, master thesis



Relative Numerical Cost of the Material Model – MAT_124

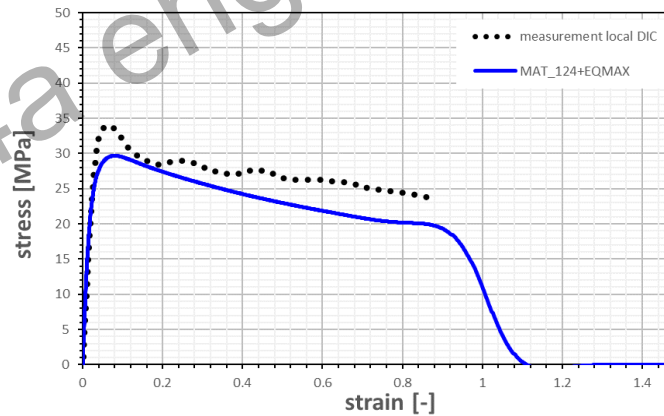


3 POINT BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



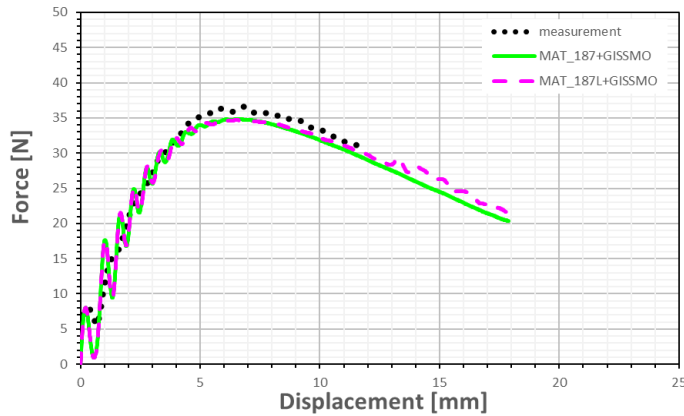
TENSION TEST

..... averaged test curves
 — result of simulation

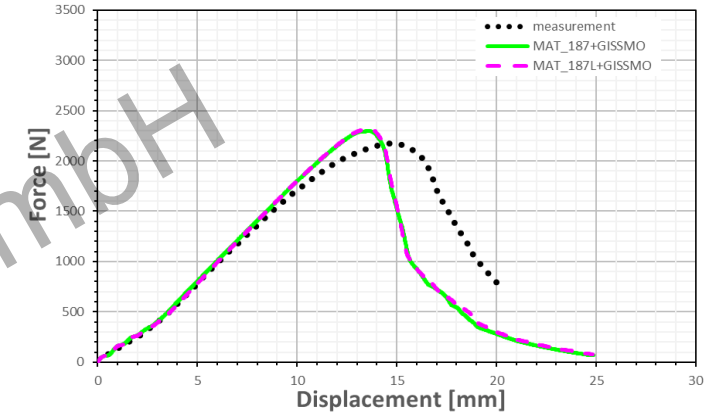
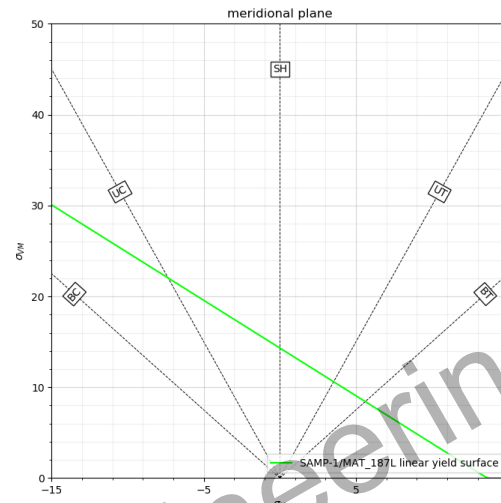
source: Benjamin Hirschmann, master thesis



Relative Numerical Cost of the Material Model – MAT_187

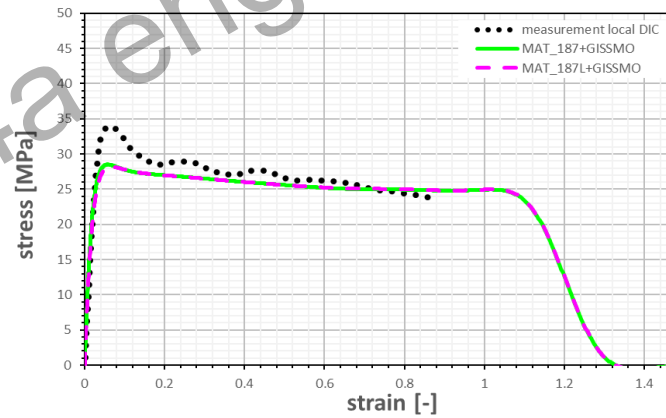


3 POINT BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



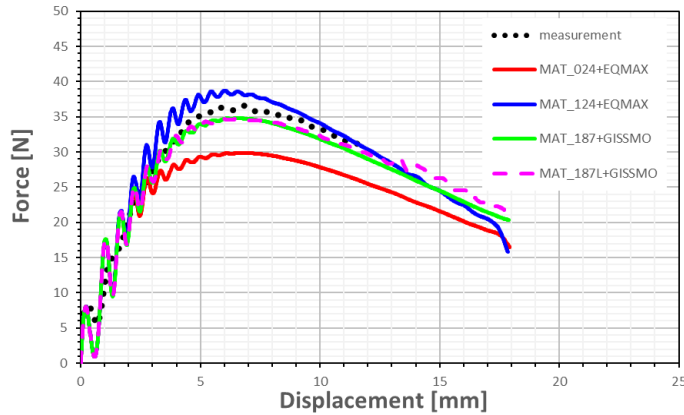
TENSION TEST

..... averaged test curves
 — result of simulation

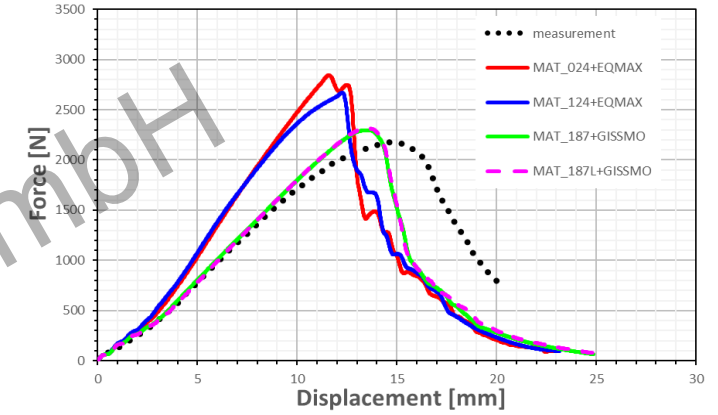
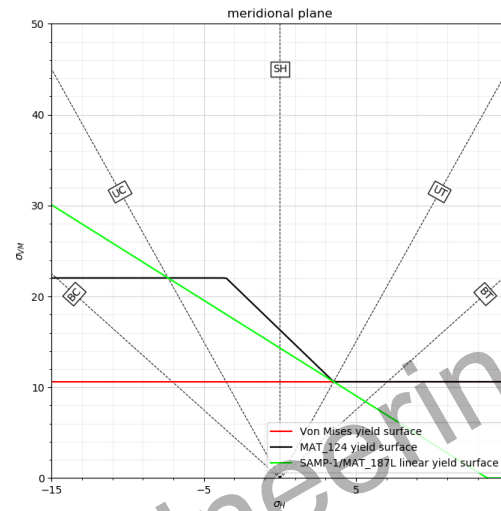
source: Benjamin Hirschmann, master thesis



Relative Numerical Cost of the Material Model

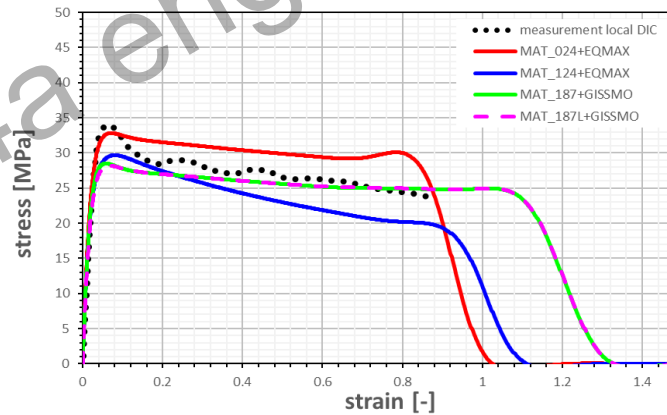


3 POINT BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



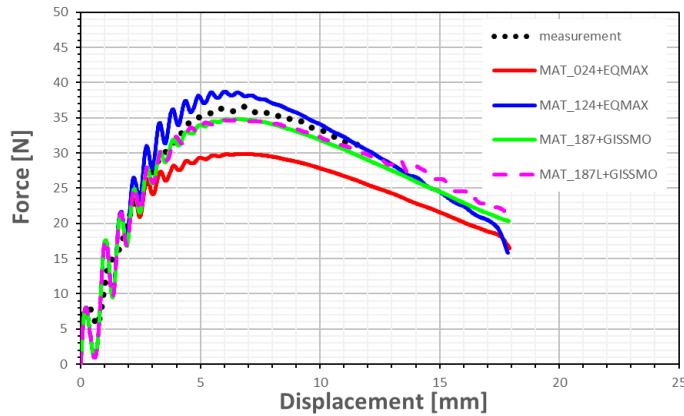
TENSION TEST

..... averaged test curves
 — result of simulation

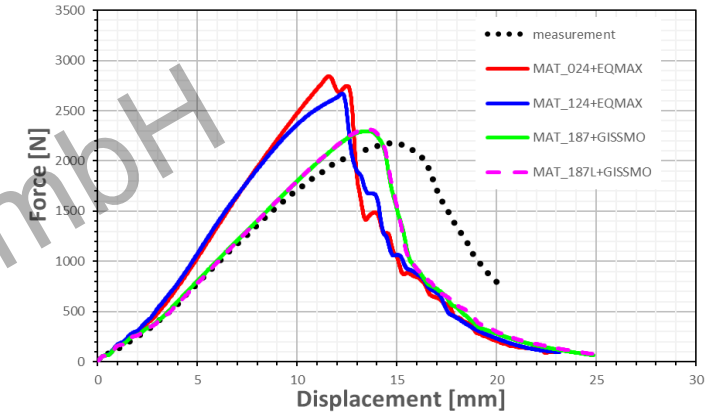
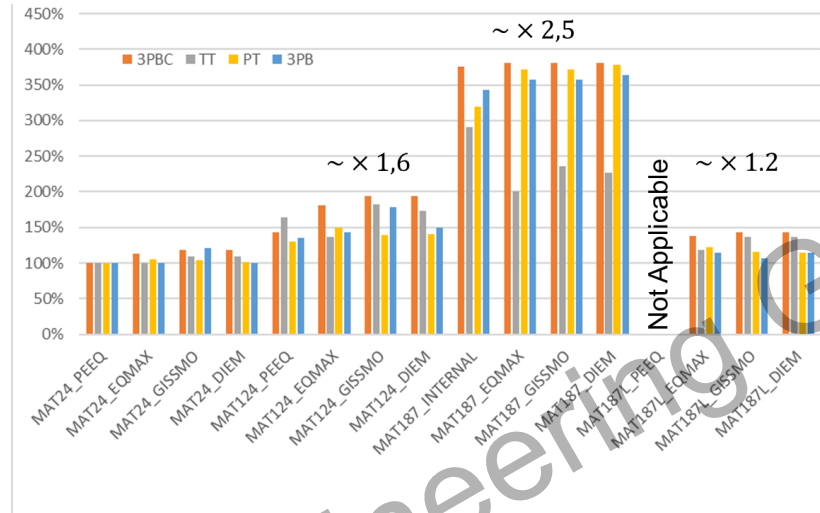
source: Benjamin Hirschmann, master thesis



Relative Numerical Cost of the Material Model

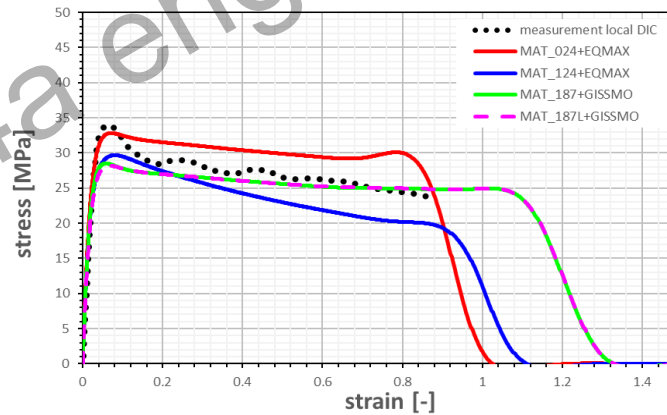


3 POINT BENDING



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



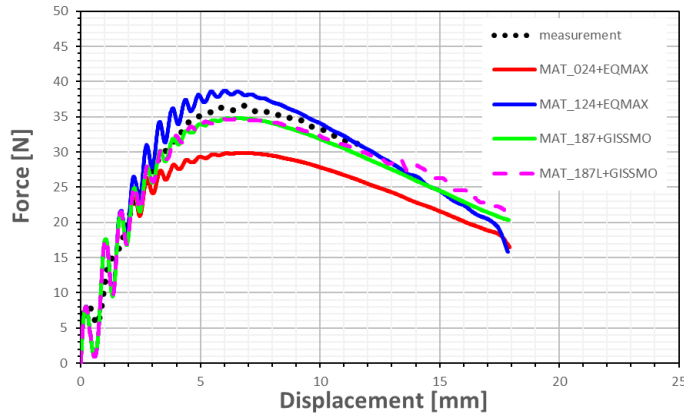
TENSION TEST

..... averaged test curves
 — result of simulation

source: Benjamin Hirschmann, master thesis



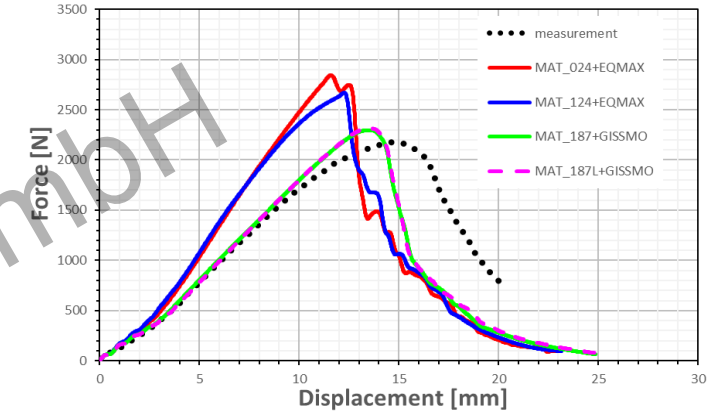
Relative Numerical Cost of the Material Model



3 POINT BENDING

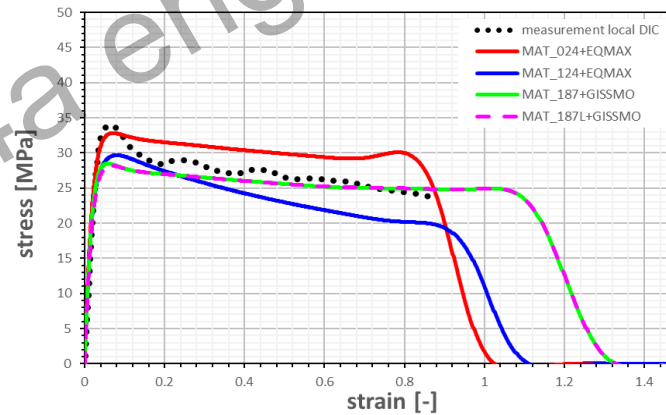
Material model	CPU Time
*MAT_024	1
*MAT_124	1.6
*MAT_187	2.5
*MAT_187L	1.2

CPU Time comparisons



PUNCTURE TEST

IMPETUS™ ~ 3 m/s



TENSION TEST

..... averaged test curves
 — result of simulation

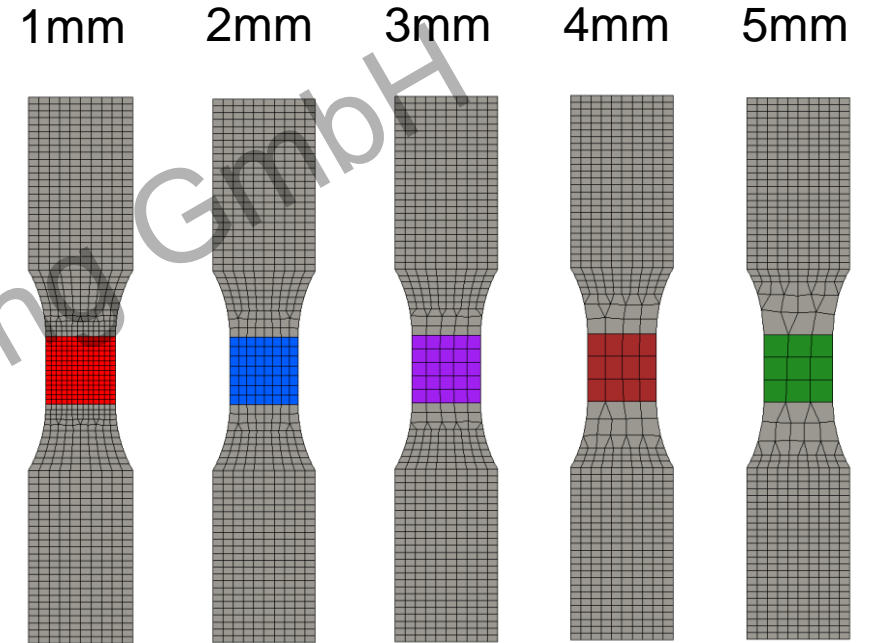
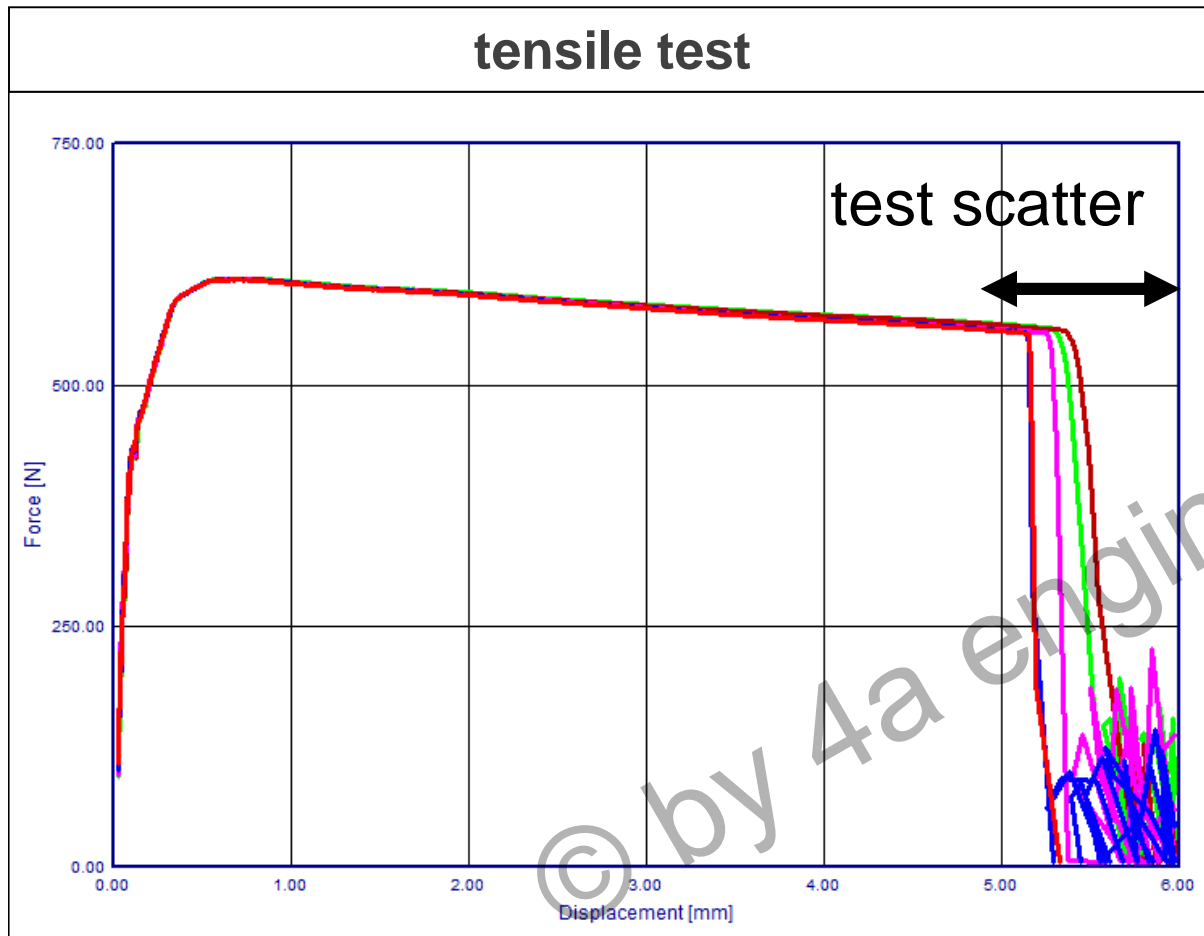
source: Benjamin Hirschmann, master thesis



Element Regularisation

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*MAT-SAMP 1 with internal failure model – influence element size

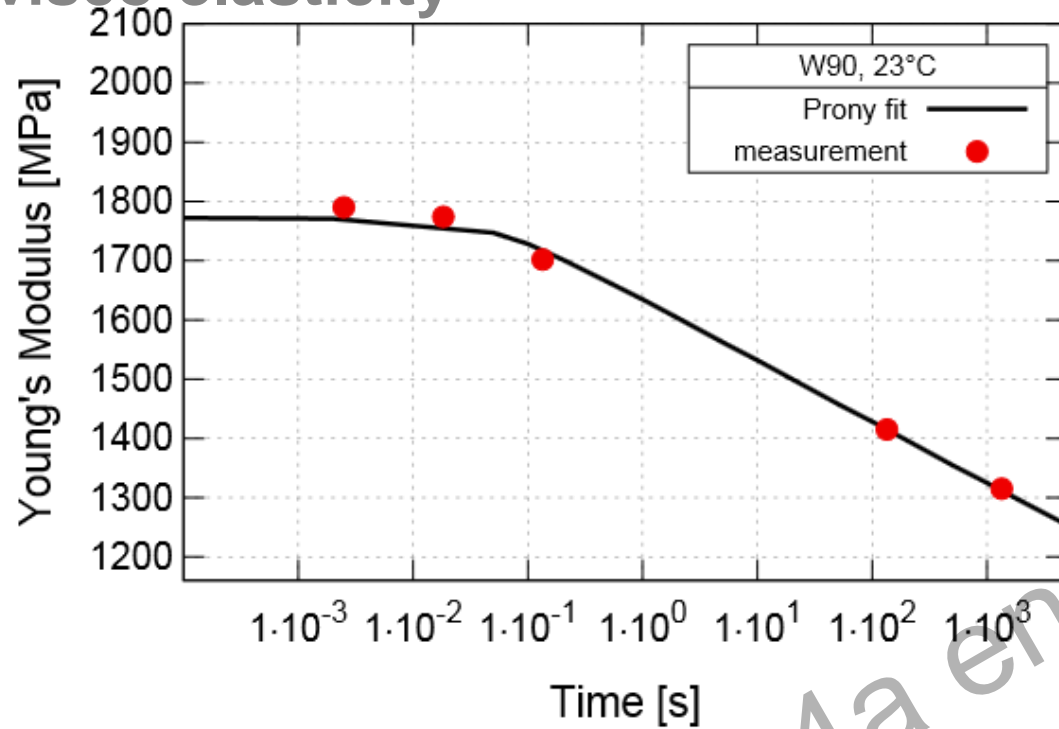


source: Benjamin Hirschmann, master thesis

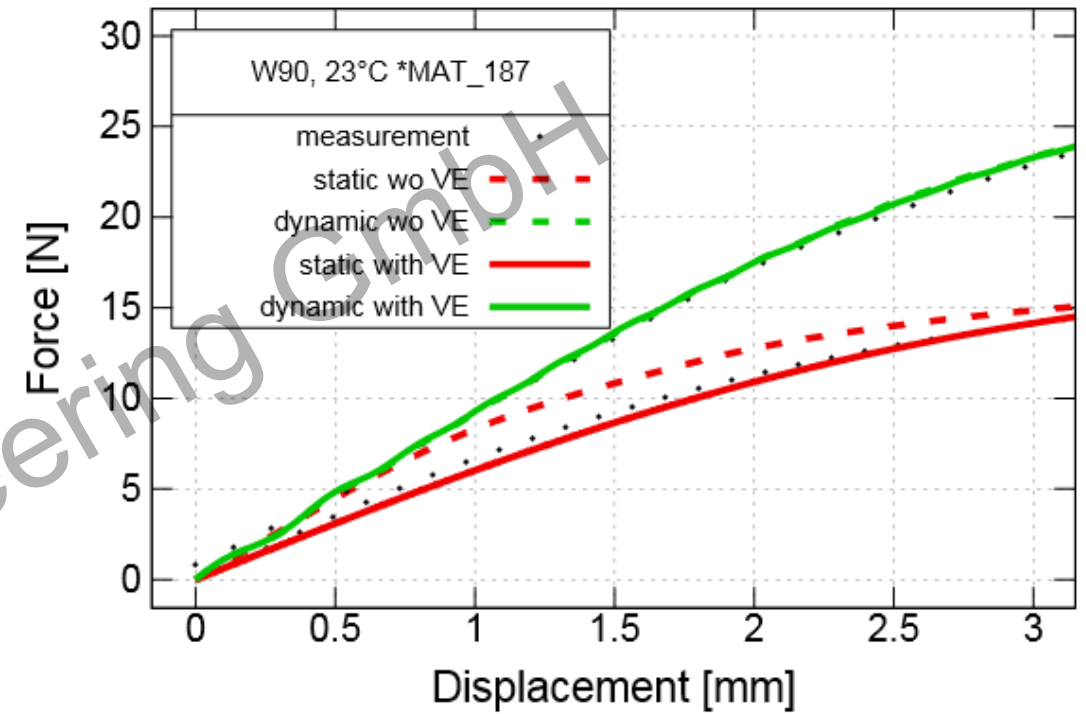
UPCOMING MODELS
***MAT_ADD_INELASTICITY**

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Upcoming material models visco-elasticity



→ implementing visco-elasticity:
6-term Prony fit to use in **MAT_124*

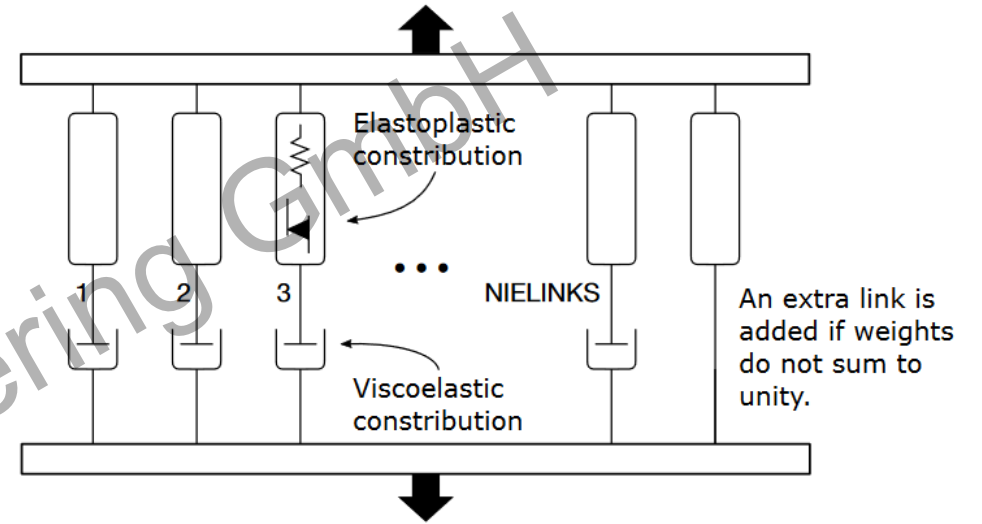


→ implementing visco-elasticity:
strain-rate dependent Young's Moduli
to use in **MAT_187*

Upcoming material models

*MAT_ADD_INELASTICITY

- the purpose of this card is to add inelastic features to a standard arbitrary material card → modular concept
- supported in implicit and explicit for a few element types → under development
- inelastic features
 - isotropic hardening plasticity
 - creep
 - Visco-elasticity



LS-DYNA_Manual_Volume_II_Dev (r:11680)

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Anisotropic Failure

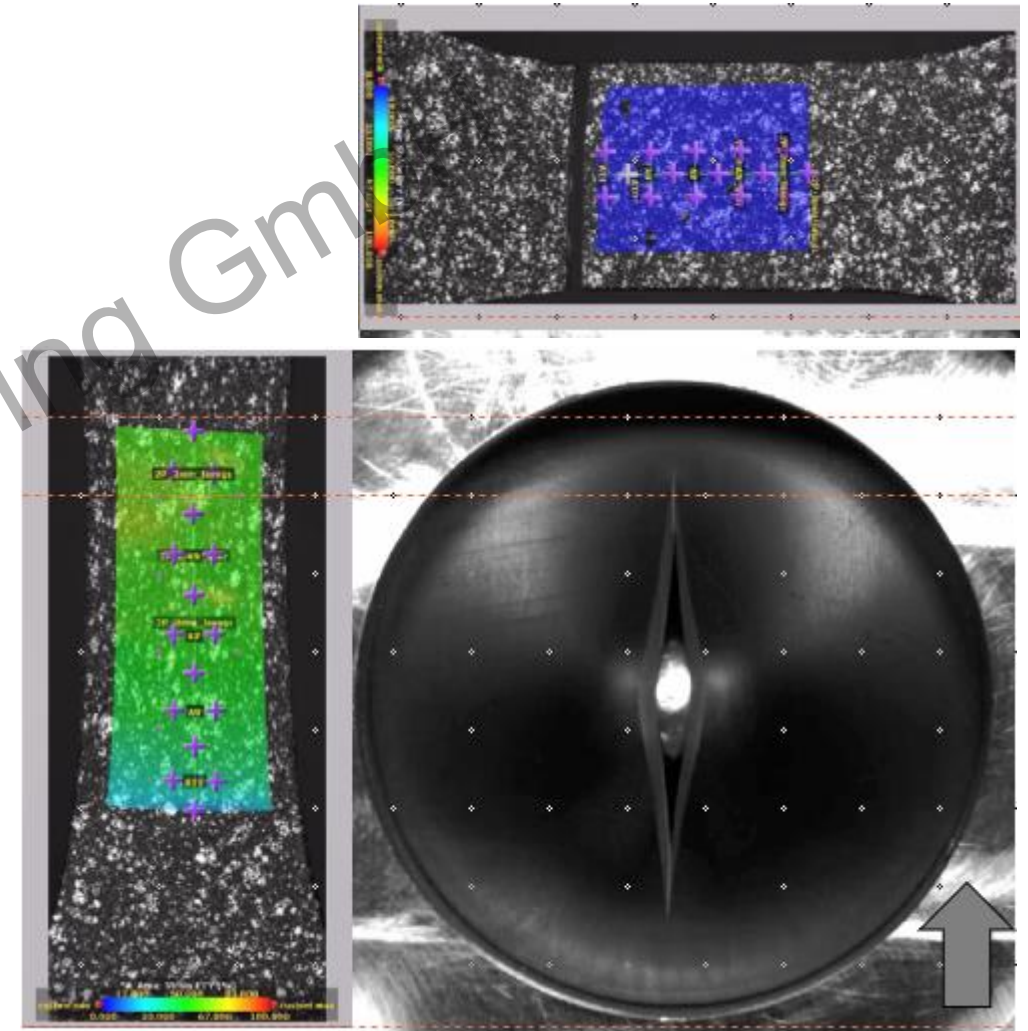
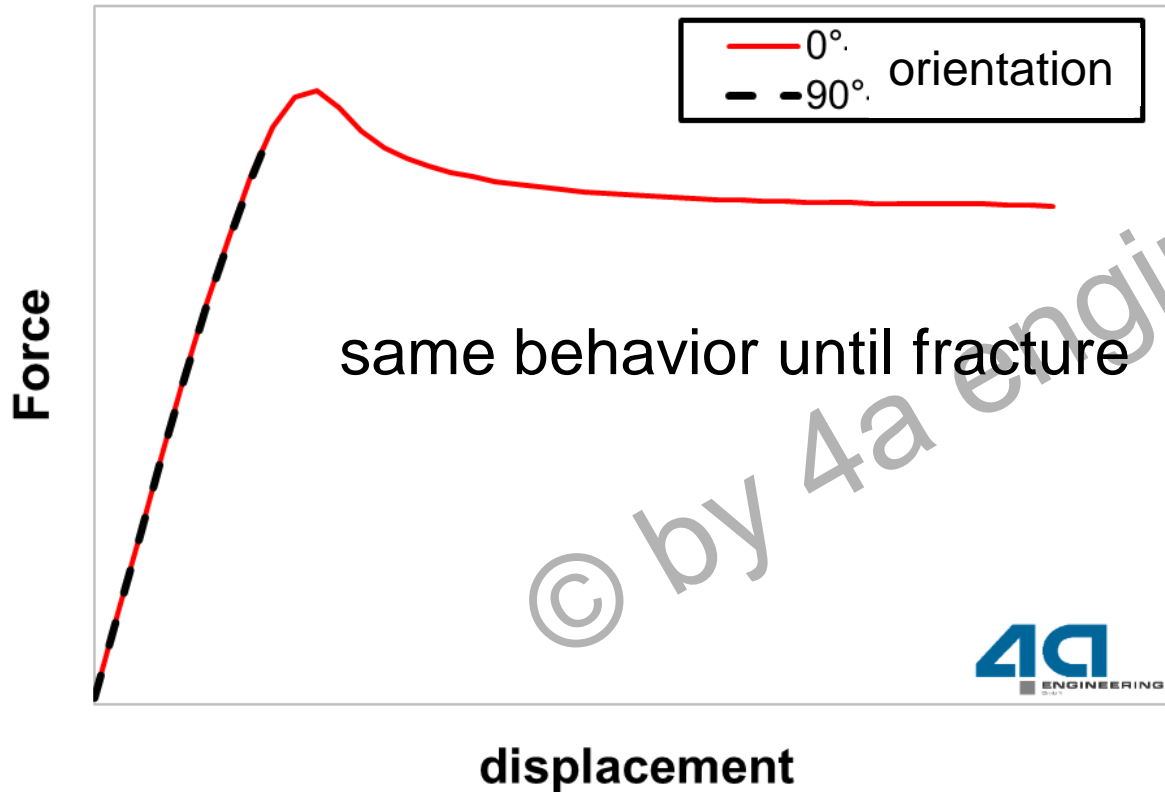
(*MAT_ADD_GENERALIZED_DAMAGE)

Plastics ?

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Influence of manufacturing process on failure

- example: ABS
 - The induced orientation by the injection molding process leads to an anisotropic failure behavior.



Summary
Part 1: Modeling of isotropic thermoplastics

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Summary Deformation

- Motivation and general material behavior of thermoplastics
- dynamic and static measurements for a talc filled PP
- discussed material models
 - ***MAT_024** → ***MAT_SAMP-1**
 - describe observed deformation behavior
 - numerical costs
- ***MAT_187L** – new material model
 - small increase in numerical costs **1.2**
 - **qualitative accuracy** of the simulation results could be **improved**.

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Summary Failure

- material characterization in the triaxiality range of 0.33 to 0.66
- GISSMO \neq DIEM (each model has some specialties)
 - GISSMO can be used for plastics
→ benefits of model often not used for plastic materials
 - DIEM → table input for initial failure enables more flexibility over triaxiality / over strain rate → BIAx
- **Simple as Possible, as Complex as Necessary**
- tools needed to handle data and to fit complex failure models



IMPETUS



VALIMAT

Intelligent reliable solutions for plastics, composites, metals, foams, ...

◀ **IMPETUS**

✓ **VALIMAT**

◉ **MICROMECH**

➔ **FIBERMAP**

Foams

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

Metals

efficient
dynamic testing

from test to validated
material cards

3D anisotropic
material cards

individual mapping
process information

Intelligent reliable solutions for plastics, composites, metals, foams, ...

IMPETUS



VALIMAT



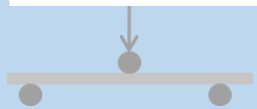
MICROMECH



FIBERMAP



Fiber reinforced Plastics (SFRT & LFRT)



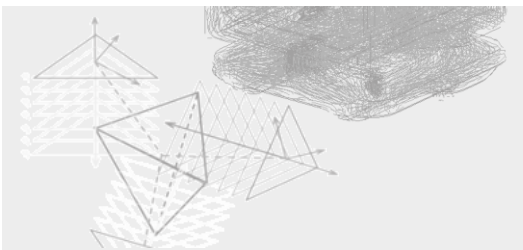
efficient
dynamic testing



from test to validated
material cards



3D anisotropic
material cards

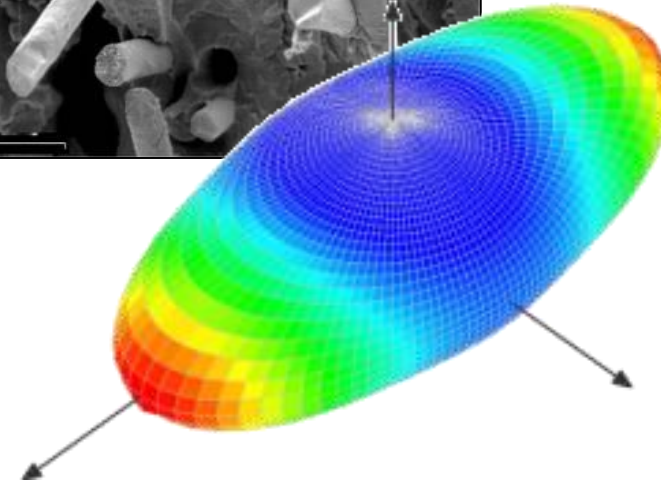
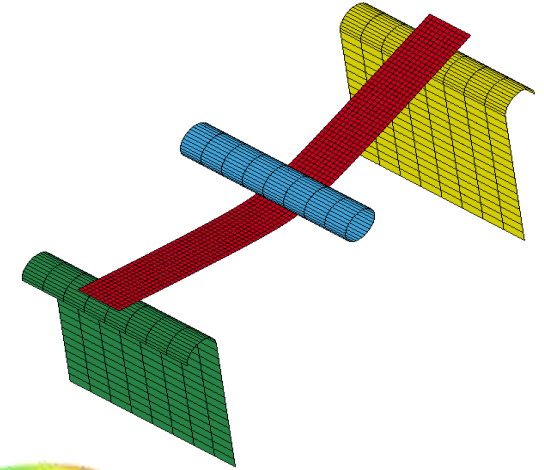
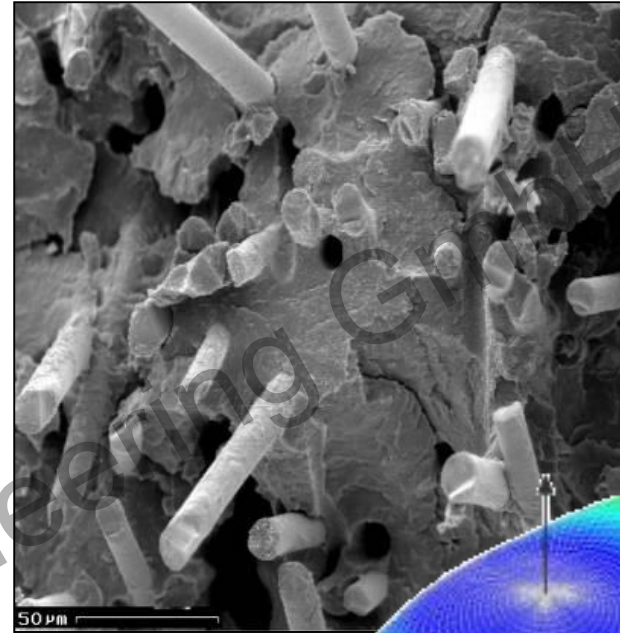


individual mapping
process information

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Short and long fiber reinforced thermoplastics

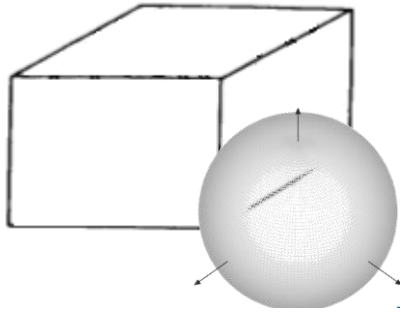
- Material model in LS DYNA
- Motivation
- Manufacturing influence
- Material model approaches
- Material characterization
- Casestudy - sleeve



© by 4a engineering GmbH

Motivation – current simulation standard

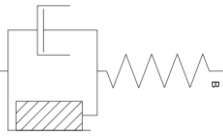
*MAT_024



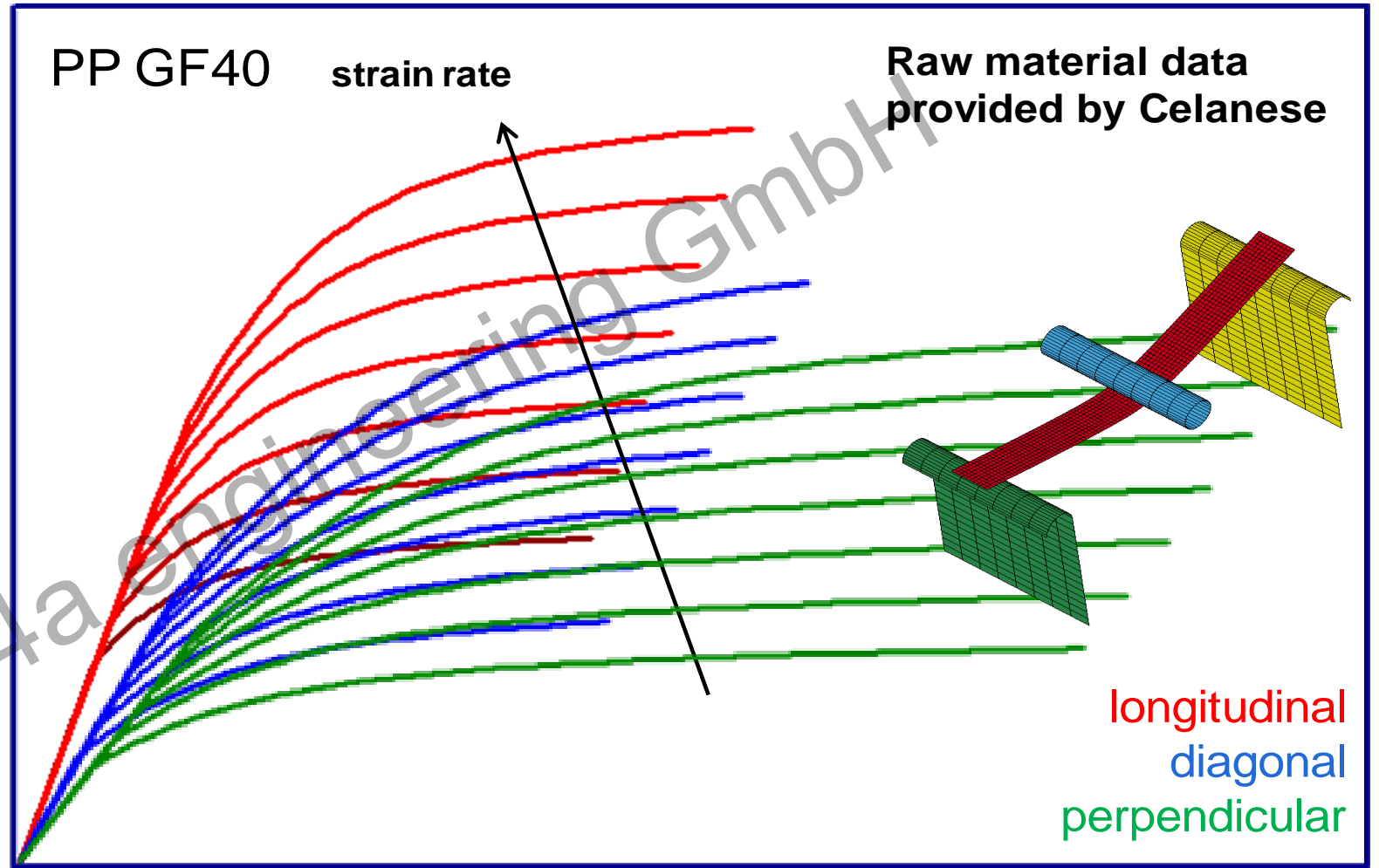
macro scale
constitutive law

Mises plasticity

- quick & dirty
- critical loading transversal to fiber orientation



stress

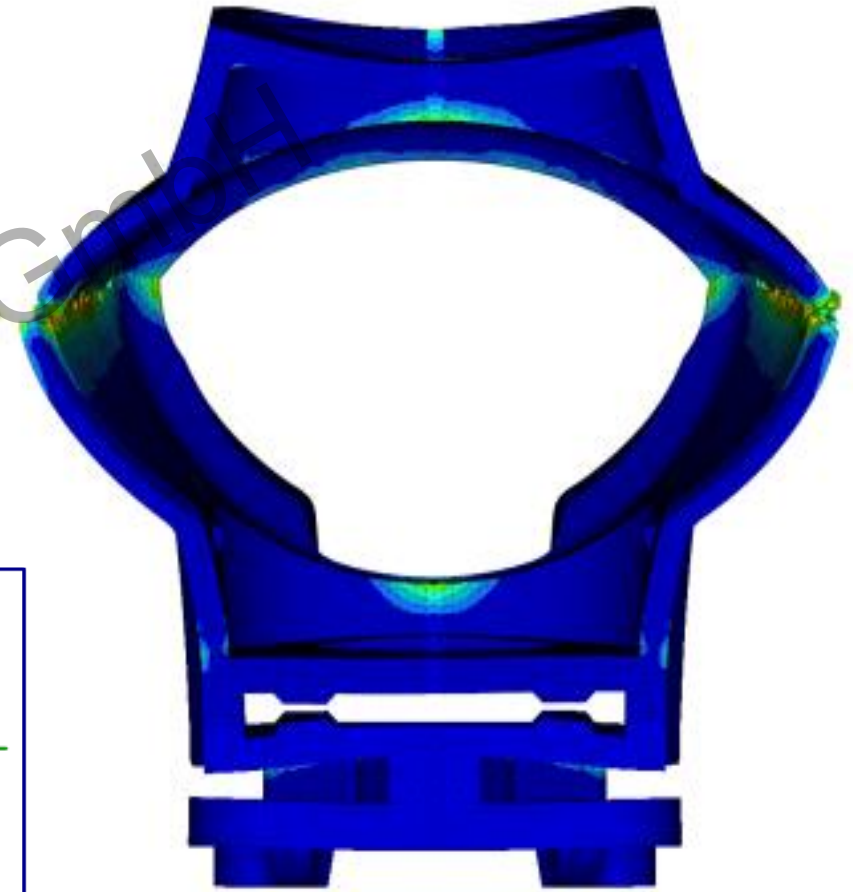
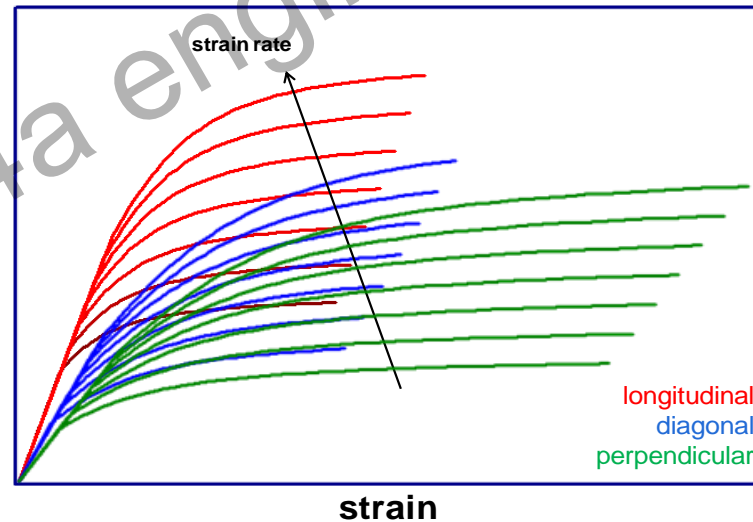


strain

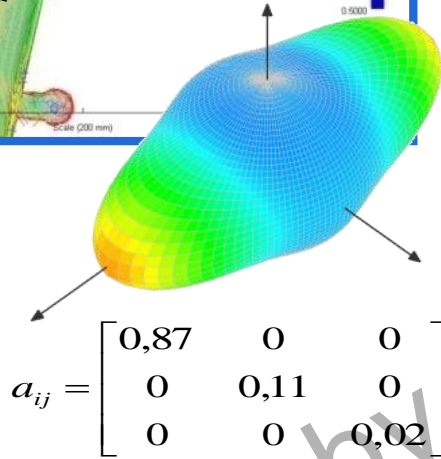
Motivation – current simulation standard



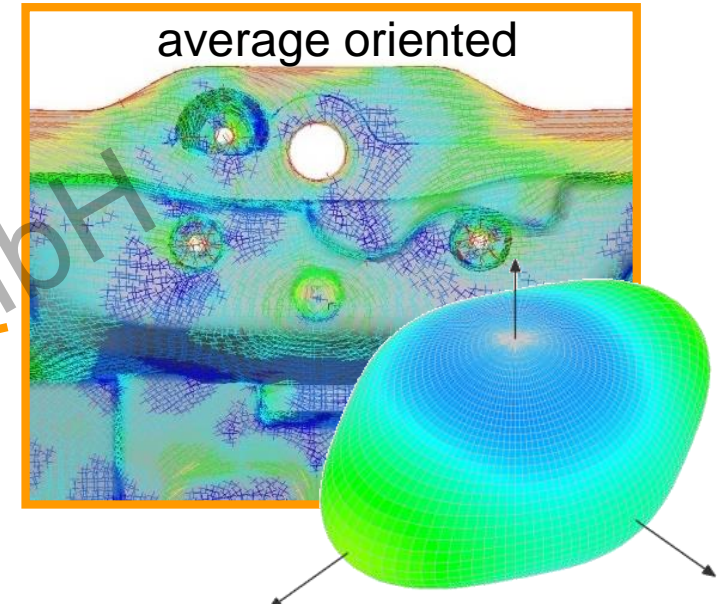
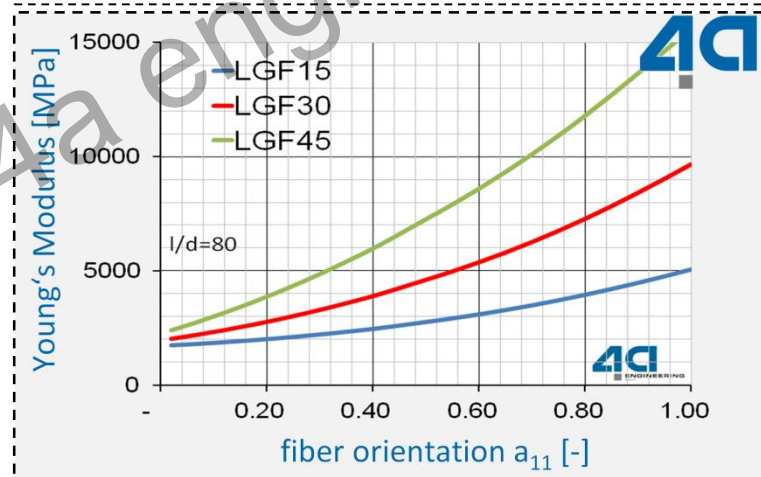
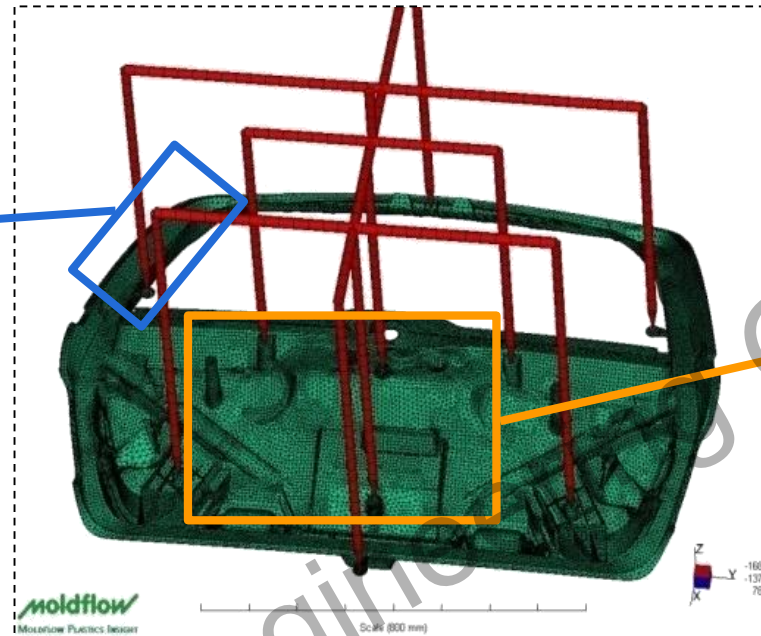
isotropic



Fiber orientation – development in typical part



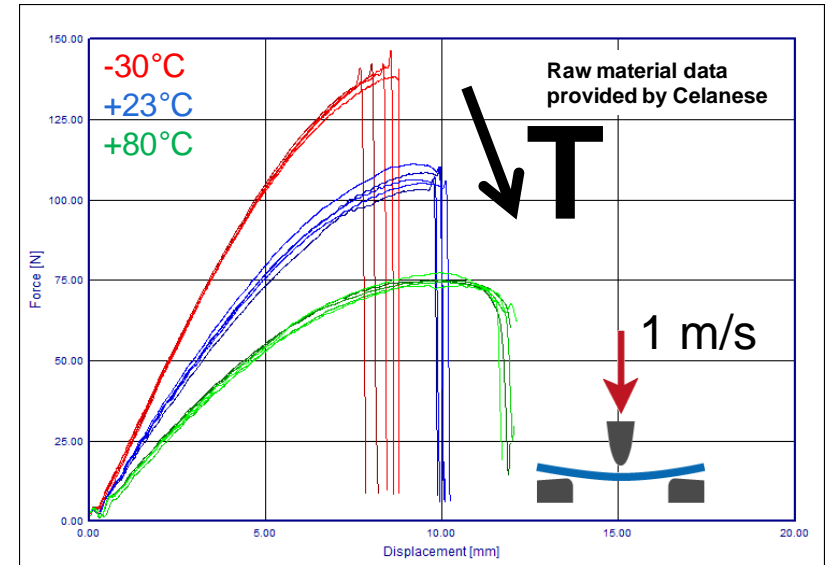
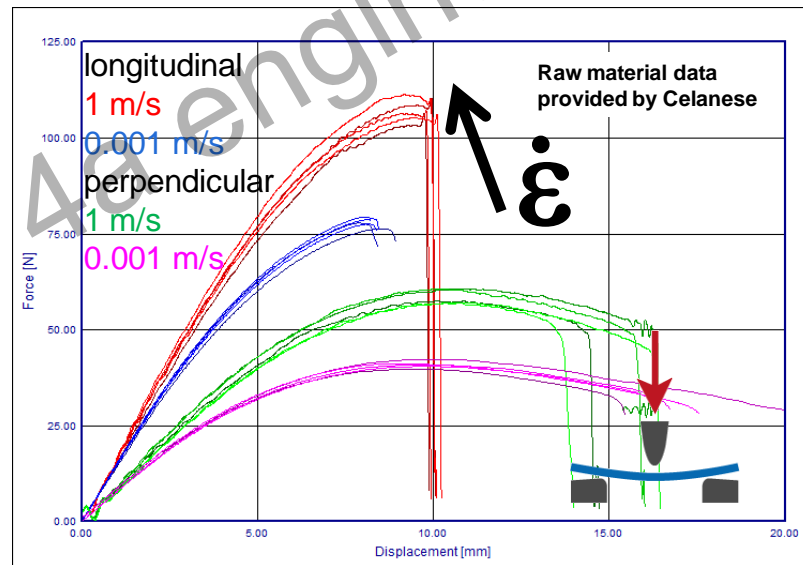
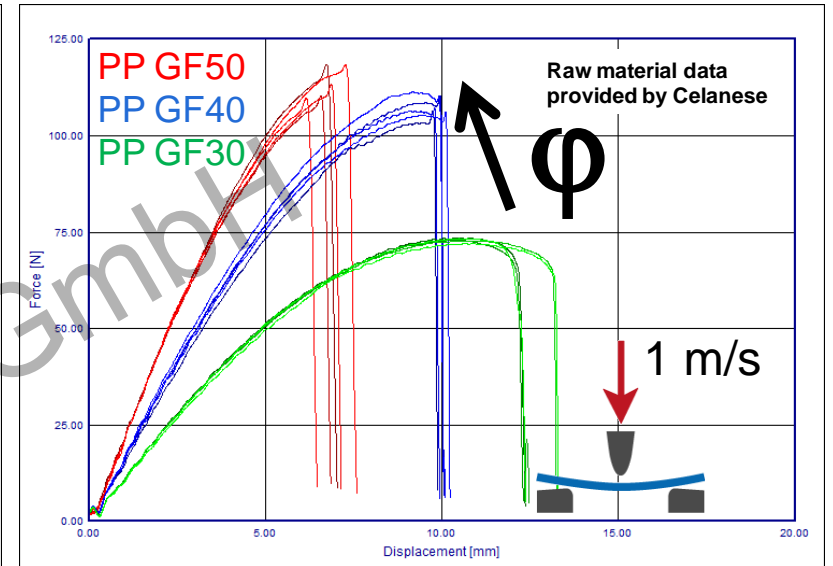
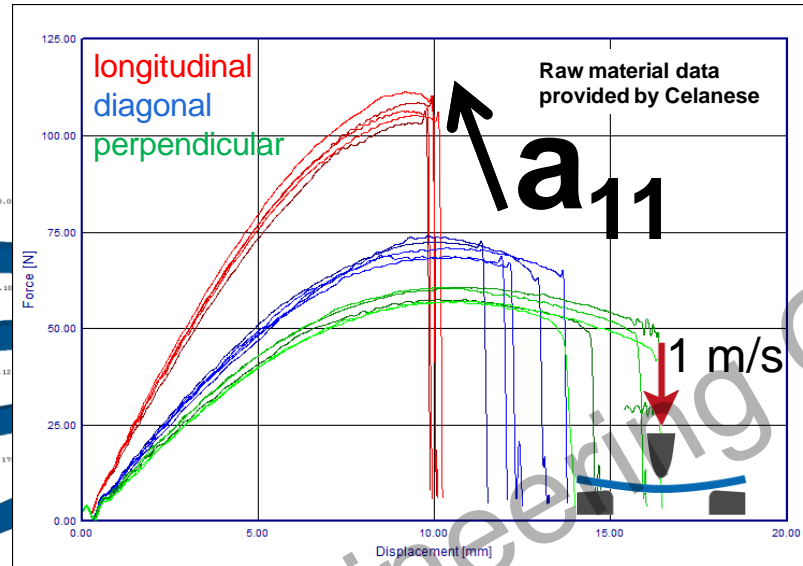
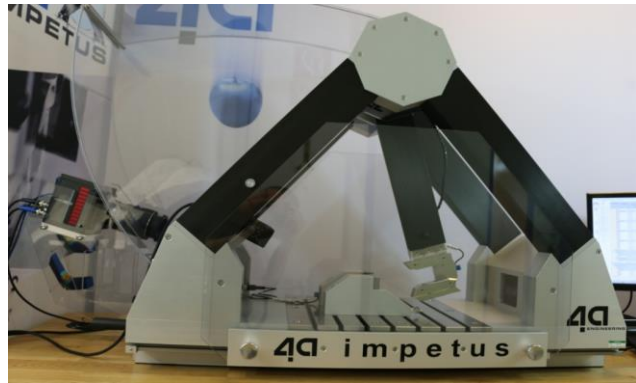
$$a_{ij} = \begin{bmatrix} 0,87 & 0 & 0 \\ 0 & 0,11 & 0 \\ 0 & 0 & 0,02 \end{bmatrix}$$



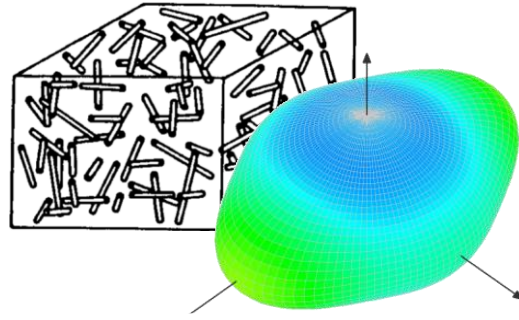
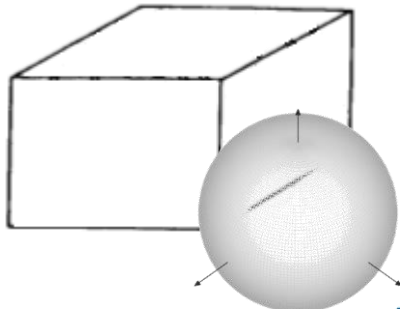
$$a_{ij} = \begin{bmatrix} 0,66 & 0 & 0 \\ 0 & 0,32 & 0 \\ 0 & 0 & 0,02 \end{bmatrix}$$

Source: P. Reithofer - Integrative Simulation – Berücksichtigung der prozessbedingten Anisotropie, 4a Technologietag 2011

Typical material behavior – SFRT / LFRT



Typical material models in LS-DYNA



Hill plasticity → „extended“ von Mises

$$\sigma_{eq} = \sqrt{F(\sigma_{22} - \sigma_{33})^2 + G(\sigma_{33} - \sigma_{11})^2 + H(\sigma_{11} - \sigma_{22})^2 + \dots}$$

macro scale

constitutive law

→ composite

Mises plasticity

- quick & d
- crit
- orientation

**MAT = 024*

elastic

- orthotro
- anis
- elastic
- city

**MAT = 157*

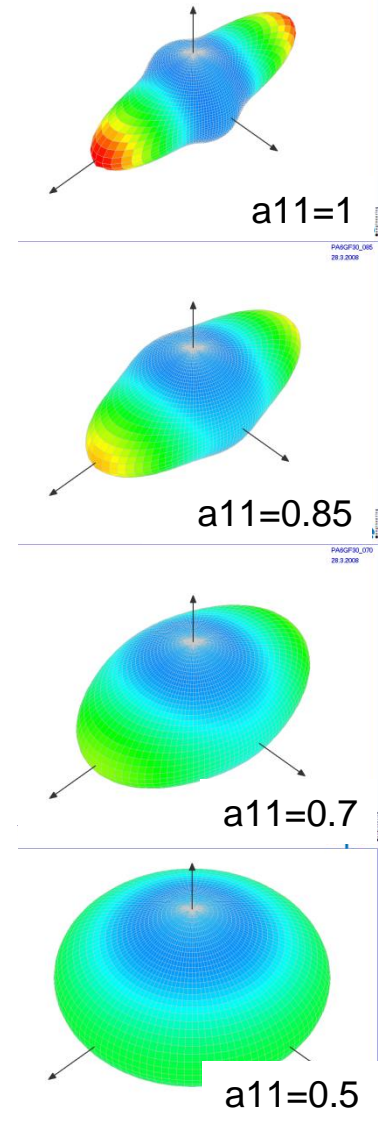
α – orientation dependent

material models in LS DYNA – short and long fiber reinforced thermoplastics

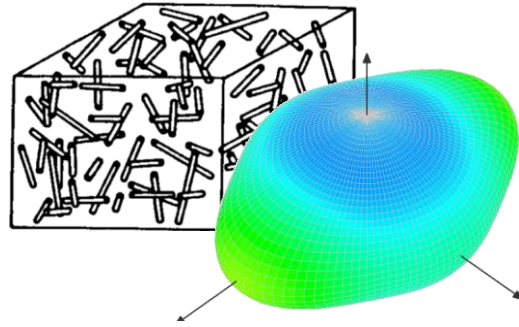
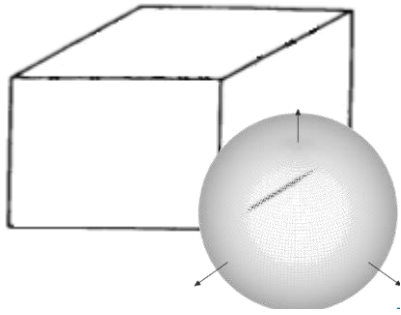
description	variables	Number of variables	dependencies
anisotropic stiffness	Cij	21	$C_{ij}(a_{ij}, \varphi, C^M, C^F)$
Hill plasticity	3D: F, G, H, L, M, N 2D: r00, r45, r90	6	$f(a_{ij}, \varphi, \sigma^M, \sigma^F)$
stress-strain curve	Loadcurve	3	$f(a_{ij}, \varphi)$
failure	Loadcurve	6	$f(a_{ij}, \varphi)$

- Not possible to generate samples with **explicit defined and varying a_{ij}**
- Hard to characterize, too many possibilities in a_{ij}

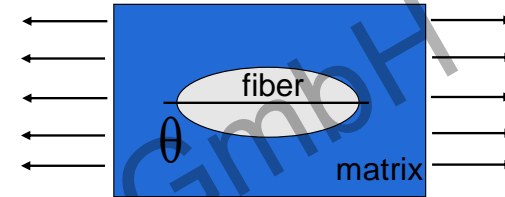
→ Micro mechanical model is needed



Typical material models in LS-DYNA



$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$



Eshelby Tensor

macro scale

constitutive law

Mises plasticity

- quick & d...
- critic...
- orientation

***MAT = 024**

→ composition

elastic

- orthotro...
- anisotro...
- elastic...
- plasticity

***MAT = 157**

α – orientation dependent

micro scale

homogenization

M... matrix

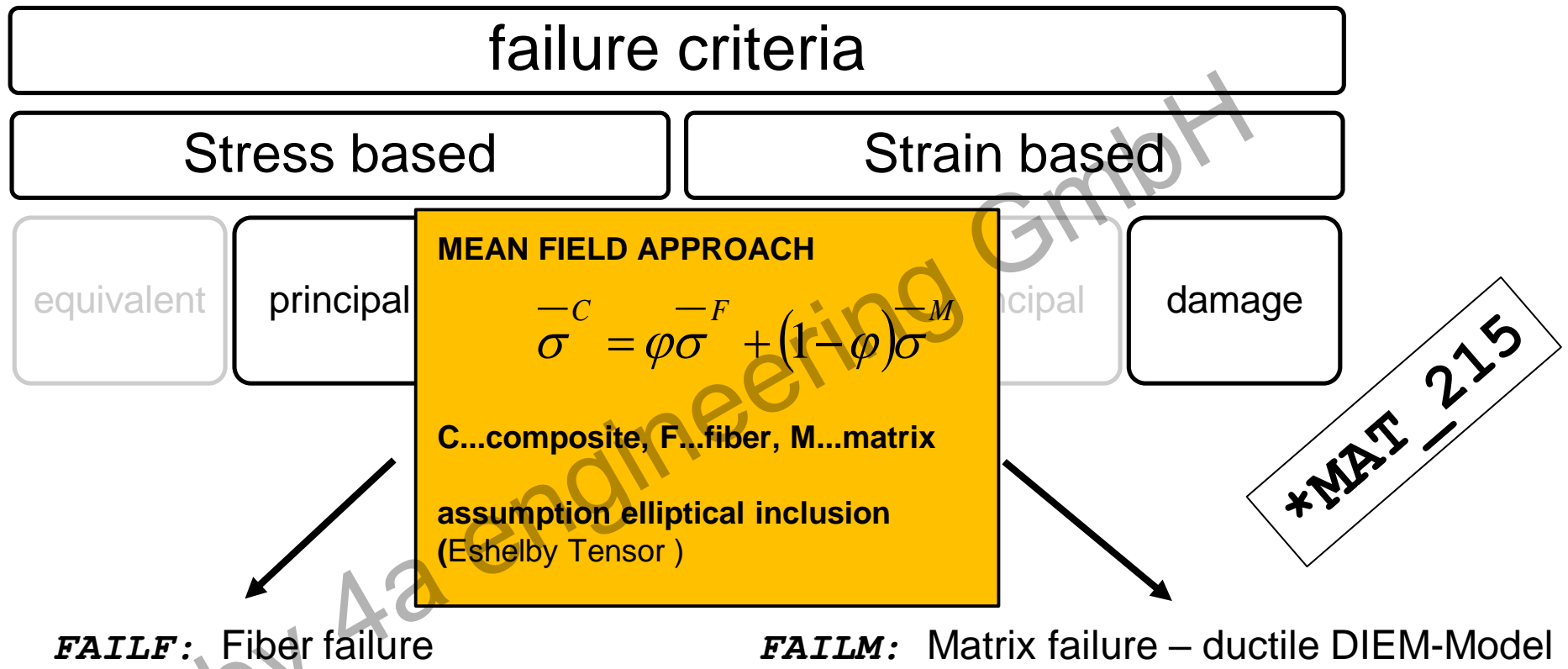
- isotropic elas...
- viscoplasti...

F... fiber

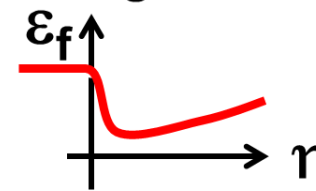
- isotropic...

***MAT = 215**

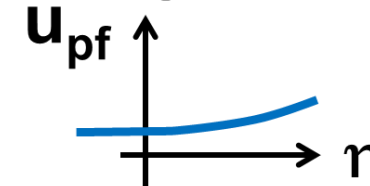
Micro mechanical motivated failure



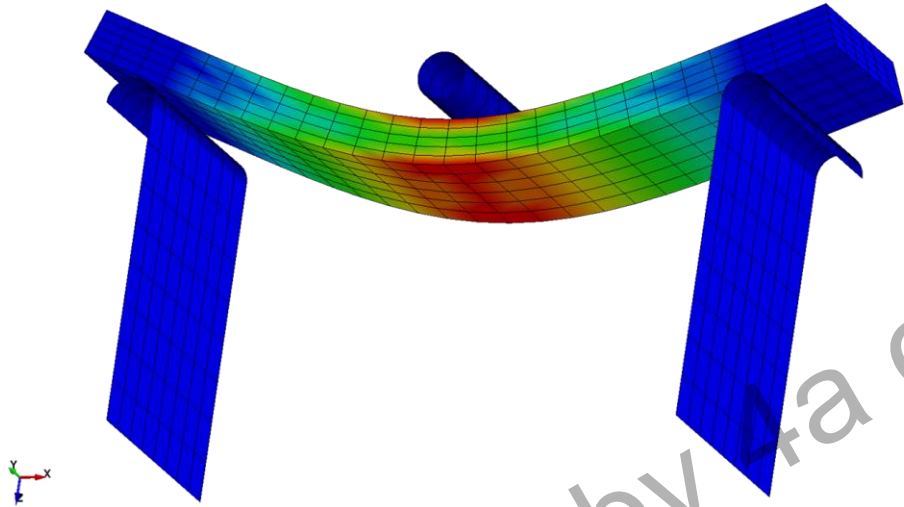
Damage Initiation



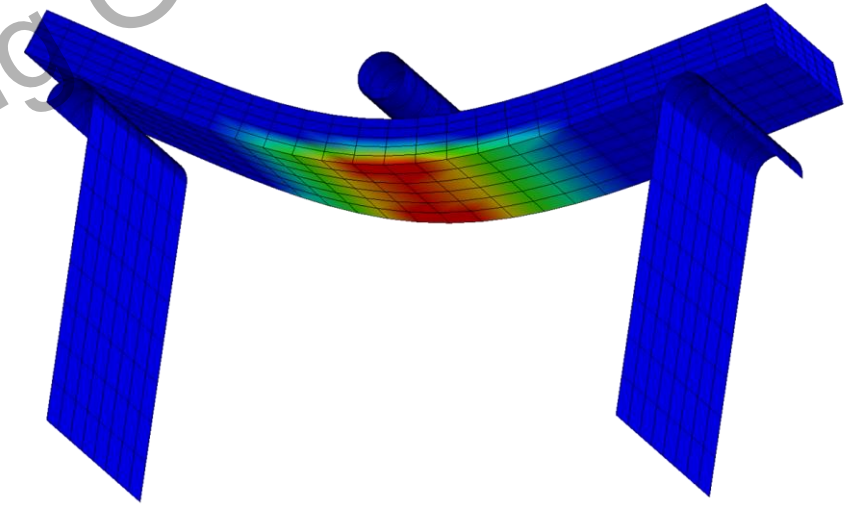
Damage Evolution



Micro mechanical motivated failure



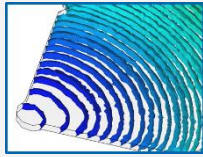
*History#6 (step8: 0-0.13):
Fiber damage init.*



*History#4 (step8: 0-0.81):
dm - matrix damage init.*

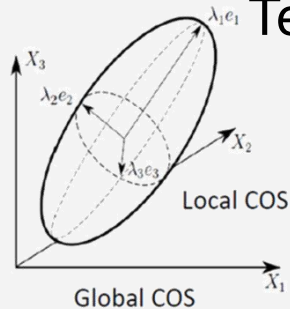
Material models – present approaches

Process simulation

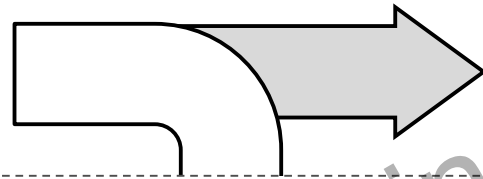


$$a_{ij} = \begin{bmatrix} a_{xx} & a_{xy} & a_{xz} \\ & a_{yy} & a_{yz} \\ & & a_{zz} \end{bmatrix}$$

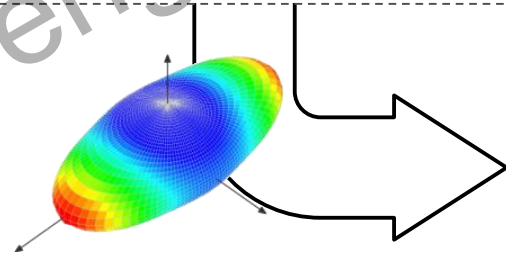
Tensor 2nd order



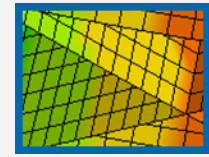
MOLDFLOW



$$C^{-1} = \begin{bmatrix} \frac{1}{E_1} & -\frac{\nu_{21}}{E_2} & -\frac{\nu_{31}}{E_3} & 0 & 0 & 0 \\ -\frac{\nu_{12}}{E_1} & \frac{1}{E_2} & -\frac{\nu_{32}}{E_3} & 0 & 0 & 0 \\ -\frac{\nu_{13}}{E_1} & -\frac{\nu_{23}}{E_2} & \frac{1}{E_3} & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1}{G_{23}} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{G_{31}} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1}{G_{21}} \end{bmatrix}$$



Structural simulation

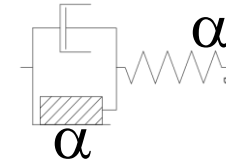


Homogenization (Micro Scale)
Mean Field Theory

$$\bar{\sigma}^C = \phi \bar{\sigma}^F + (1 - \phi) \bar{\sigma}^M$$

*MAT_215

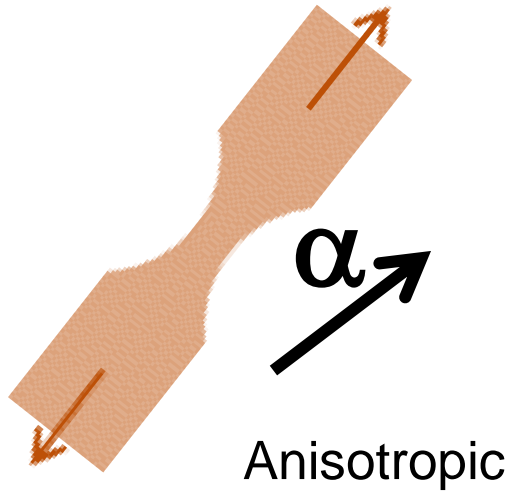
Composite (Macro Scale)
Hill Plasticity



*MAT_157



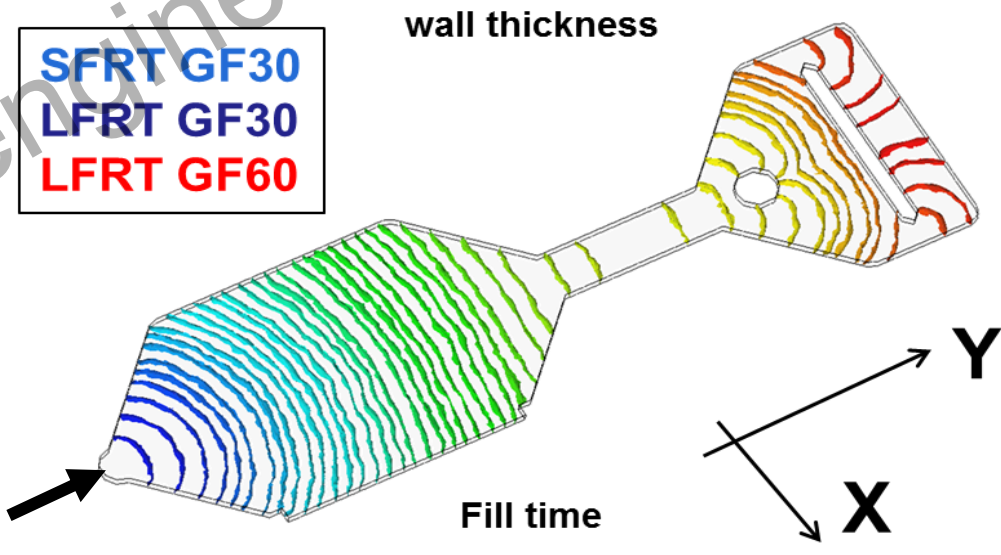
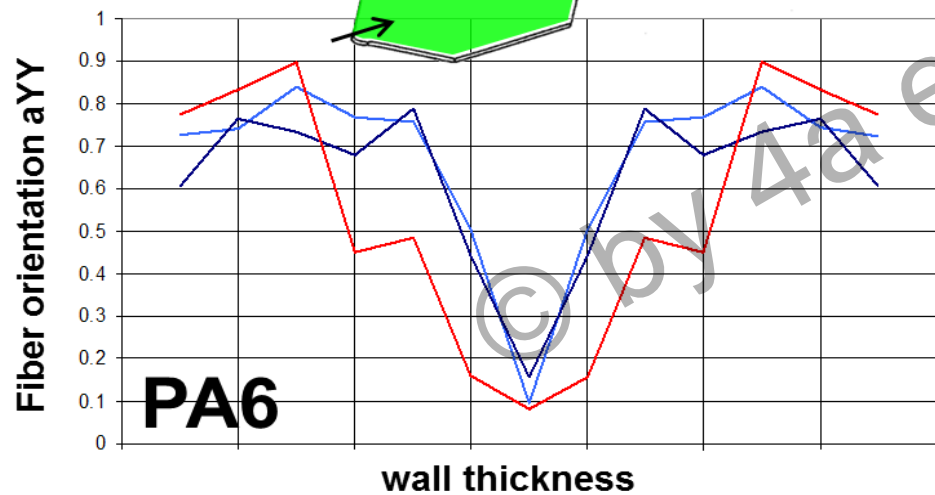
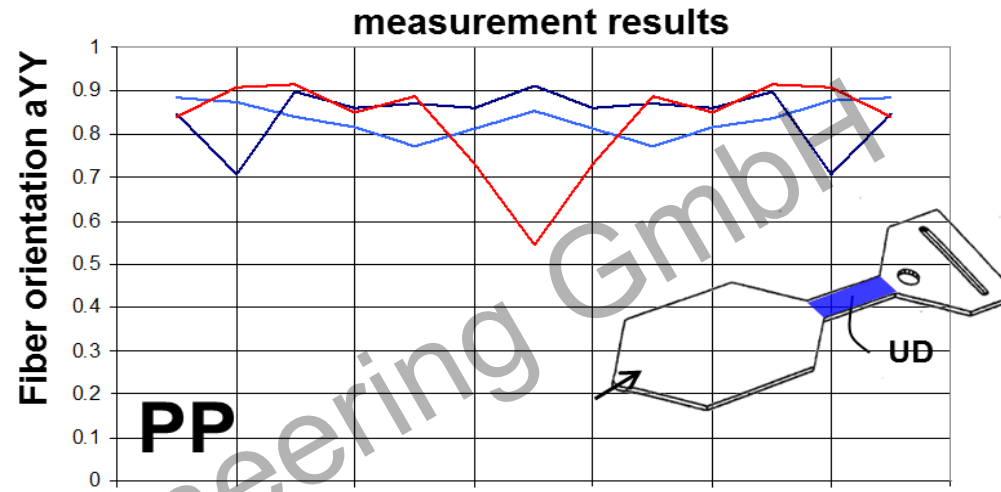
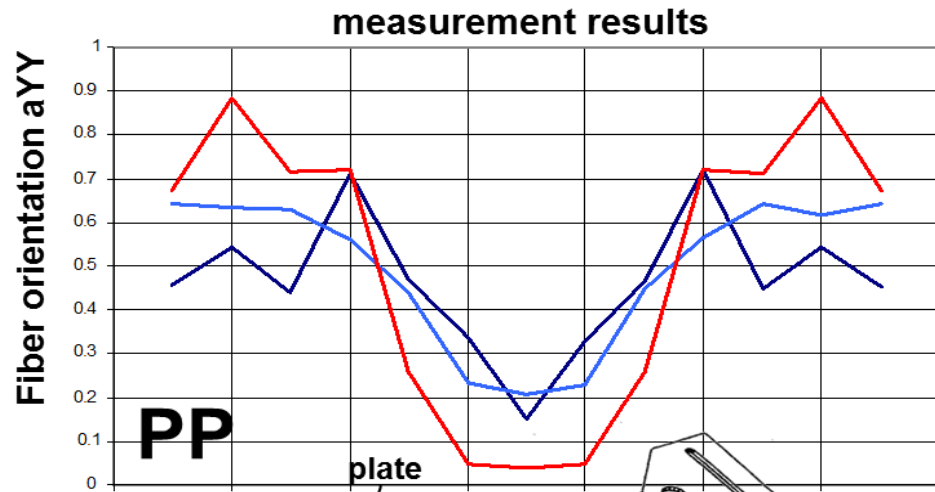
From test to material card



Why not tension (only)?

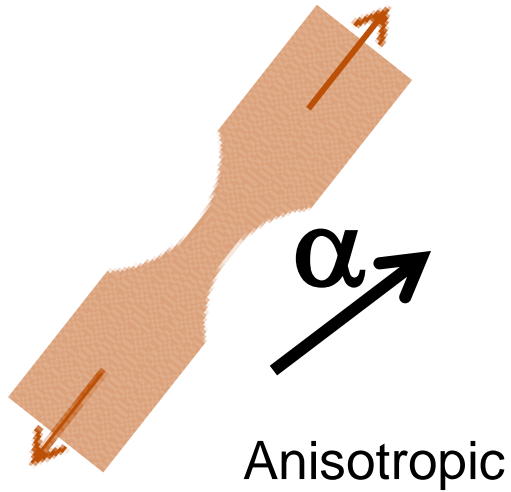
© by 4a engineering GmbH

Fiber orientation – development based on flow / viscosity

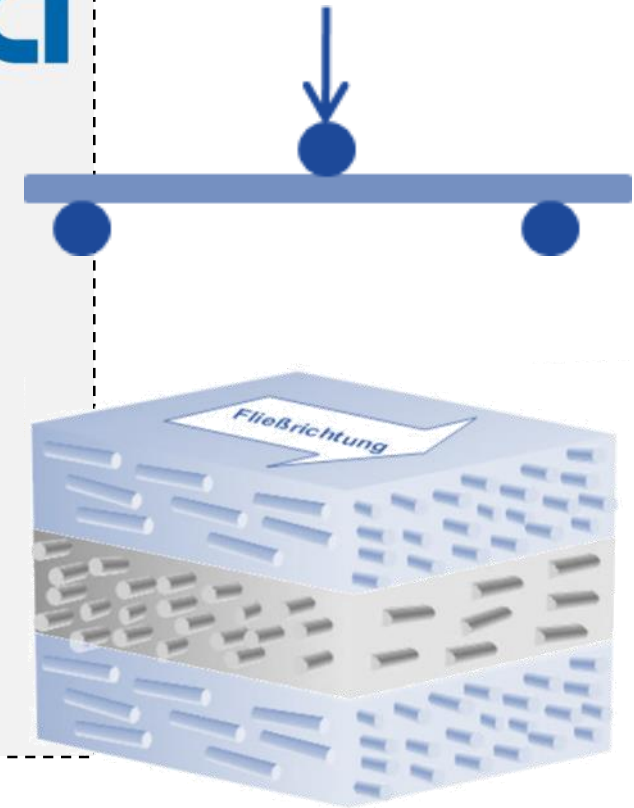
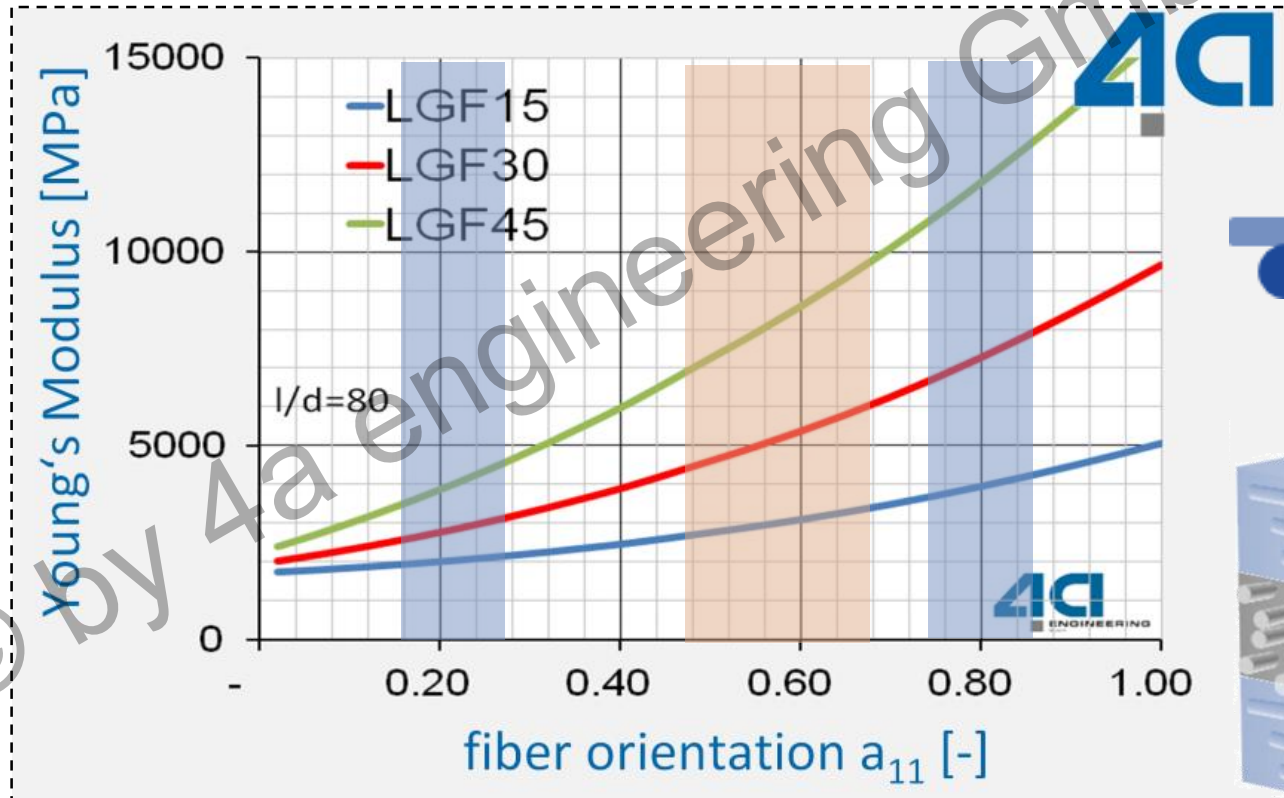


Source: 4a – EU Nelofite project , 2005

From test to material card

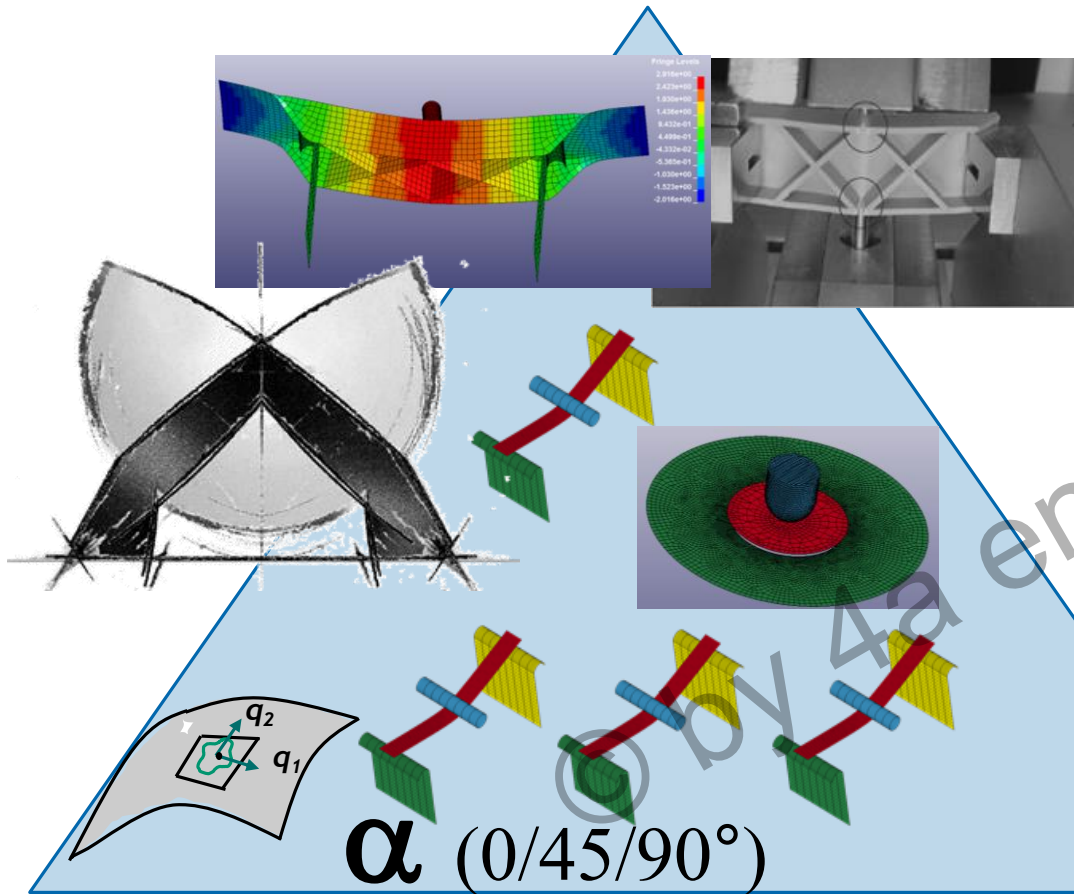


Why not tension (only)?

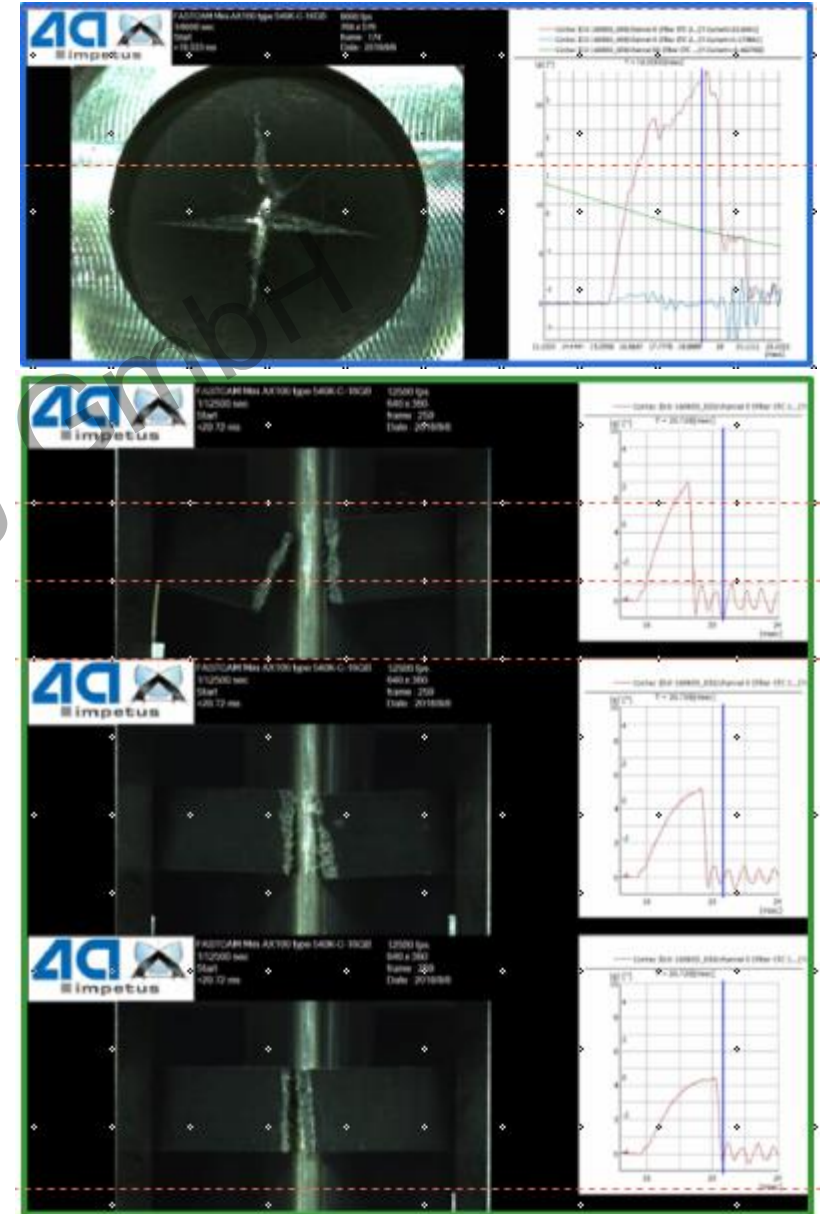
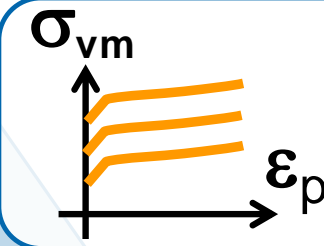
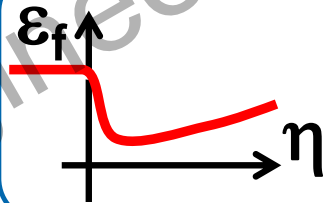


Pflamm-Jonas 2001

From test to material card



component validation



Source: P Reithofer, et.al., failure criteria SFRT and LFRT,

How to get *MAT_215 ?



fiber

- mechanical properties
- fiber content
- aspect ratio
- fiber orientation

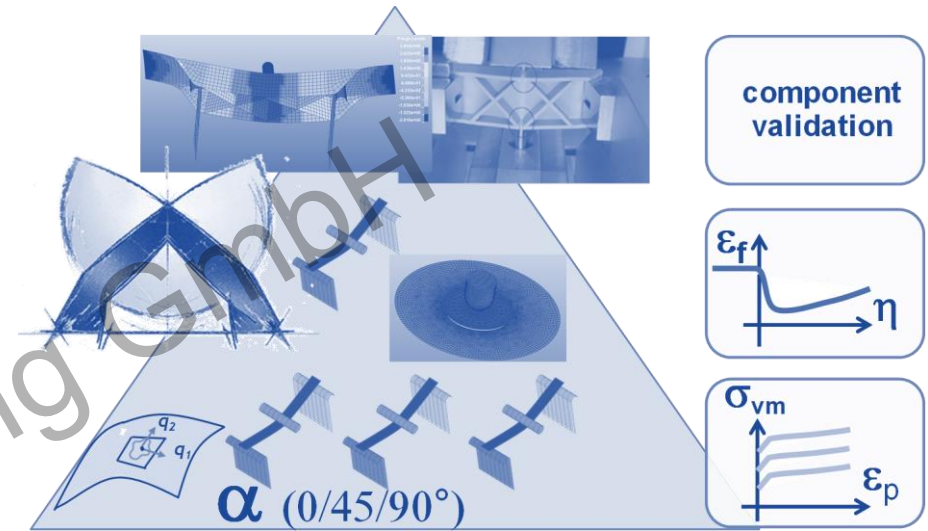
literature
engineering
judgement

tests (μ CT, ...)

matrix

- pseudo mechanical properties
 - yield
 - hardening
 - failure

REVERSE ENG.



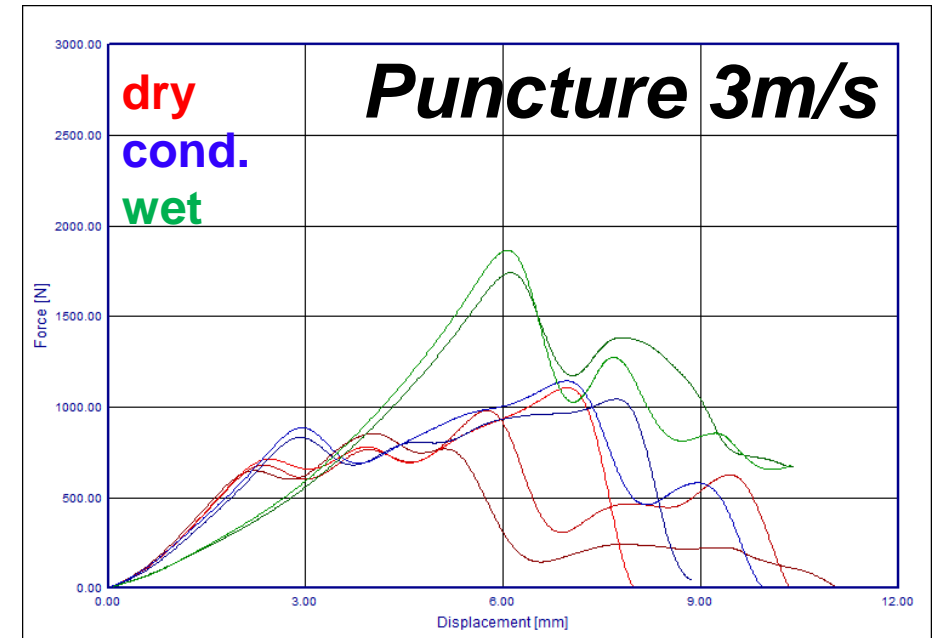
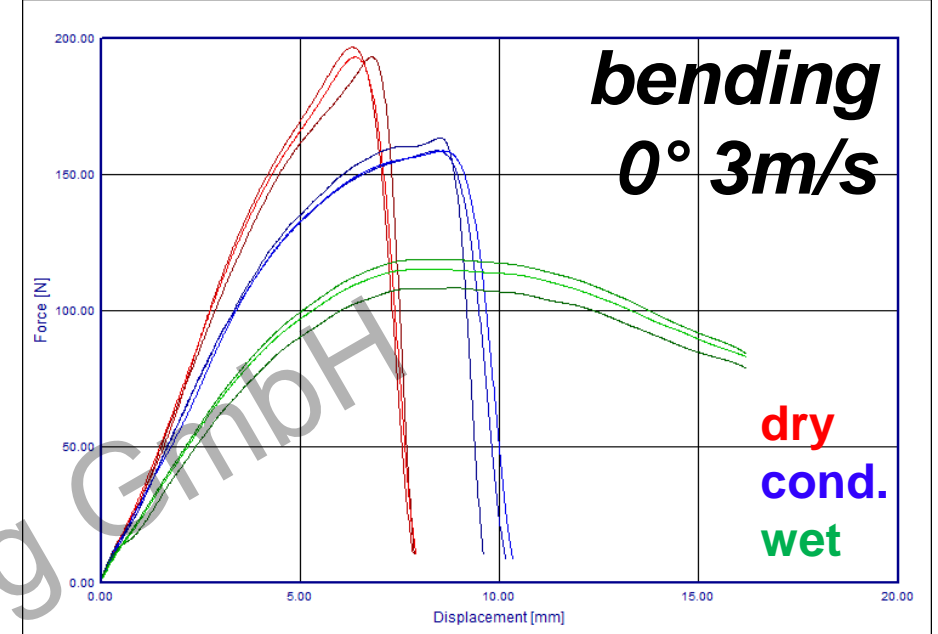
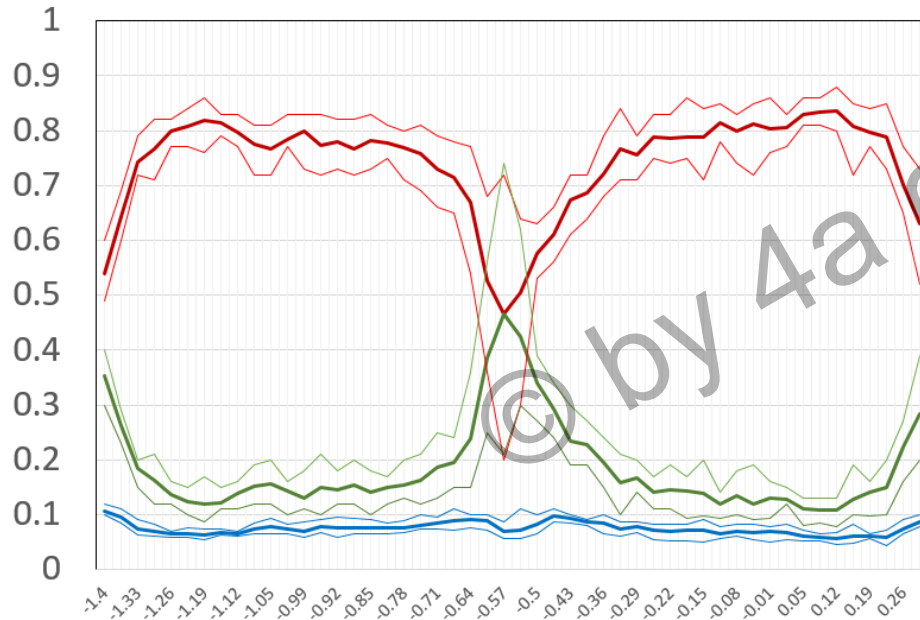
tests

- bending and/or tensile
 - testing in different directions
0°, 30° (45°), 90° sample orientation
- uniaxial and biaxial
- static and dynamic

How to get *MAT_215 – case study PA6 GF30 I

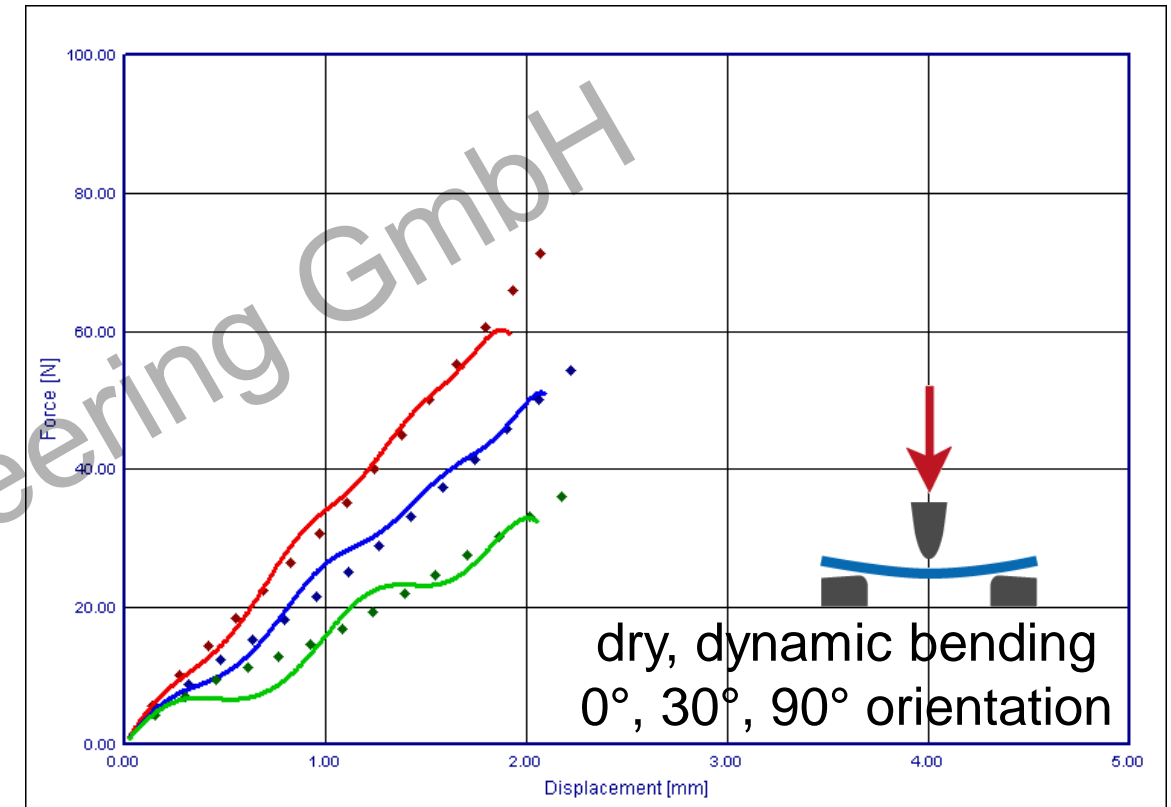
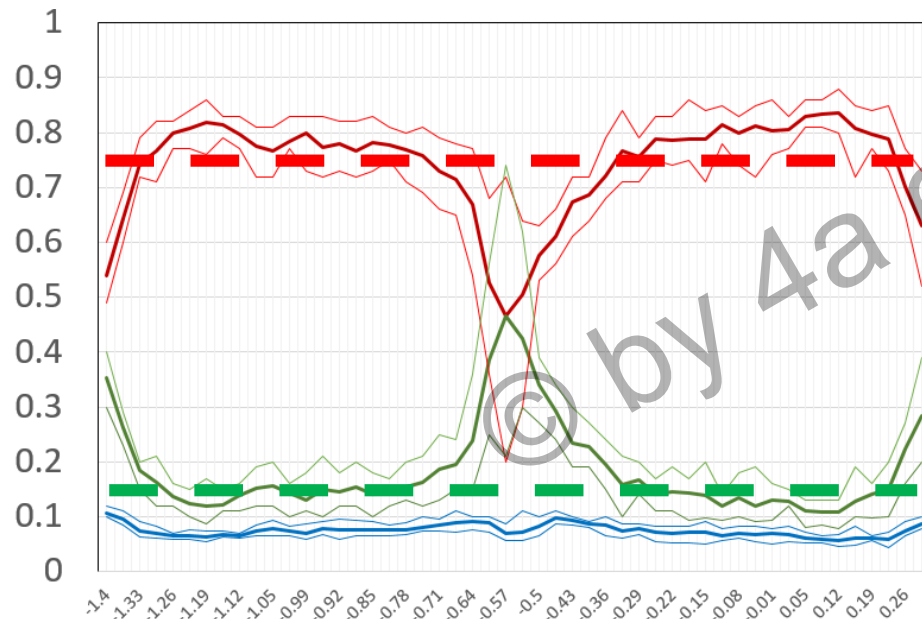
Provided by consortium (PCCL, HILTI, Hirtenberger)

- plaques for puncture tests
- bending samples (0°, ~30°, 90°)
- different moisture contents (dry, cond., wet)
- μ CT measurements



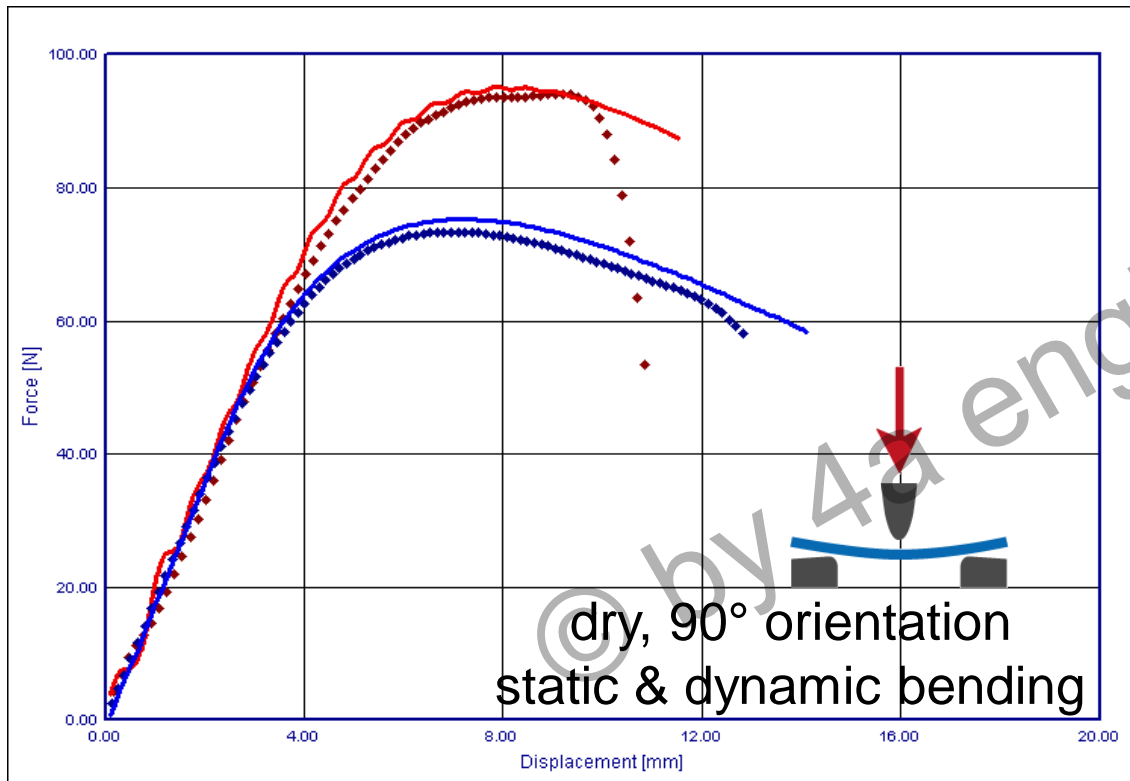
1st step: set up the composite

- Fiber properties from literature
- Fiber content 30%wt → **-0,3**
- Aspect ratio typical for short fibers $l/d=20$
- μ CT measurements → average



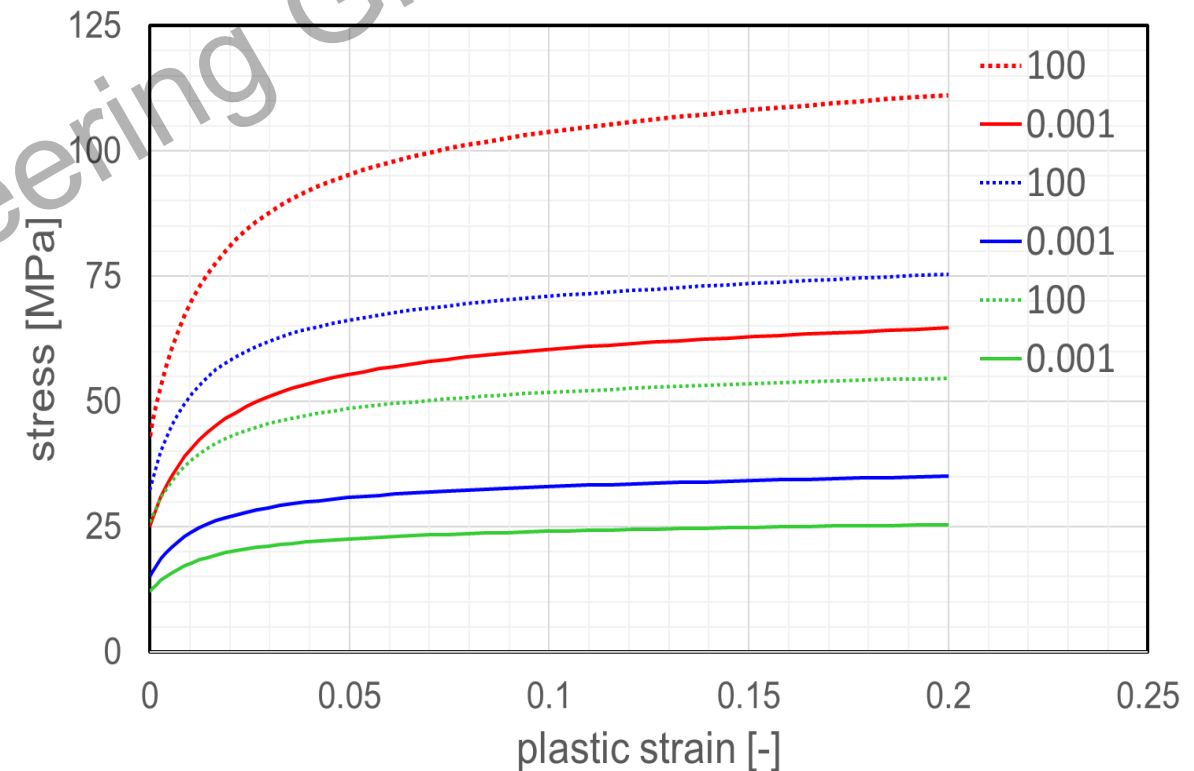
2nd step: matrix hardening

- parameter identification of hardening law



Matrix in dependence of moisture

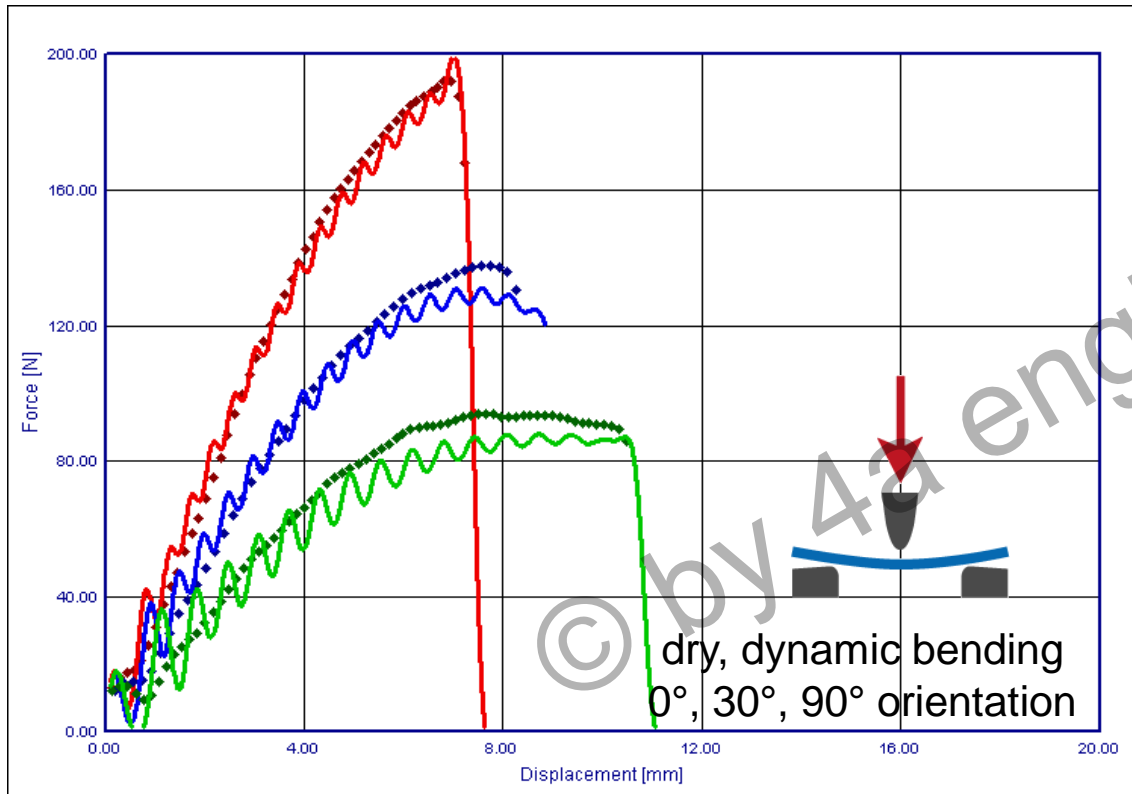
Young's Mod. [MPa]	dry	cond.	wet
	2500	1600	1450



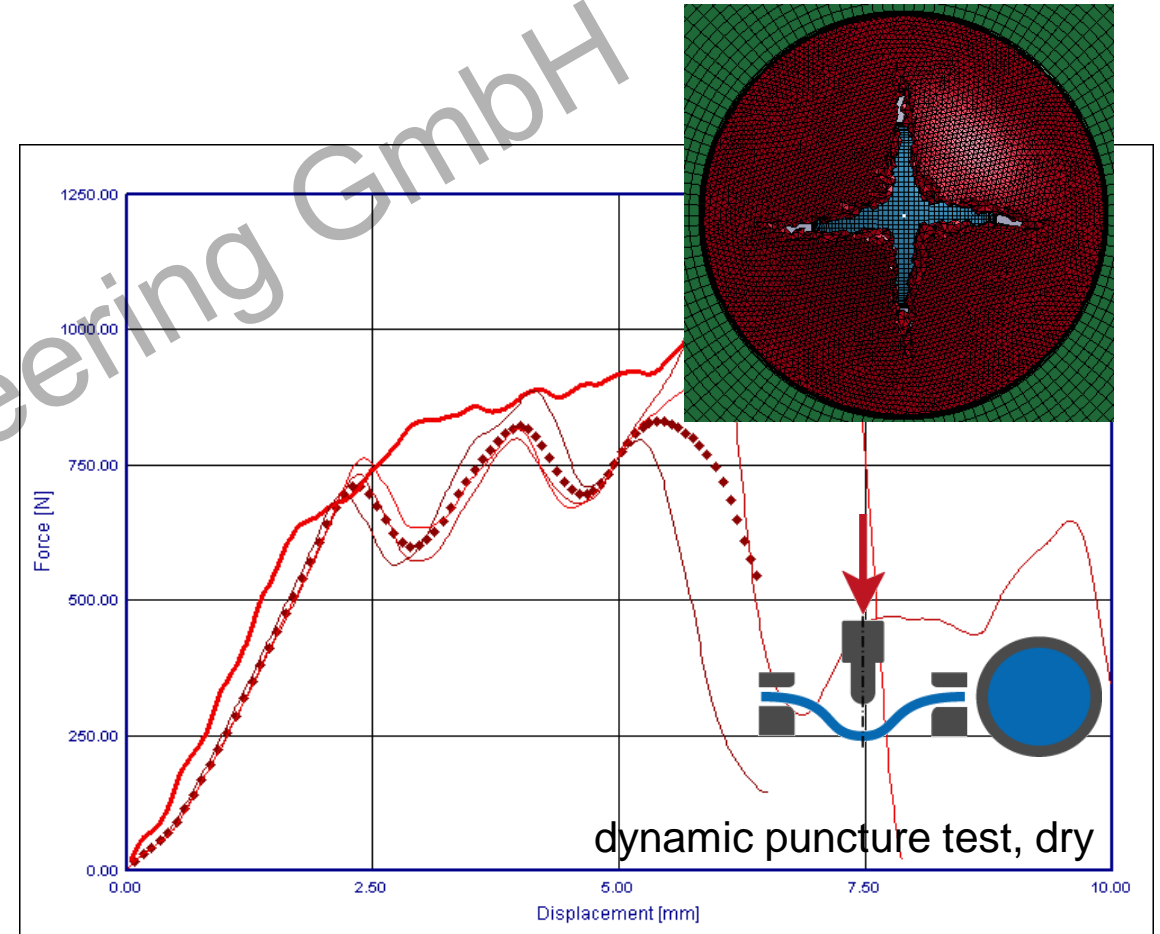
How to get *MAT_215 – case study PA6 GF30 I

3rd step: validation on dynamic bending

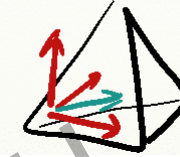
4th step: failure strains



5th step: validation on dynamic puncture

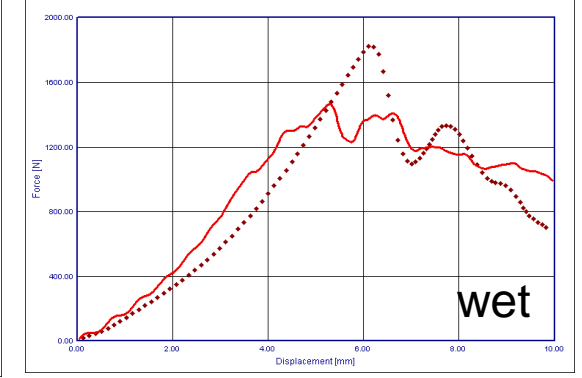
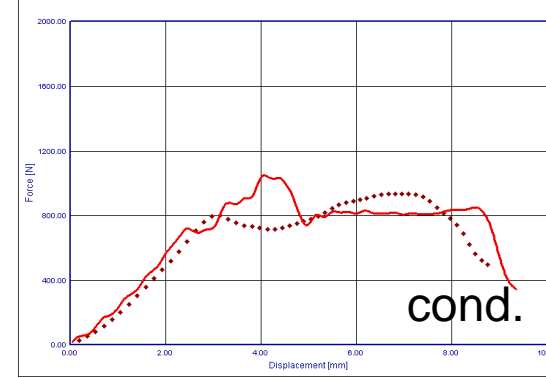
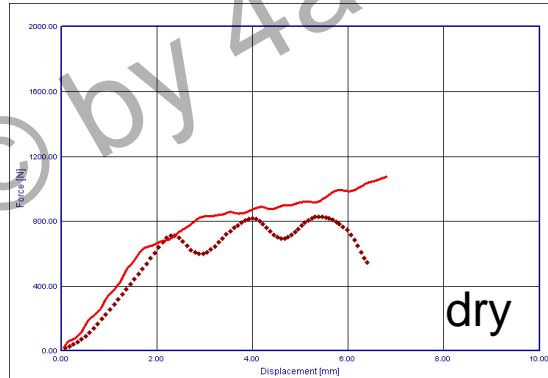
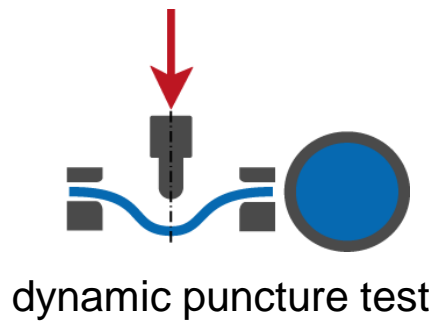
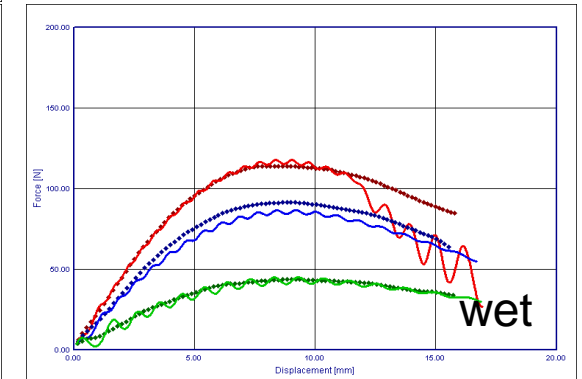
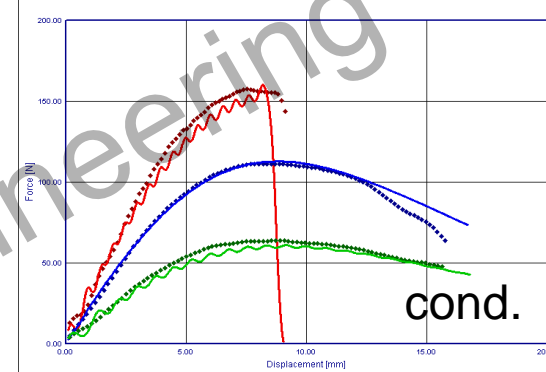
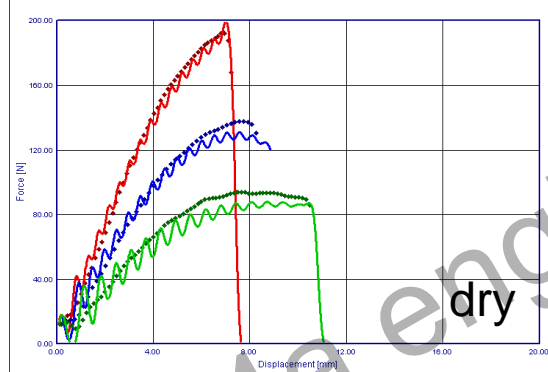
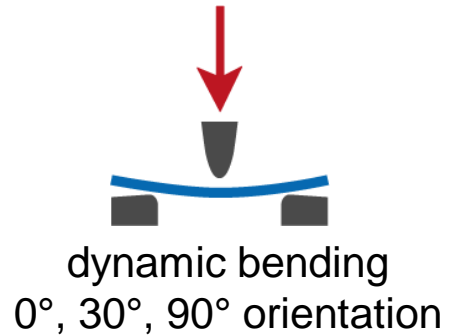
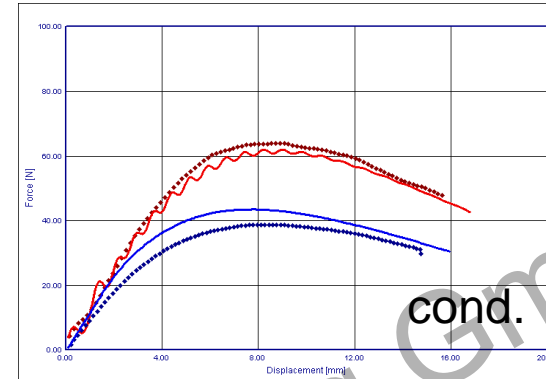
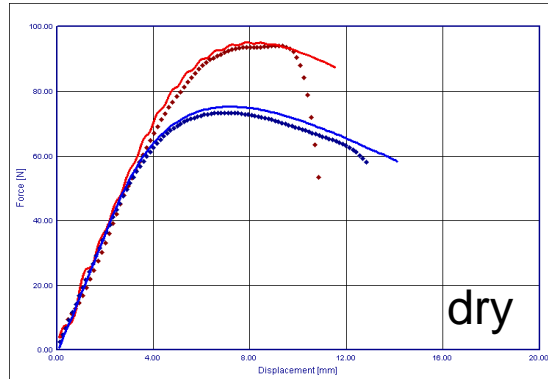
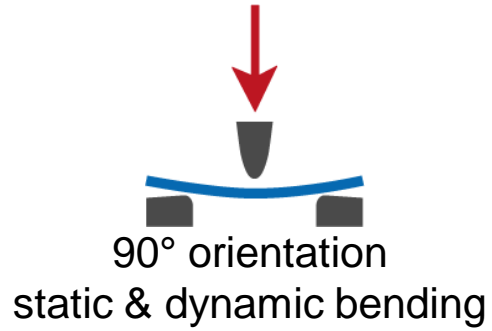


Second material - PA6 GF30 different moisture contents



ELTYP4
0.5 mm

..... averaged test curves
— result of simulation



Source: P Reithofer, et.al., failure criteria SFRT and LFRT

injection mold for material characterization

DOM & Wall thickness



Melt- & Weldlines

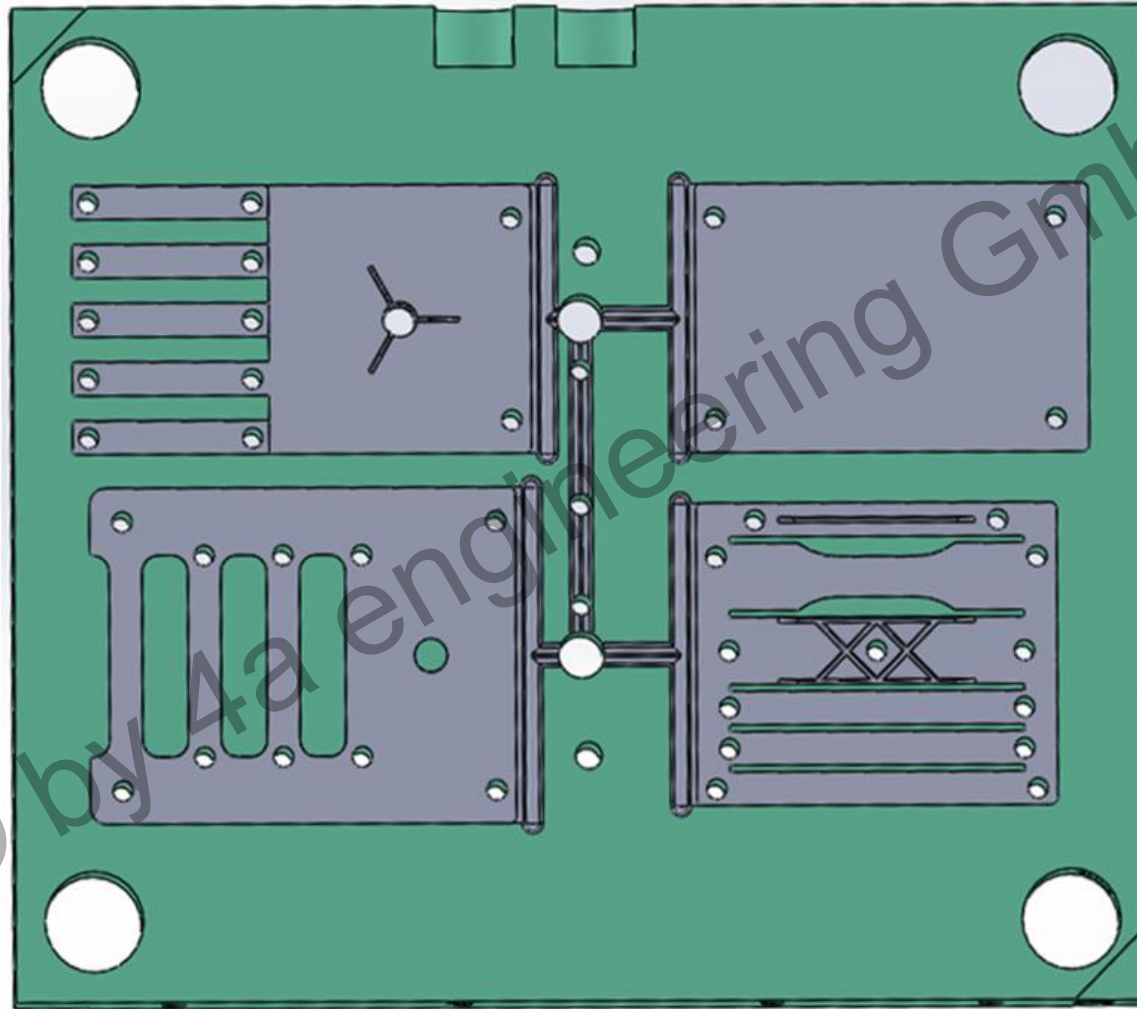


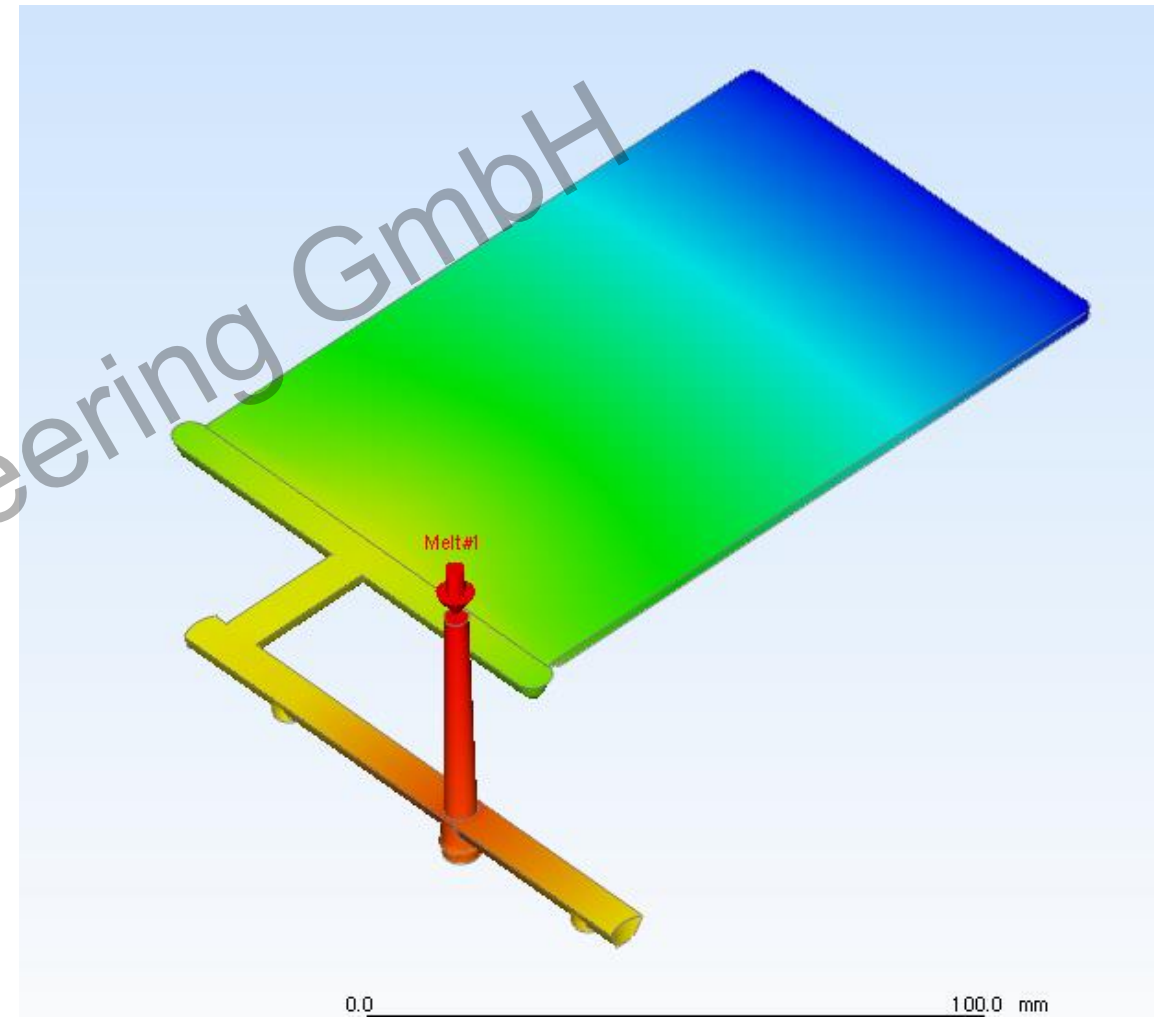
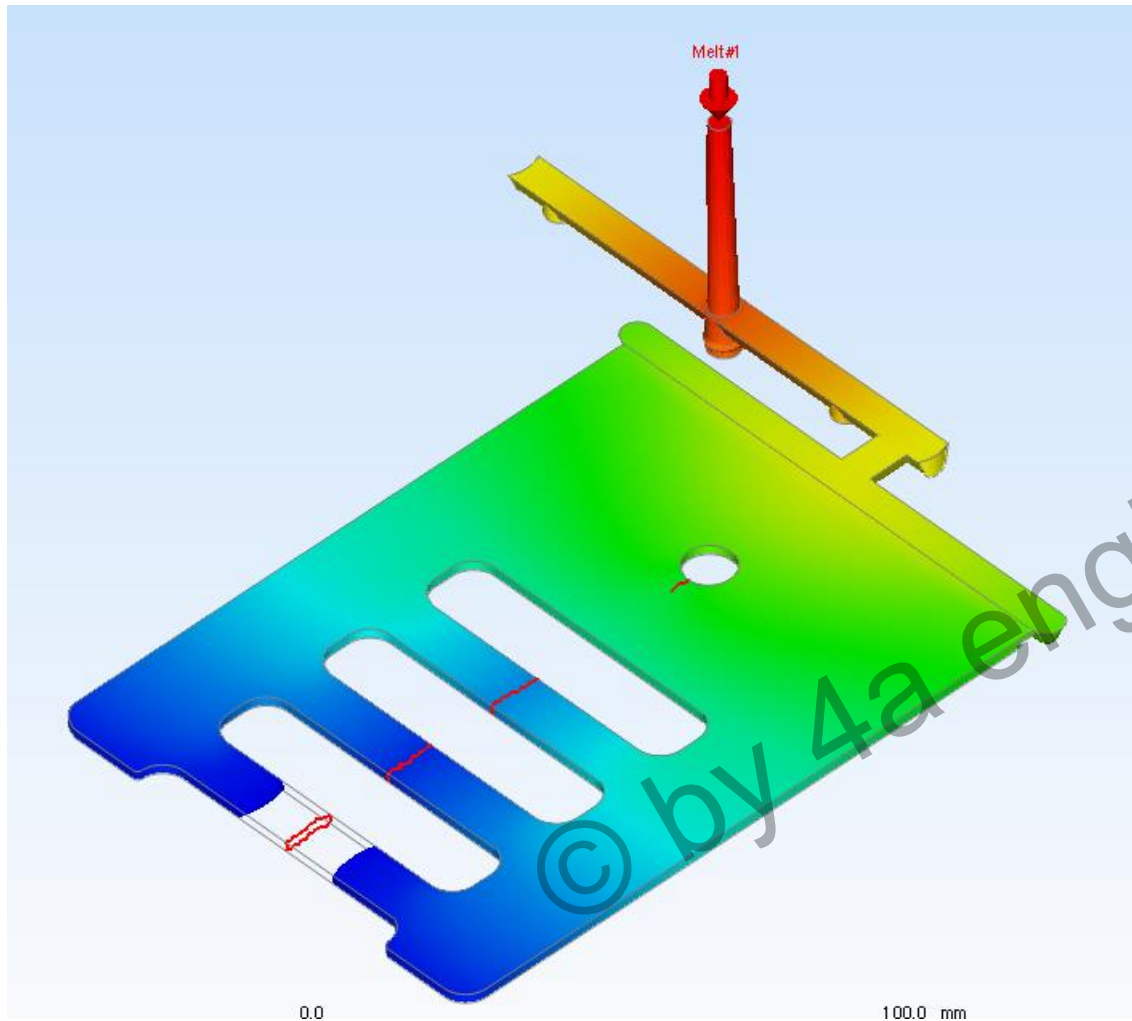
Plate 120 x 80 x 2 mm



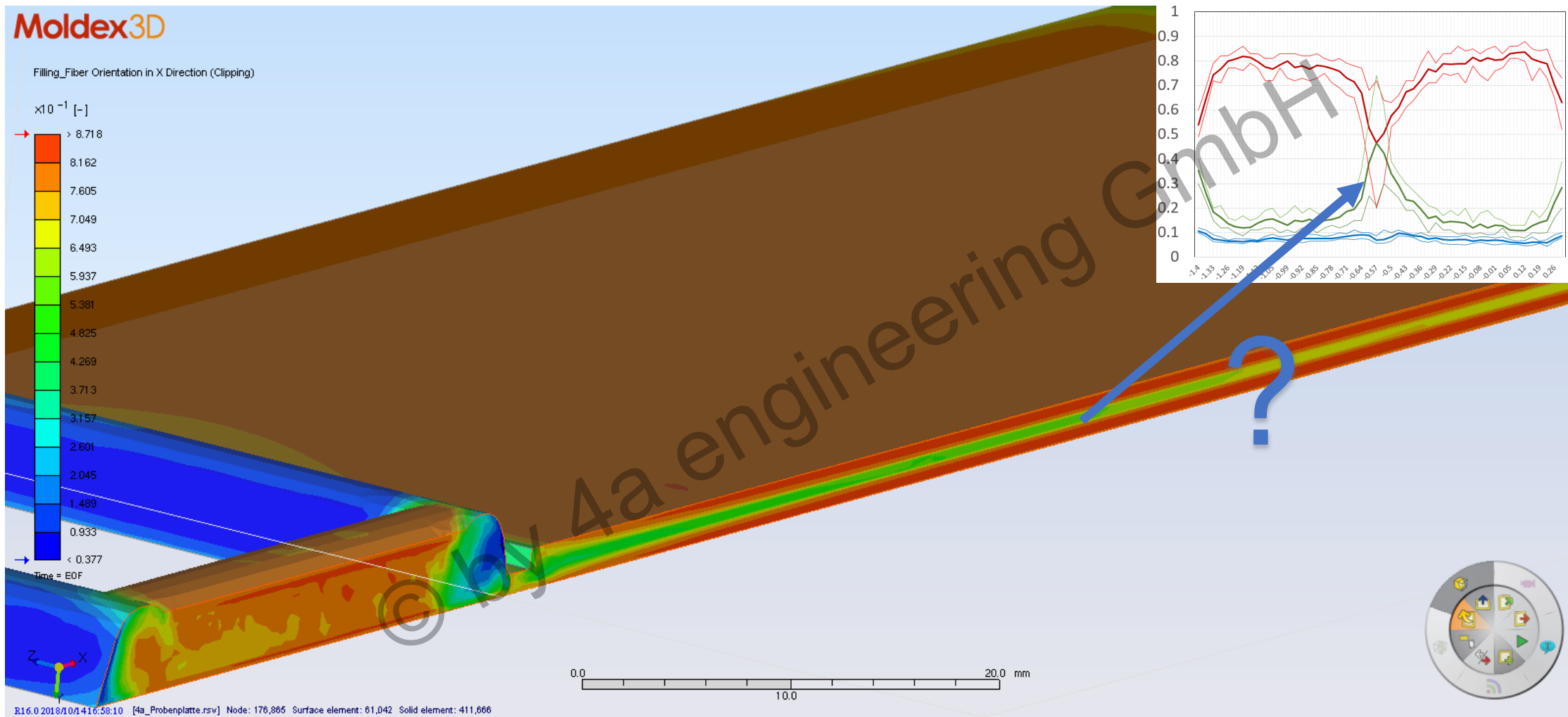
Multi-Specimen & Rib & Component



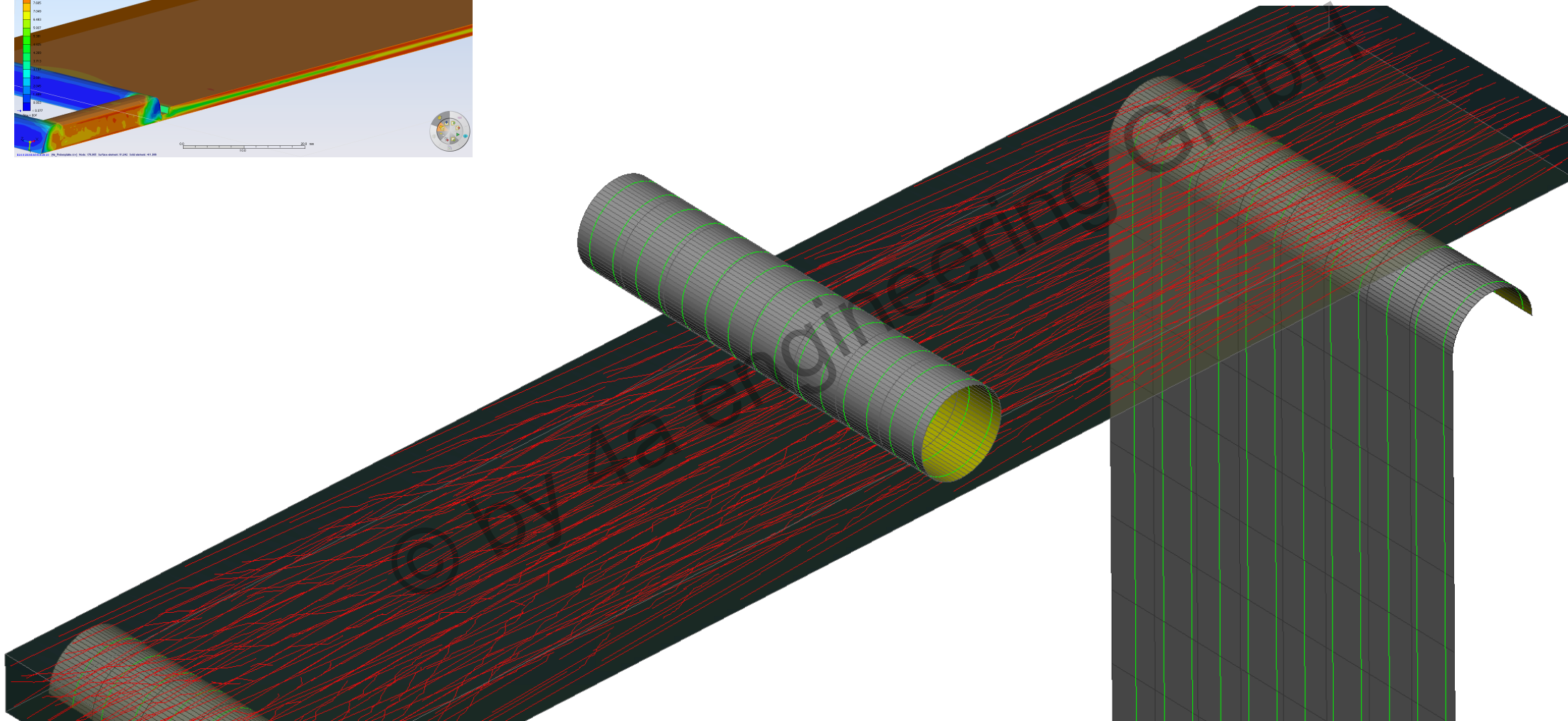
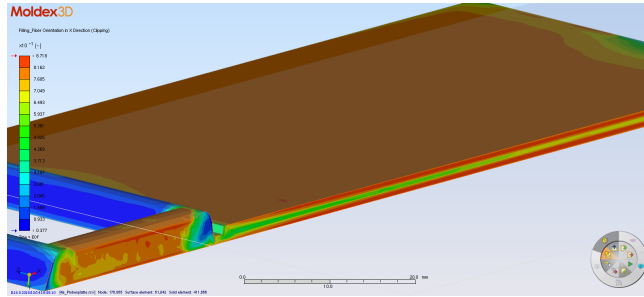
injection mold – process simulation

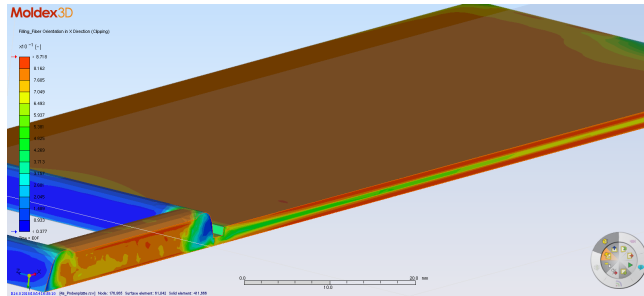


injection mold – process simulation fiber orientation

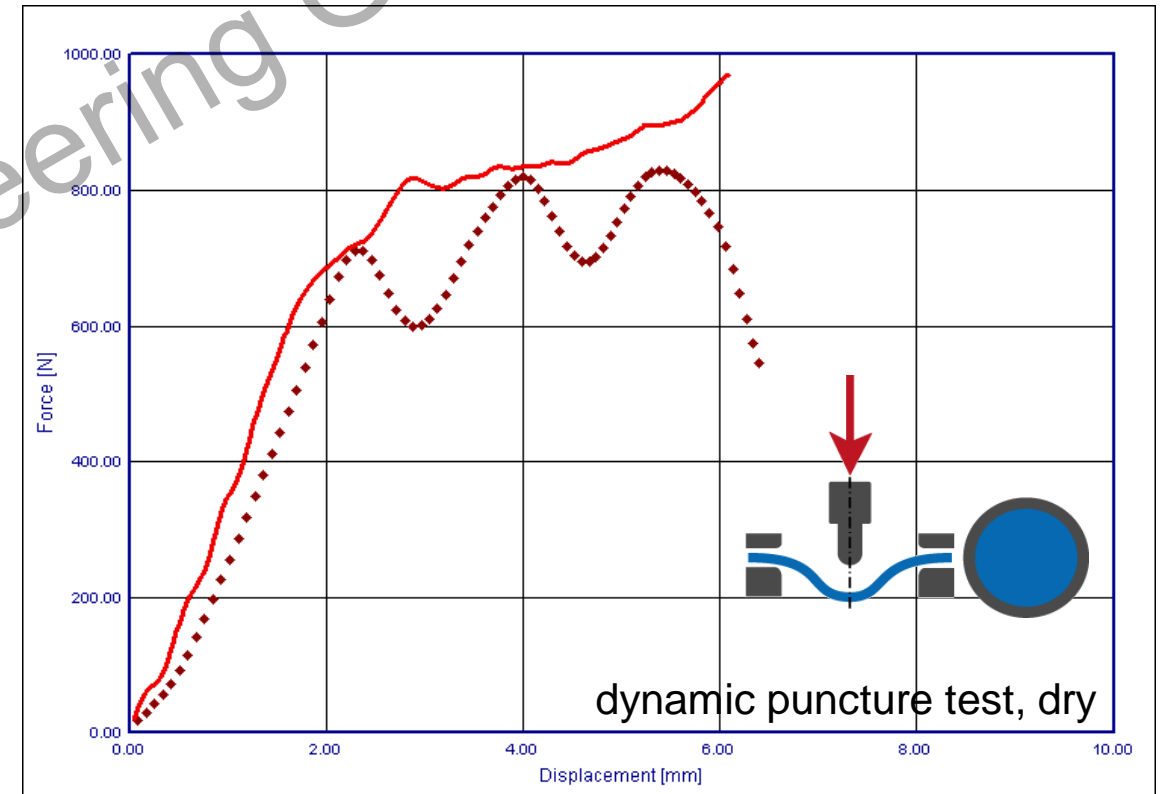
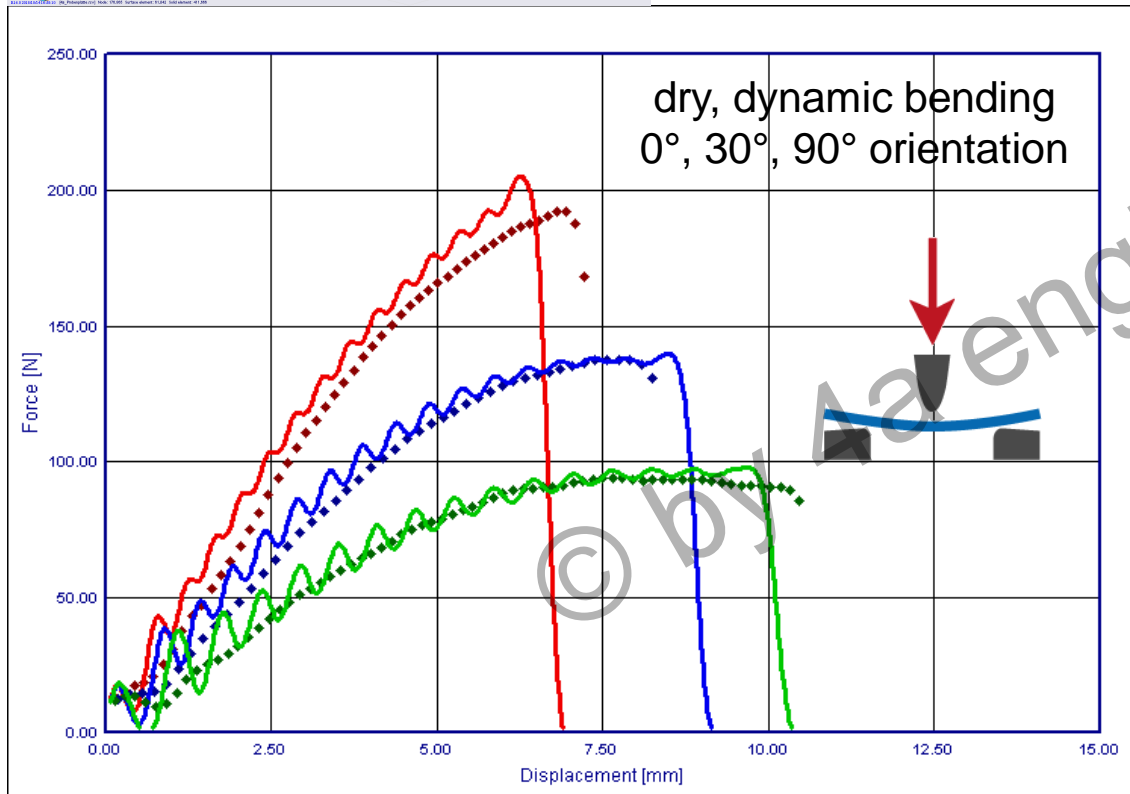


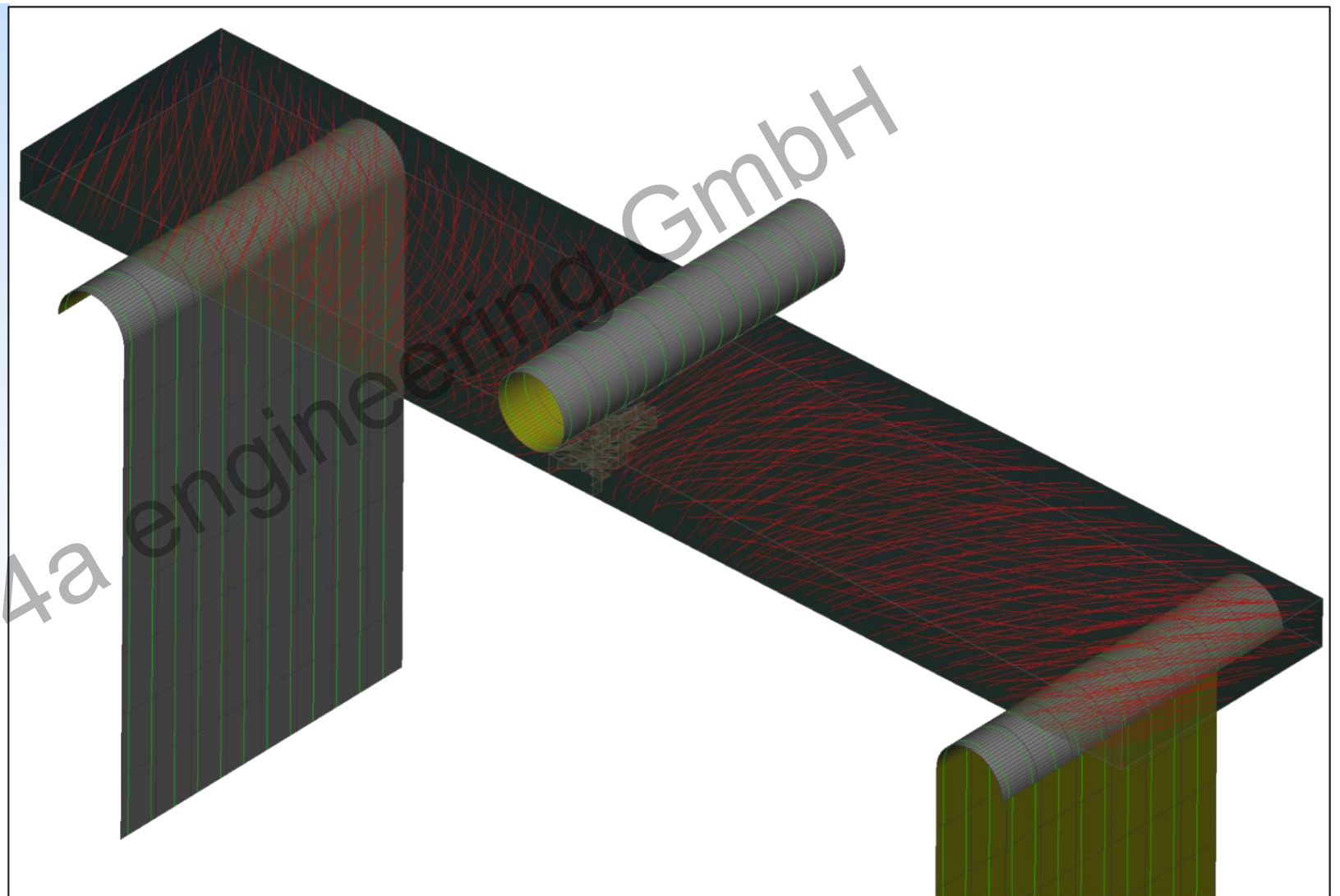
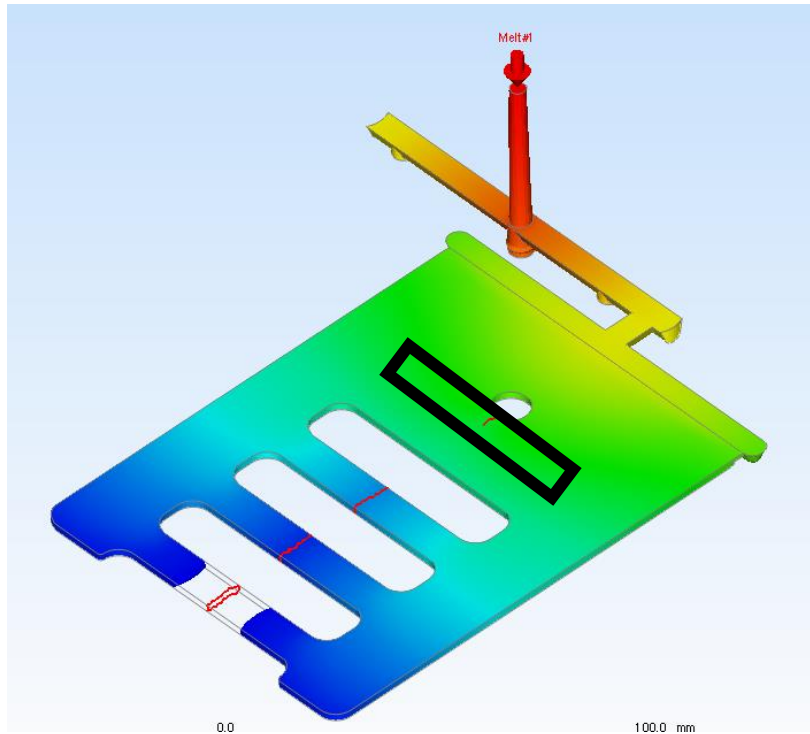
injection mold – process simulation & mapping





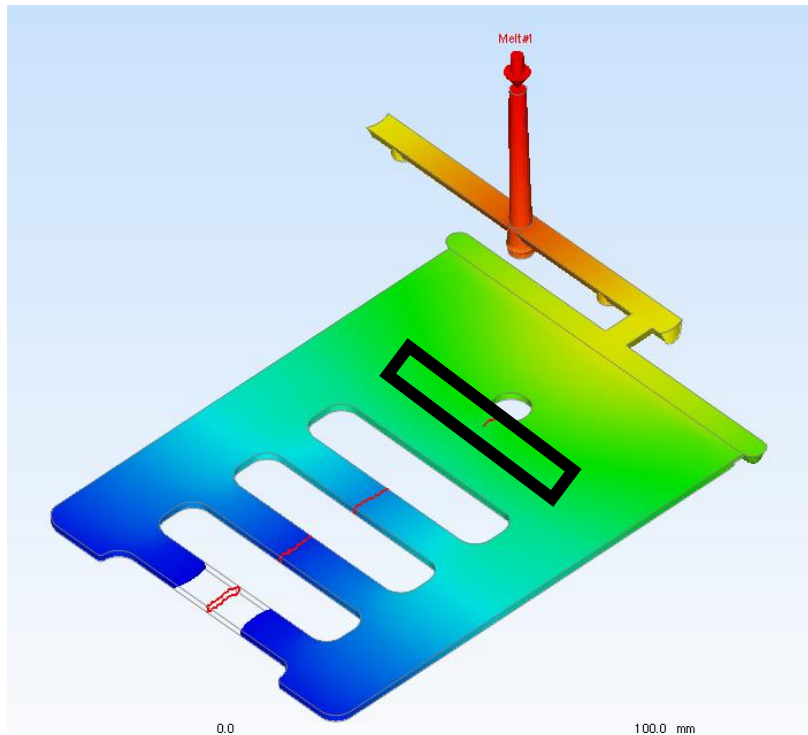
Scale of hardening curve ~20%





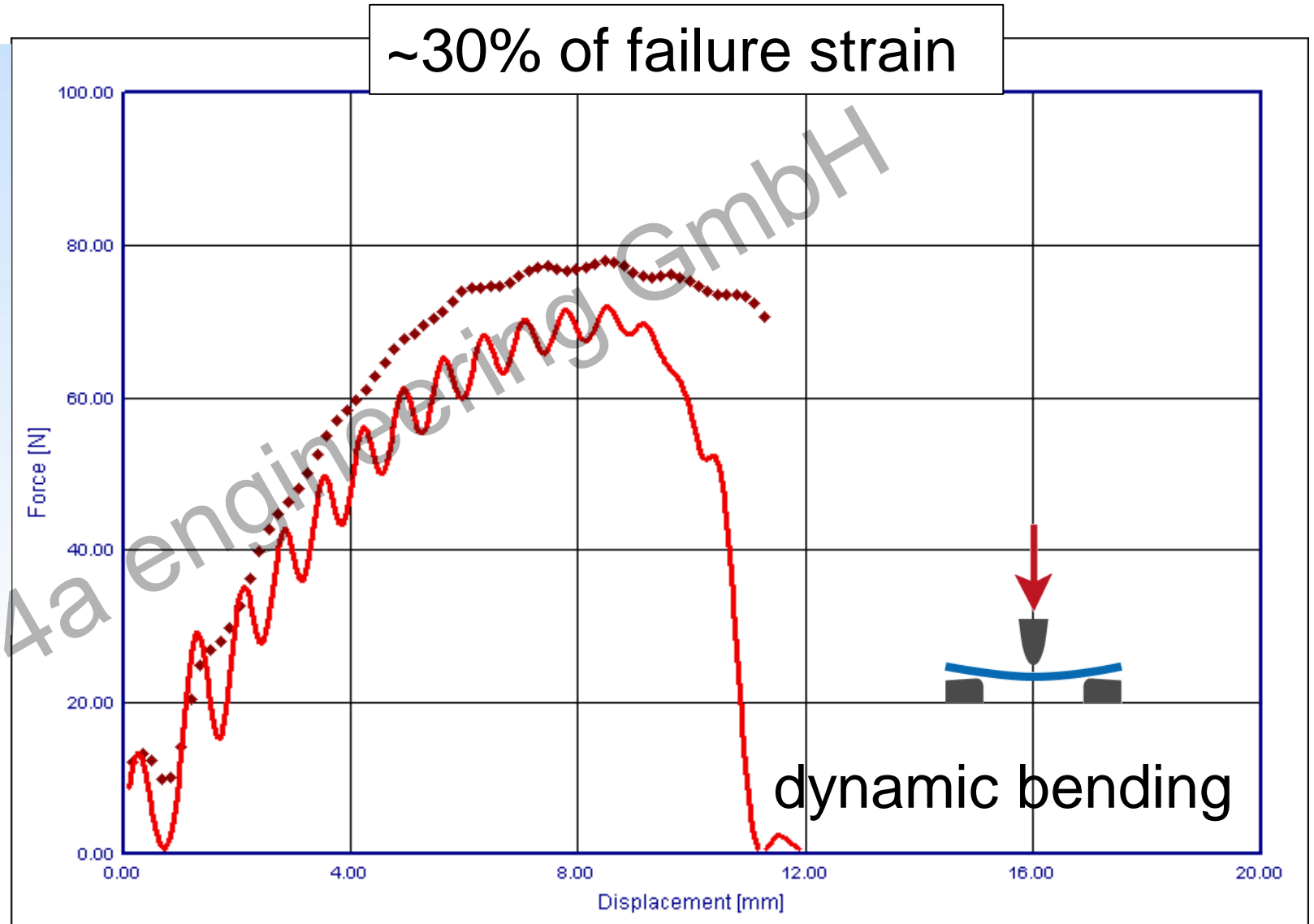
meltline

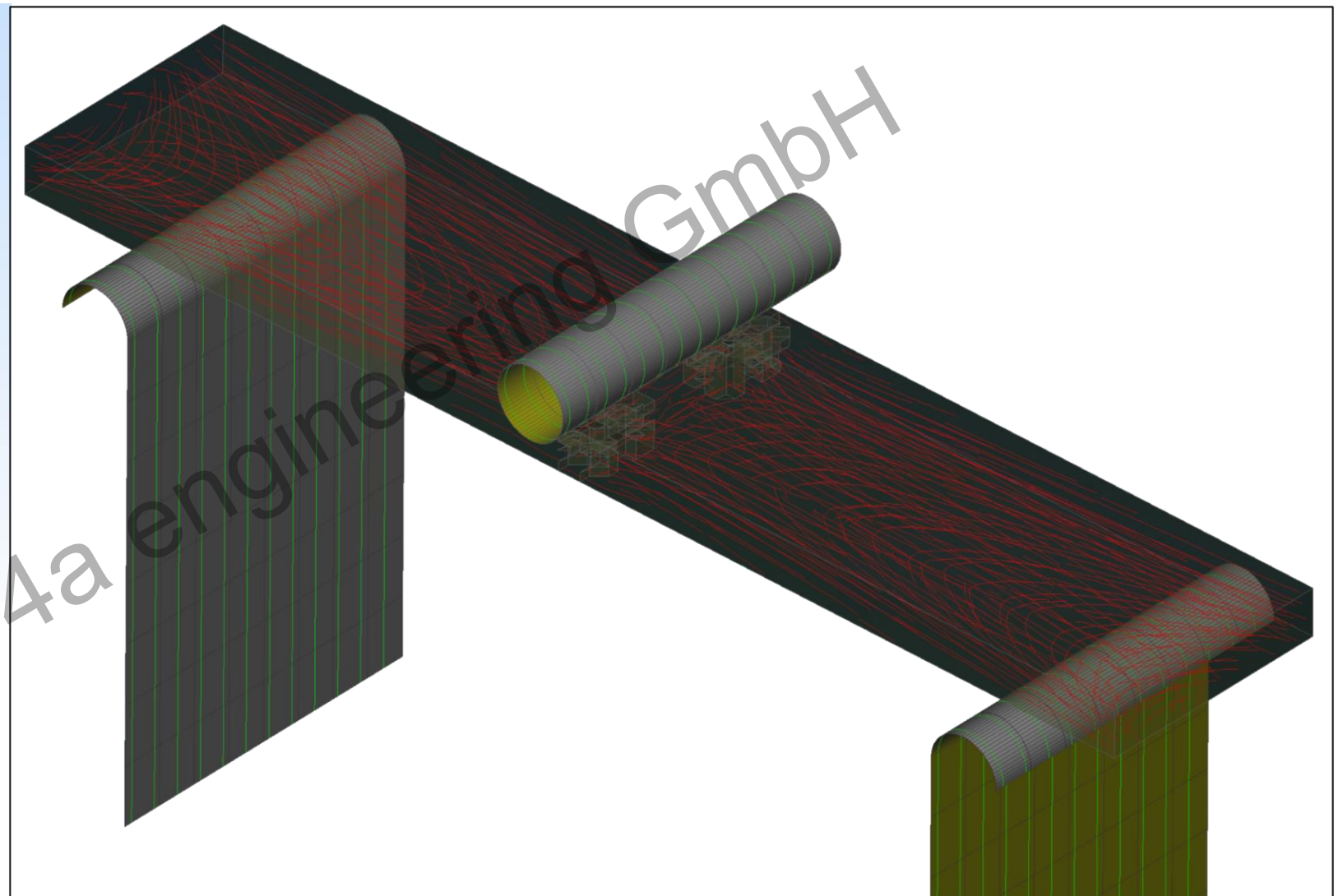
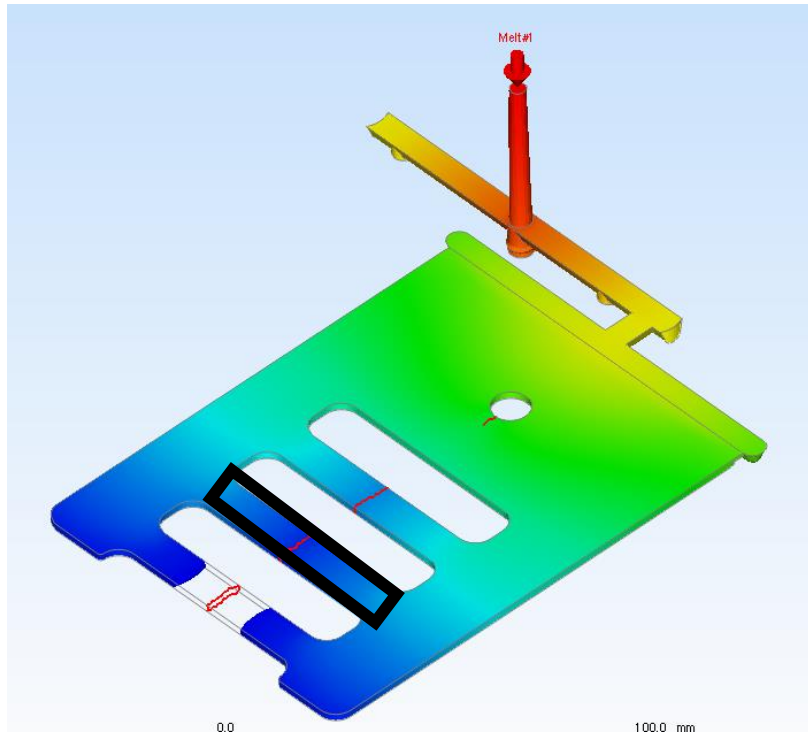
© by 4a engineering GmbH



meltline

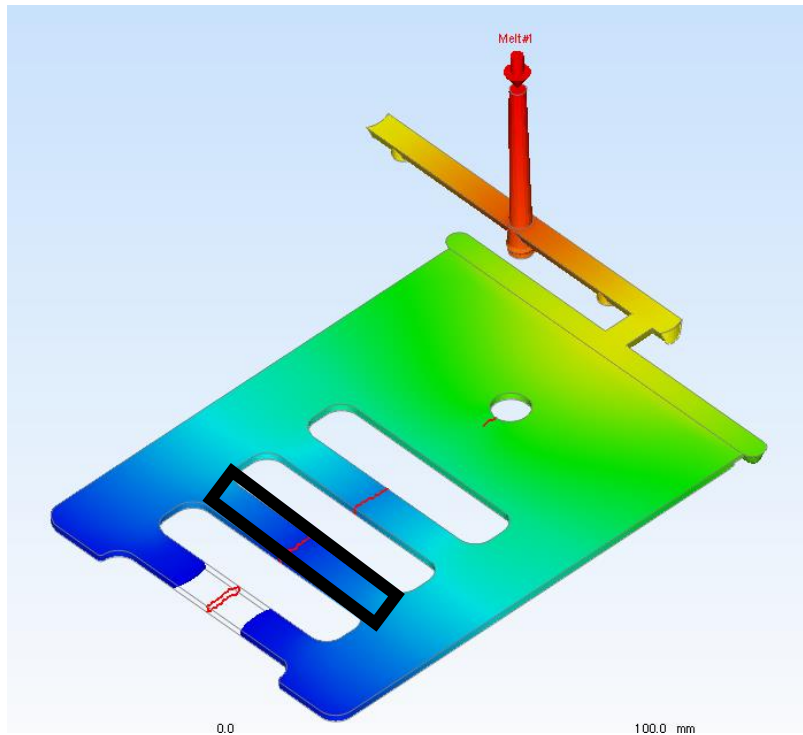
© by 4a engineering GmbH





weldline

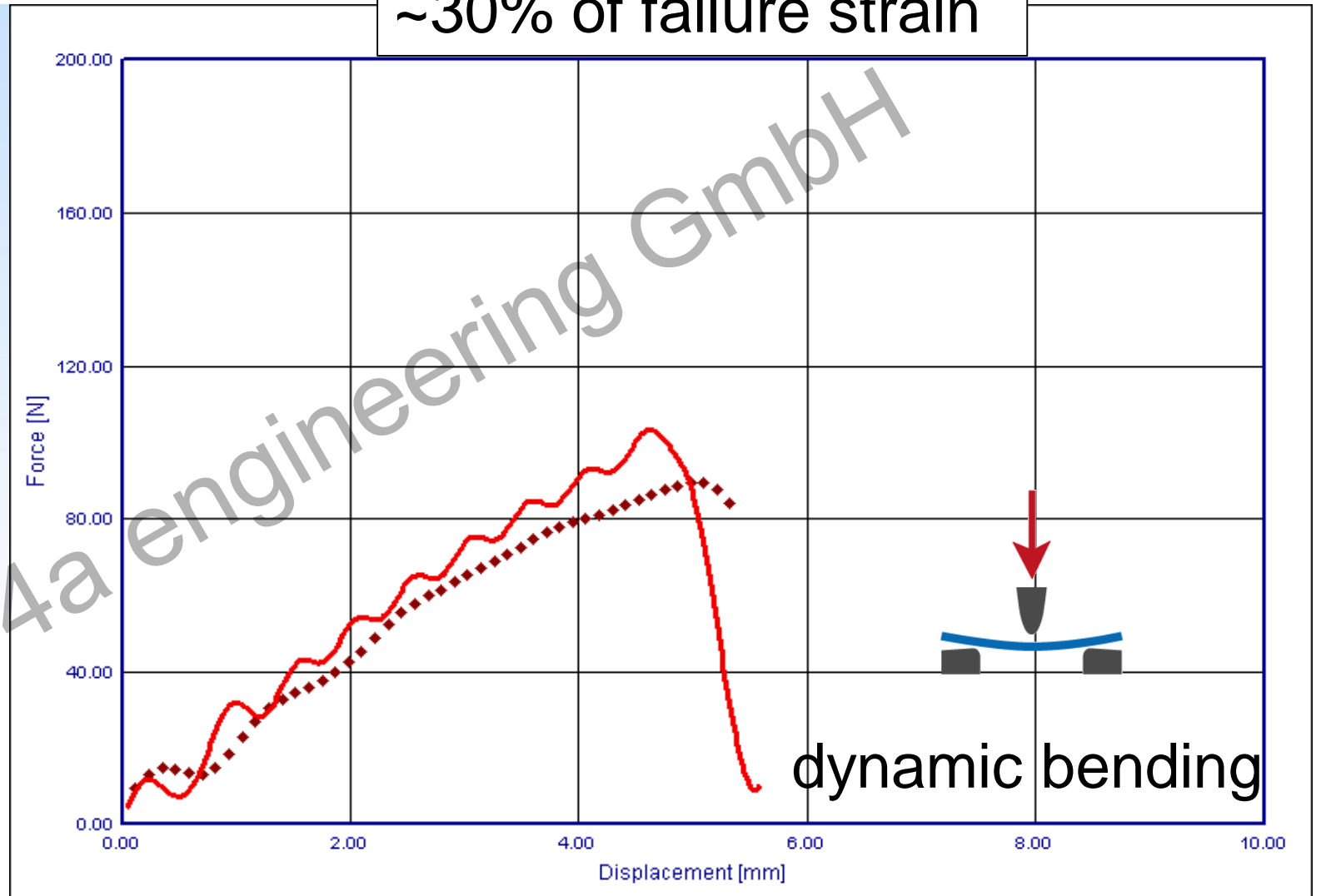
© by 4a engineering GmbH



weldline

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~30% of failure strain

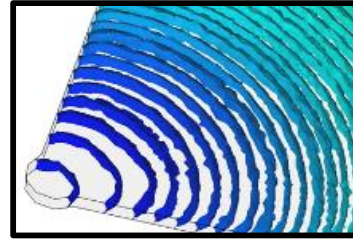
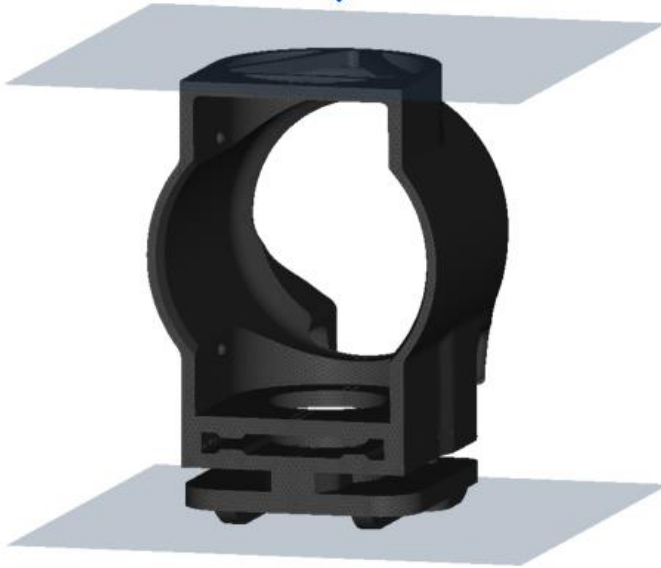


dynamic bending

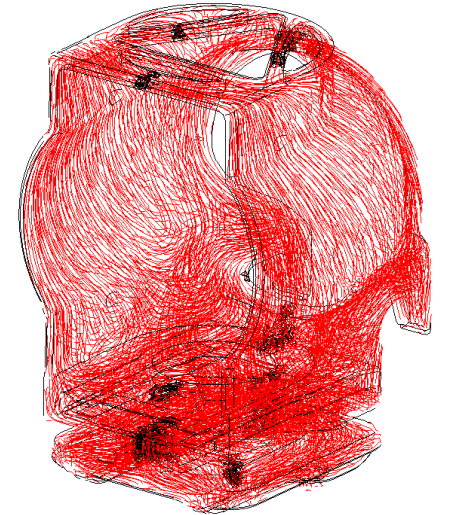
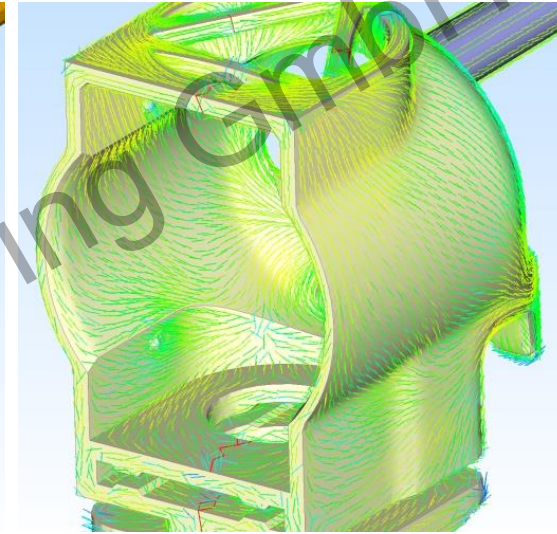
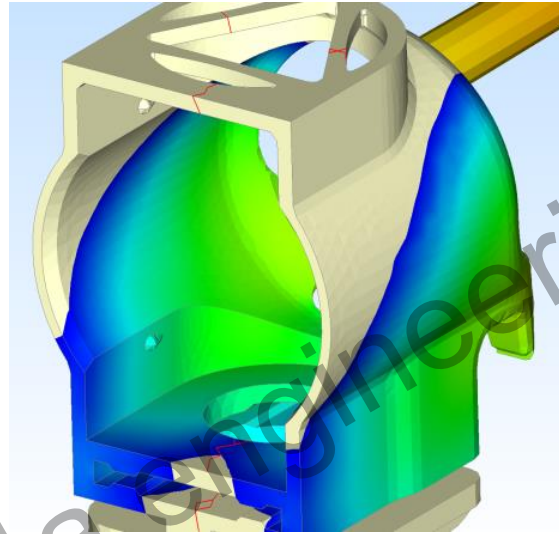
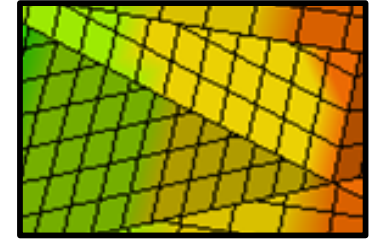
Casestudy - sleeve

$m=7.15 \text{ kg}$, $v_{\text{int}}=3.1 \text{ m/s}$

the Platte



FIBERMAP



Typische Elementgröße: 0.25mm
Elementtyp: Tetrahedron Type 10
Elementanzahl: 469 470



See more: R. Steinberger, et.al. Hirtenberger Automotive Group – *Considering the Local Anisotropy of Short Fiber Reinforced Plastics*, European Dynaforum 2017

Casestudy - sleeve

test

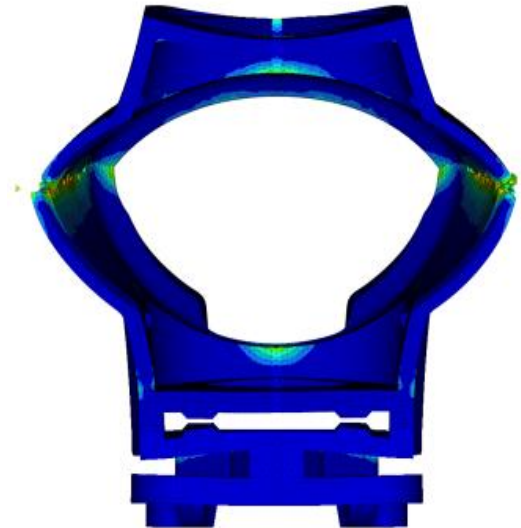
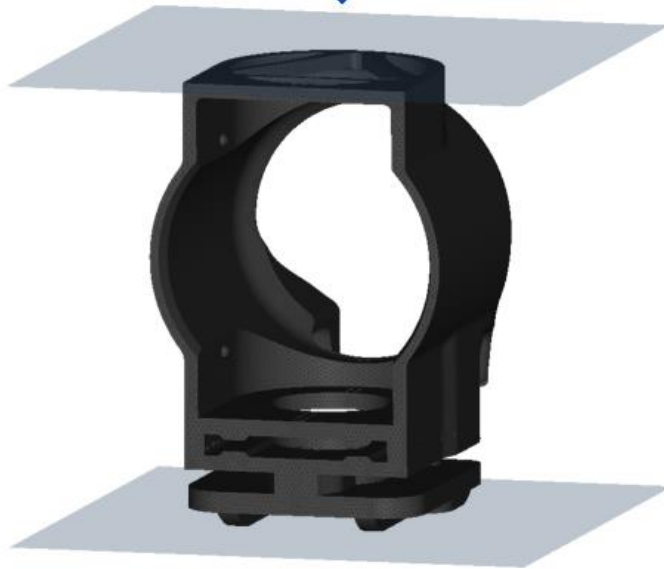
**MAT_157/215*
local anisotropy

**MAT_24*
isotropic

$m=7.15 \text{ kg}$, $v_{\text{int}}=3.1 \text{ m/s}$



the Platte



Typische Elementgröße: 0.25mm
Elementtyp: Tetrahedron Type 10
Elementanzahl: 469 470



See more: R. Steinberger, et.al. Hirtenberger Automotive Group – *Considering the Local Anisotropy of Short Fiber Reinforced Plastics*, European Dynaforum 2017

Intelligent reliable solutions for plastics, composites, metals, foams, ...

◀ **IMPETUS**

✓ **VALIMAT**

◉ **MICROMECH**

➤ **FIBERMAP**

Foams

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

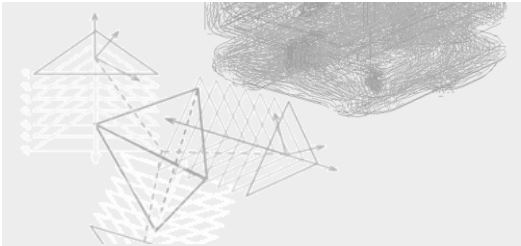
Metals

efficient
dynamic testing

from test to validated
material cards

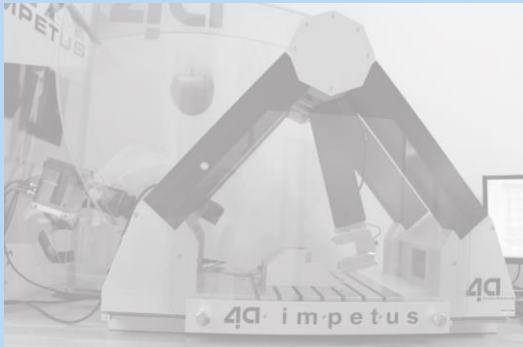
3D anisotropic
material cards

individual mapping
process information



Intelligent reliable solutions for plastics, composites, metals, foams, ...

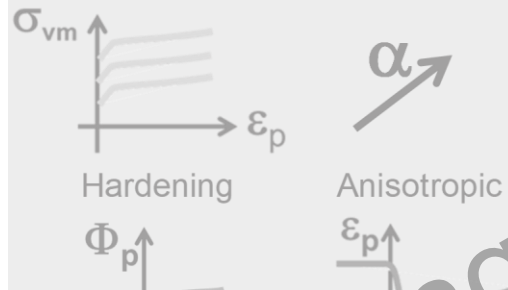
 **IMPETUS**



Composites (Carbon)

efficient
dynamic testing

 **VALIMAT**



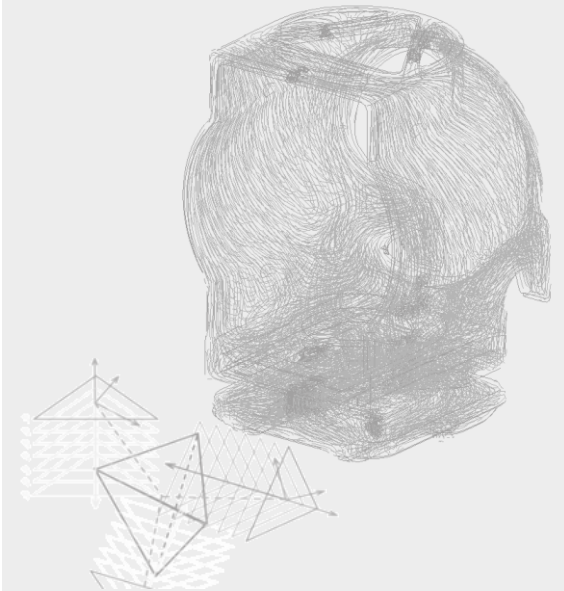
from test to validated
material cards

 **MICROMECH**



3D anisotropic
material cards

 **FIBERMAP**



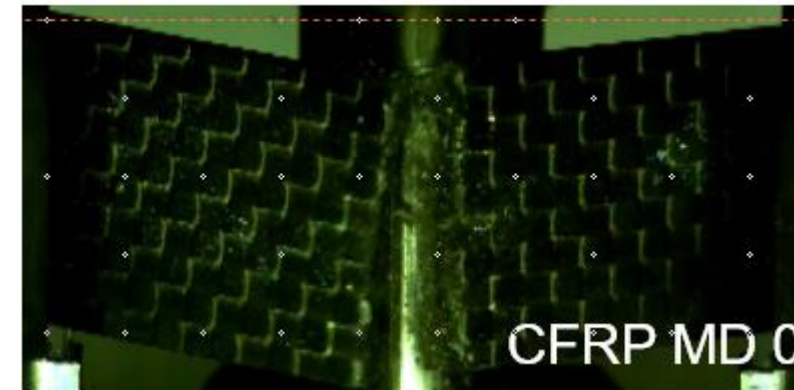
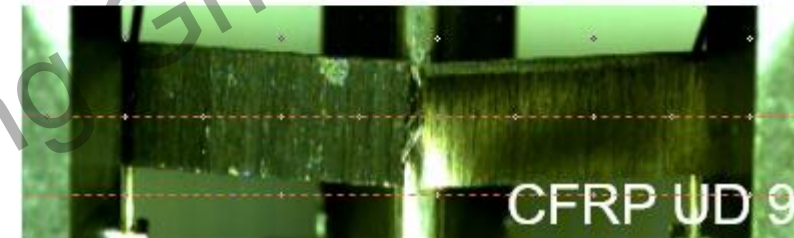
individual mapping
process information

Composites – typical test setup

specimen		0°	45°	90°
	UD	static		
	MD		static, cyclic	
	UD	static, dynamic		
	MD	static, dynamic		
	MD	Puncture		

Material Card

Validation



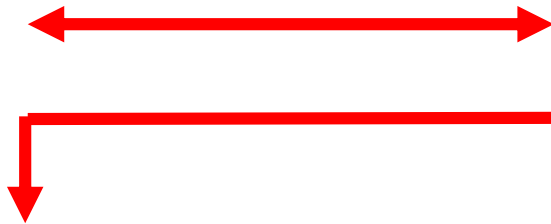
Composites – available LS-DYNA material models



No.	Elastic	Plastic	Damage	Strain rate	Failure	
22	Orthotropic	None	None	None	Orientation dependent	Carbon, Glass, Kevlar endless & fabric
54/55	Orthotropic	None	Elastic Orthotropic	Strength	Chang-Chang/ Tsai-Wu Orientation dependent	
58	Orthotropic	None	Elastic Orthotropic	Strength, Stiffness	mod. Hashin Orientation dependent	
158	Orthotropic	None	Elastic Orthotropic	Visco-elasticity	Orientation dependent	
261	Orthotropic	None	Elastic Orthotropic	None	failure Pinho (Puck) Orientation dependent	
262	Orthotropic	None	Elastic Orthotropic	None	failure Camanho (Puck) Orientation dependent	

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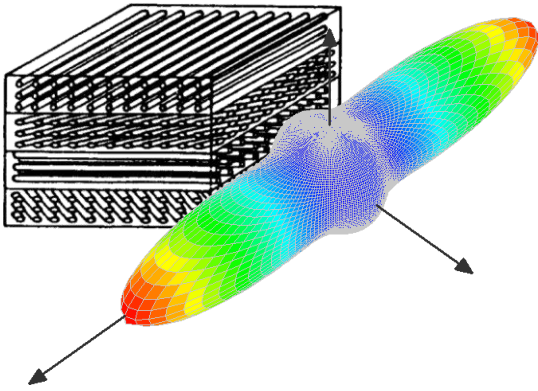
*Part_Composite



Material behaviour	
Material source	Implemented
Elasticity	Not isotropic elastic
Plasticity	Not selected
Failure/Damage	Not selected
Material card	*MAT_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_157)
Deformation	*MAT_COMPOSITE_DAMAGE (*MAT_022)
Damage/Failure	*MAT_ENHANCED_COMPOSITE_DAMAGE (*MAT_054)
Materialcard id	*MAT_LAMINATED_COMPOSITE_FABRIC (*MAT_058)
Density	*MAT_RATE_SENSITIVE_COMPOSITE_FABRIC (*MAT_158)
Plasticity	*MAT_LAMINATED_FRACTURE_DAIMLER_PINHO (*MAT_261)
Function (Hardening, Elastic curve form)	*MAT_LAMINATED_FRACTURE_DAIMLER_CAMANHO (*MAT_262)
Strain rate dependency	*MAT_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_157)
Micromec	*MAT_MICROMECC (*MAT_215)
Fracture	*MAT_MICROMECC (*MAT_215)+Carbon
Postfracture	None

Material settings	
Material source	Implemented
Materialcardcase	7300_MAT22
Damage/Failurecase	Chang Chang
Materialcard id	1000000
Density	1480
Plasticity	None
Function (Hardening, Elastic curve form)	
Strain rate dependency	None
Micromec	Endless fiber reinforced plastics
Matrix	
Density of the matrix	1093
E-Modulus	3000
Poisson's ratio	0.3
Yield strength	50
Strength at Break	70
Failure strain	0.05
Fiber	
Fillerlength	20000
Fillerdiameter	20
Phi or Psi	φ
Phi	58
Psi	71.7
Fillermaterial	T300
Orientation	
Fillerorientationtype	UD
Strength	
Strength evaluation	Fiber strength
XT	2300
XC	2000
Fracture	Composite
Postfracture	None

Available LS-DYNA materialcards in VALIMAT™



$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$

C...composite, F...fiber, M...matrix

160826_004		Material	Designvariablen	Layers
Model settings				
Material				
Idealization				
Material behaviour				
Material source		Implemented		
Material card		*MAT_COMPOSITE_DAMAGE (*MAT_022)		
Materialcardcase		7500_MAT22		
Damage/Failurecase		Chang Chang		
Materialcard id		1000000		
Density		1480		
Plasticity		None		
Function (Hardening, Elastic curve form)				
Strain rate dependency		None		
Micromec		Endless fiber reinforced plastics		
Matrix				
Density of the matrix		1093		
E-Modulus		3000		
Poisson's ratio		0.3		
Yield strength		50		
Strength at Break		70		
Failure strain		0.05		
Fiber				
Fillerlength		20000		
Fillerdiameter		20		
Phi or Psi		φ		
Phi		58		
Psi		71.7		
Filler material		T300		
Orientation				
Fillerorientationtype		UD		
Strength				
Strength evaluation		Fiber strength		
XT		2300		
XC		2000		
Fracture		Composite		
Postfracture		None		

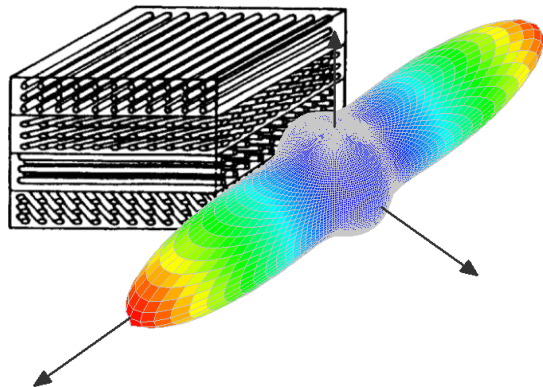
Matrix properties

Filler properties

Orientation

Strength

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$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$

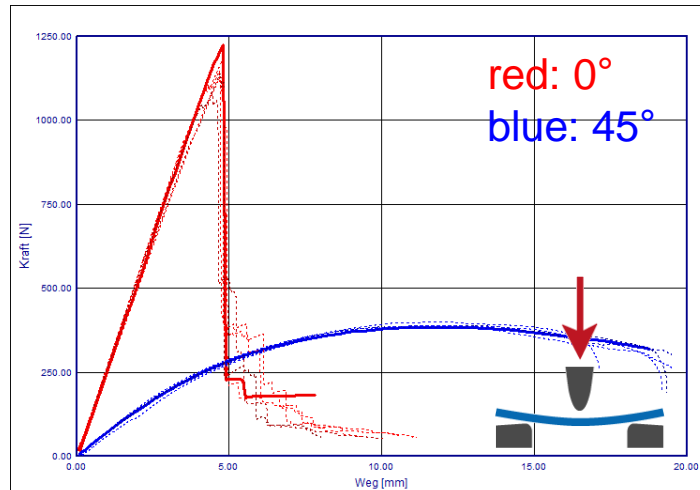
C...composite, F...fiber, M...matrix

Typical Design Variables for *MAT_022

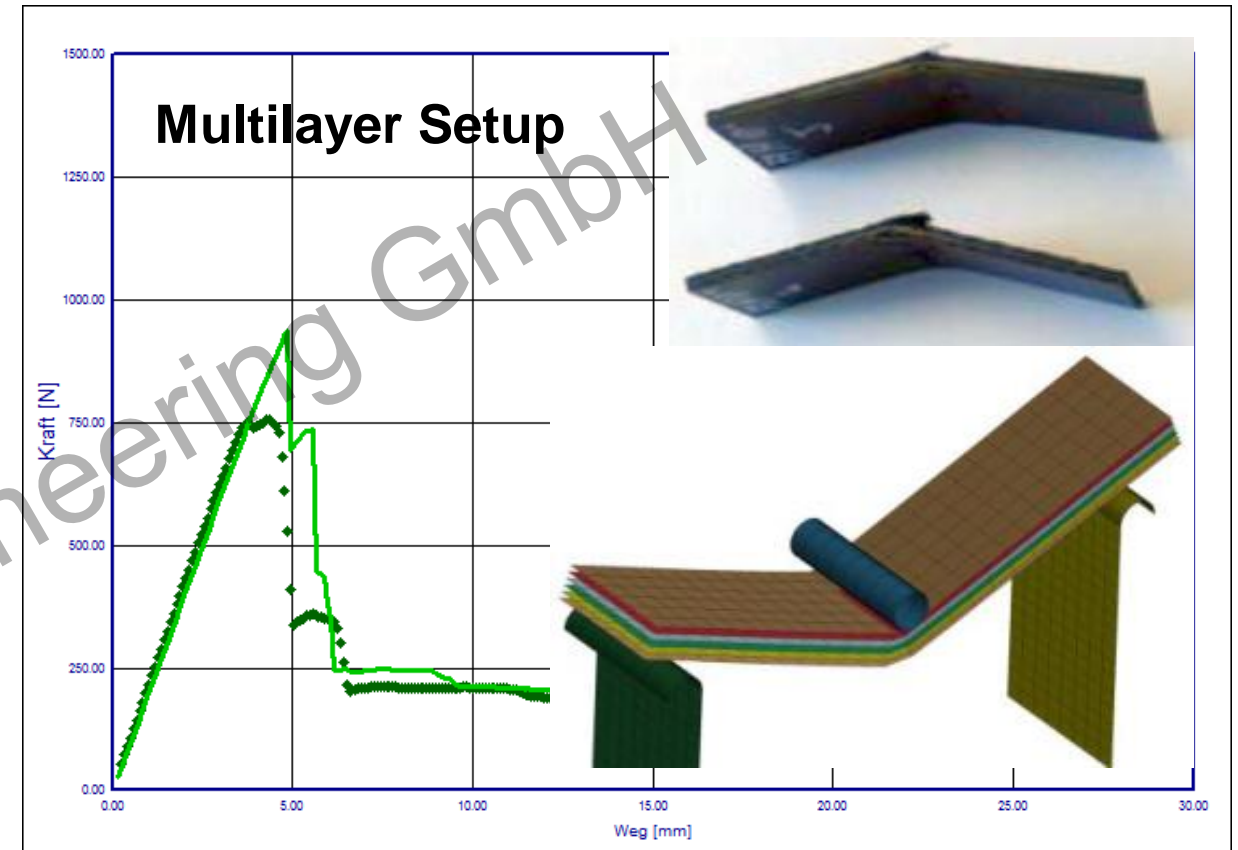
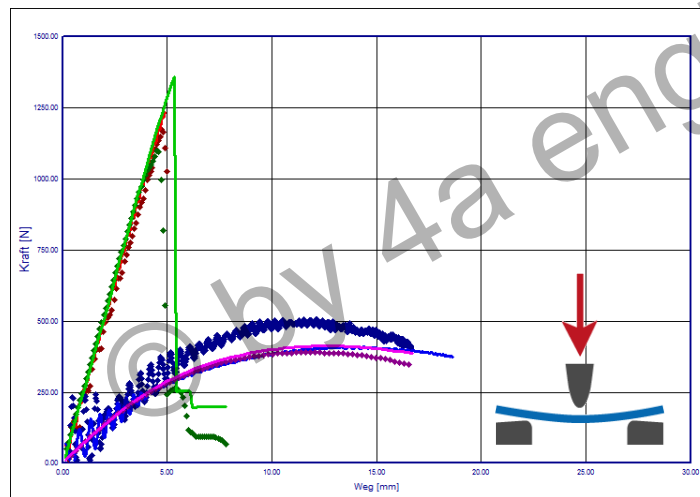
Name	Start	const...	from	to	Variance	Condi...	Description
^ GroupName: 10_elasticity							
c_E11	MMEC	<input type="checkbox"/>	100000	180000	(NULL)		young modulus tensile in 1 direction
c_E22	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		young modulus tensile in 2 direction
c_E33	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		young modulus tensile in 2 direction
c_nue21	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 21 plane
c_nue31	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 31 plane
c_nue32	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 32 plane
c_G12	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 12 plane
c_G23	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 23 plane
c_G31	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 31 plane
^ GroupName: 51_failure							
fc_R11T	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R11C	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R22T	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R22C	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R12	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		

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Orientation



static versus dynamic

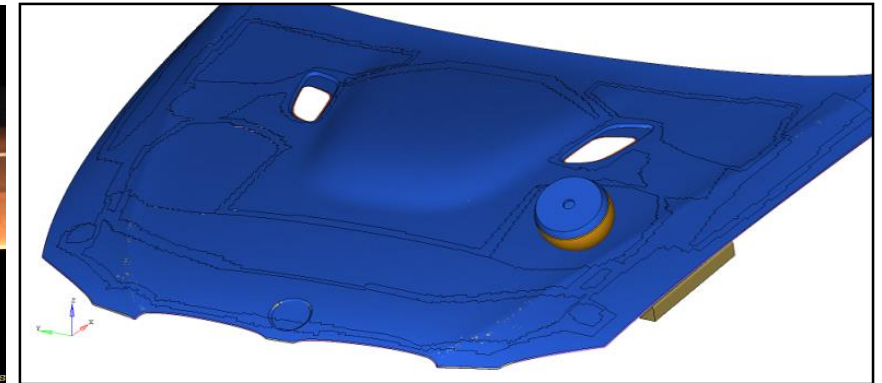
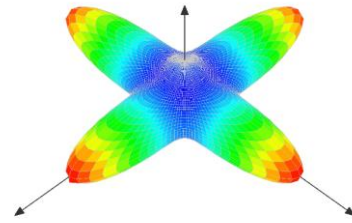


.... test
— simulation

P. Reithofer (4a engineering GmbH) & B. Fellner (MAGNA STEYR Engineering Austria) - Materialcharakterisierung von Composites; 4a Technologietag 2015

Composite – case study

- Front hood
 - Stiffness versus pedestrian safety
- Material card
 - Composite layup with anisotropic material behavior
 - Core material – Honeycomb different compression levels



[SOURCE: LINK to PAPER](#)

intelligent reliable solutions for plastics, composites, metals, foams, ...

 **IMPETUS**

 **VALIMAT**

 **MICROMECH**

 **FIBERMAP**

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

efficient
dynamic testing

from test to validated
material cards

3D anisotropic
material cards

individual mapping
process information

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Summary

Part 2: Modeling of fiber reinforced thermoplastics

Summary

- different models needed for different materials
 - COMPOSITE (higher fiber content) → elastic + damage
 - SFRT, LFRT (medium fiber content) → viscoplasticity also of importance
- Two main approaches
 - Macro scale – composite behavior
 - Micro scale – distinguish between fiber and resin/matrix behavior
- Differences
 - Flexibility in usage (Micro ++)
 - Computational effort (Macro ++)

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Summary

- LS-DYNA offers a lot of different material models for
 - thermoplastic materials
 - short and long fiber reinforced thermoplastics
 - classical composites
- all materials show different mechanical response dependent on different aspects like anisotropy, viscosity, temperature, moisture, ...
- material characterization must focus on the main behavior and material card generation must reflect that
- tools are needed to handle data and to fit complex failure models



IMPETUS



VALIMAT

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Thank you for your Attention!

4a summer-school - webinar and training Material characterization with VALIMAT® and IMPETUS®

SAVE THE DATE
07.07. - 17.07.2020

 **VALIMAT**

more information on our software



α
Anisotropic

ϵ_p
Damage/Failure

Φ_p
Triaxiality

σ_{vm}
Hardening

η

ϵ_p

www.4a-engineering.at/valimat

 **IMPETUS**

comprehensive test package overview



www.4a-engineering.at/test-packages

Appendix
Additional overview



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efficient dynamic testing

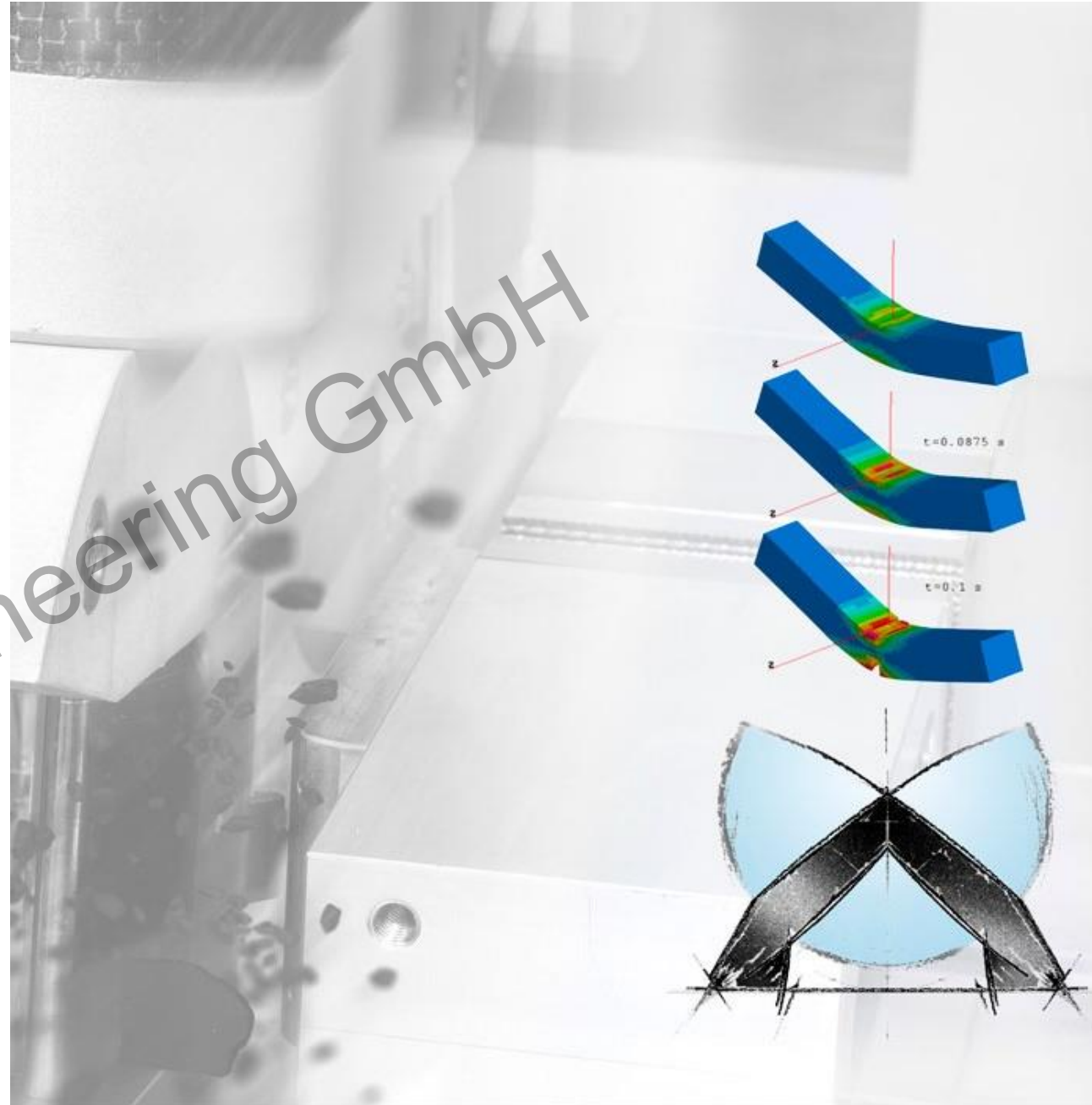
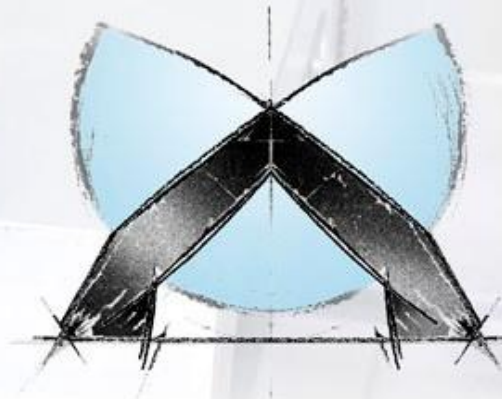
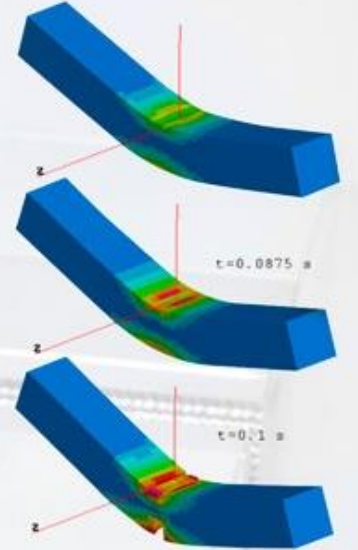


IMPETUS

engineering plastics production
excellence in testing
simulation
concepts lightweight prototypes

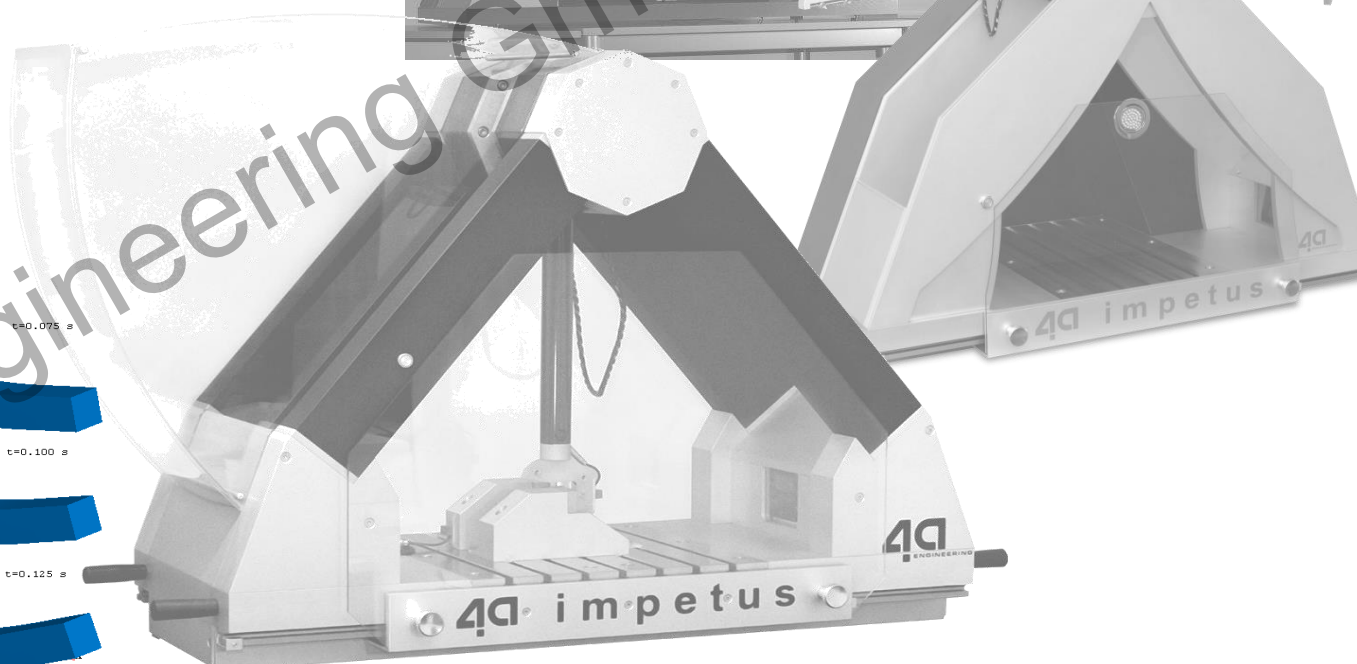
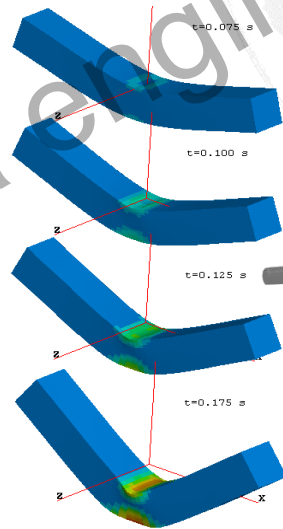


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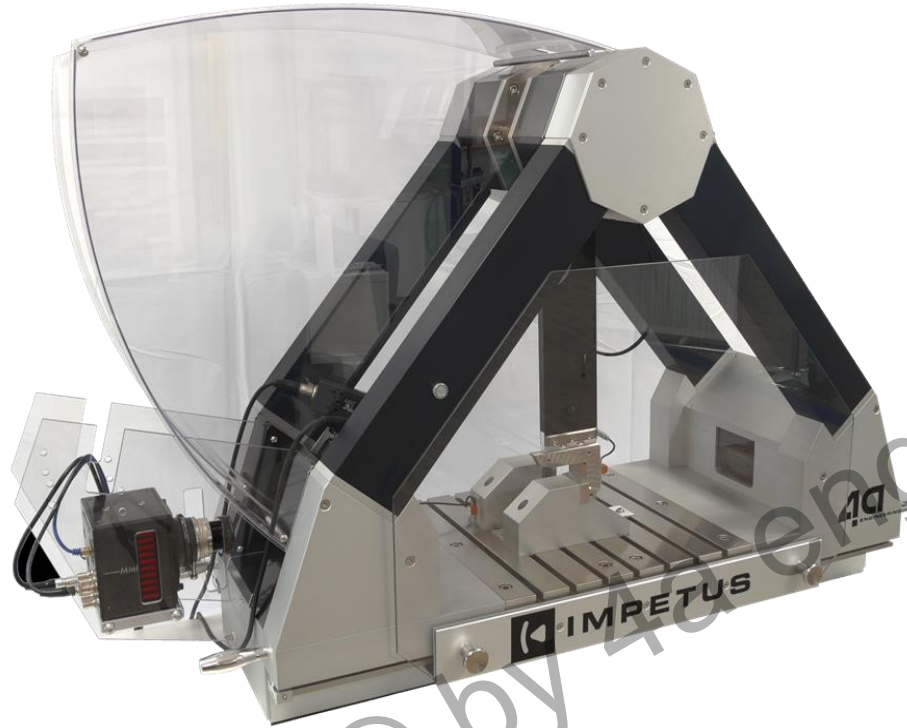


Efficient dynamic testing

- desktop testing device
- instrumented high-speed testing
 - acceleration → force / displacement
- impact velocity 0.5 – 4.5 m/s



IMPETUS™ data specification



technical specifications

maximum energy	50J
length of swing arm	500mm
mass of swing arm	1.5 - 3.0kg
impact velocity	0.5 - 4.4m/s

weights and dimensions

L x W x H	1400 x 600 x 850mm
mass	165kg

desk load and dimensions minimum required

L x W x H	1500 x 800 x 800mm
minimum load	250kg

electrical supply data

230 VAC 50 Hz	0.5A
115 VAC 60 Hz	1.0A

5V camera trigger

output level high	>2.5V
output level low	<0.5V

Highspeed camera is an optional equipment and can be ordered separately.

Photron High Speed Camera data specification



Photron

FASTCAM	MINI AX200 540K	NOVA S6 800K	NOVA S9 900K	NOVA S12 1000K
CMOS Image Sensor	1024 x 1024	1024 x 1024	1024 x 1024	1024 x 1024 px
max. fps full resolution	6400	6400	9000	12800 fps
max. Frame Rate	540000	800000	900000	1000000 fps
Light Sensitivity	40000	64000	64000	64000 ISO
L x W x H	94 x 120 x 120	217.2 x 120 x 120	217.2 x 120 x 120	217.2 x 120 x 120 mm
weight	1.5	3.3	3.3	3.3 kg

Vision Devices lighting data specification

LED VD7000

operating voltage	24 - 36 V
rated power	17 - 72 W
Luminous flux	2100 lm
Luminous flux boost	7280 lm
color temperature	6000 K
L x W x H	100 x 46 x 46 mm

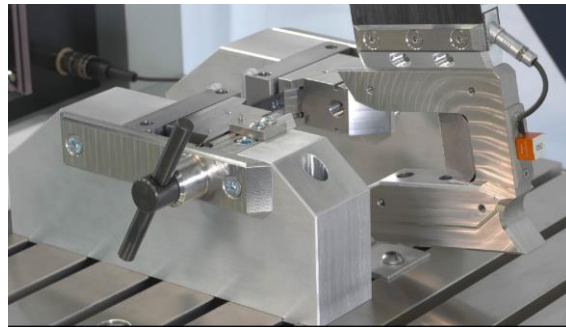


**VISION
DEVICES**

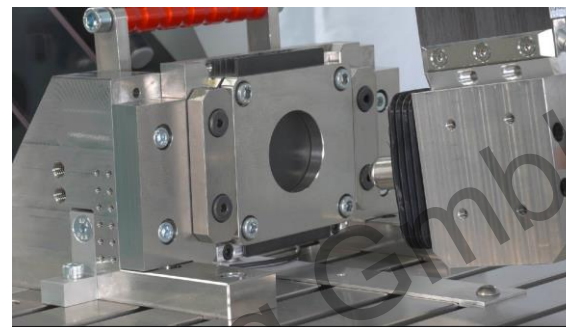
IMPETUS™ - configurations



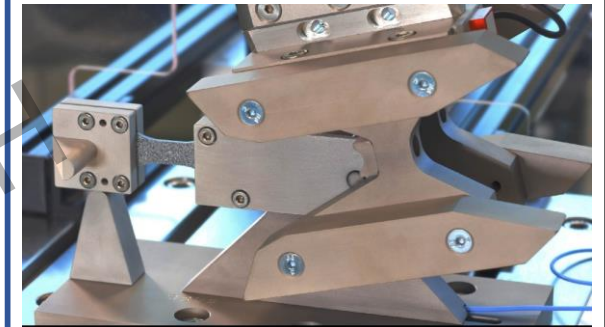
3 POINT BENDING



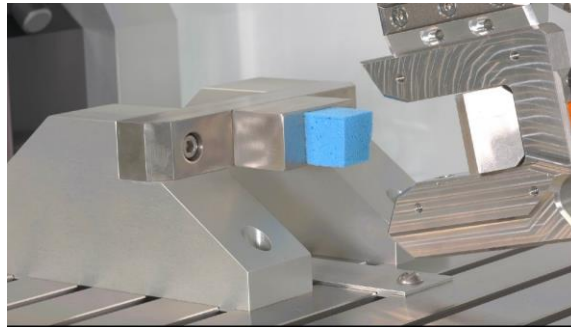
TENSION BENDING



PUNCTURE TEST



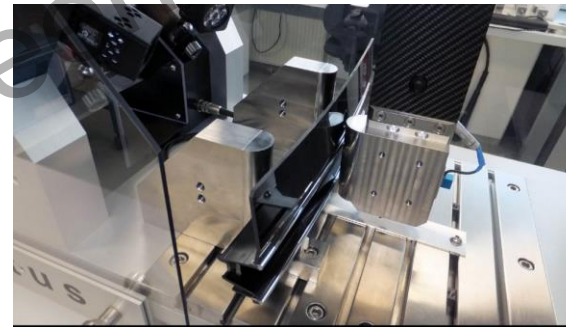
TENSION TEST



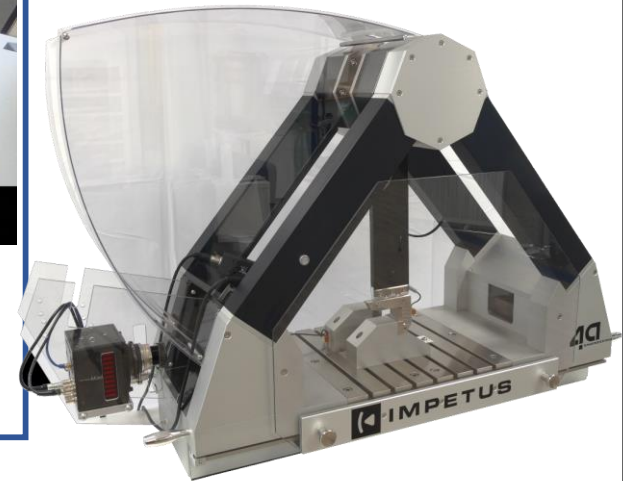
COMPRESSION TEST



SAMPLE MAGAZIN



COMPONENT TEST

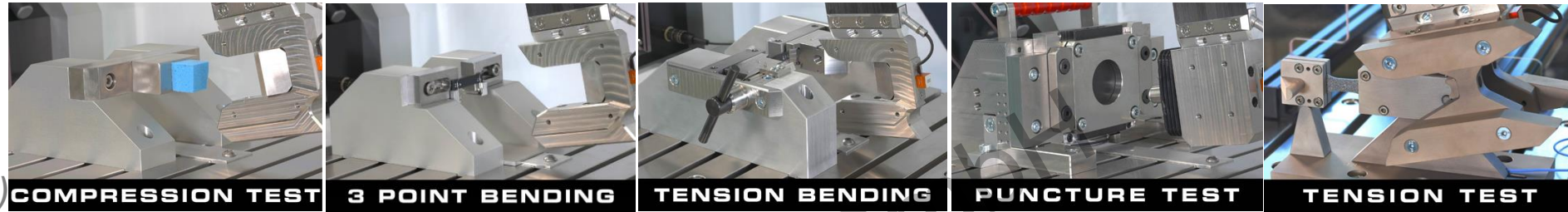


BASIC

STANDARD

PROFESSIONAL

Efficient dynamic testing



Material (*Typical thickness*)

Plastic (*1 - 4 mm*)

Foam (*20 - 30 mm*)

Composite (*1 - 4 mm*)

Aluminum (*1 - 2.5 mm*)

Metals (*0.5 - 1.5 mm*)

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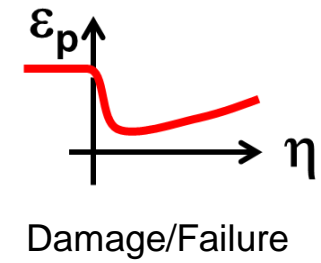
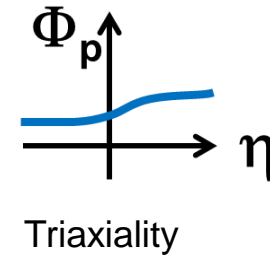
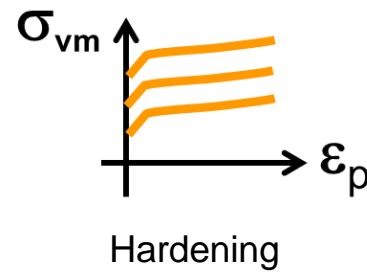
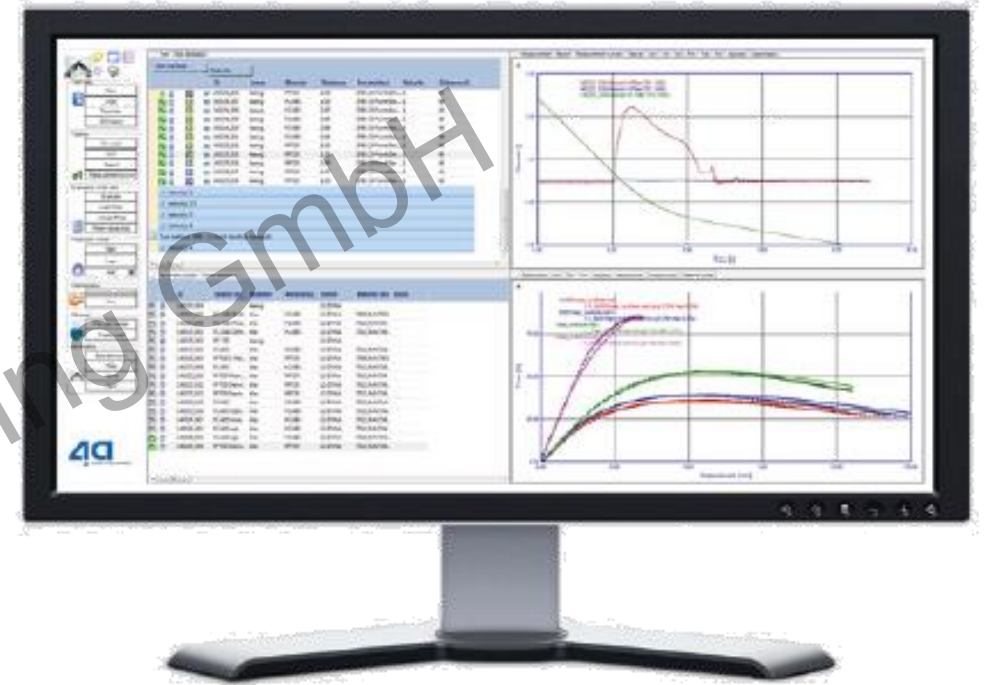


From test to material card



VALIMAT

engineering plastics production
 excellence in validation
 concepts simulation
 lightweight prototypes



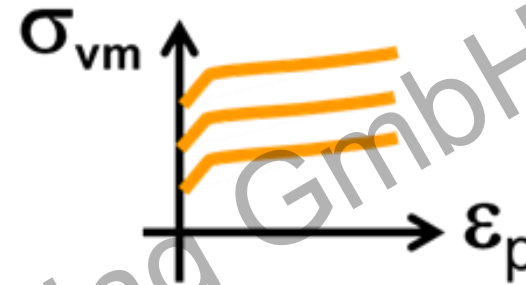
Material data generation for simulation

Current Situation

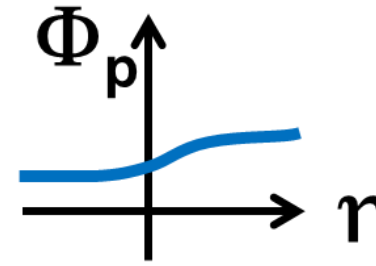
- more and more data
- Not only tension
 - Different loadcases (compression, shear,)
- More complex simulation models
Investigations on failure

NEEDED

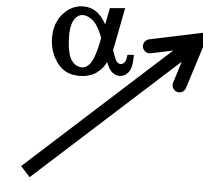
- Smart USER INTERFACE
- Optimization
- DATABASE handling data



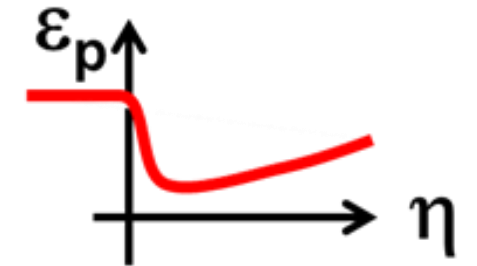
Hardening



Triaxiality



Anisotropic



Damage/Failure

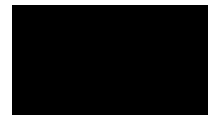
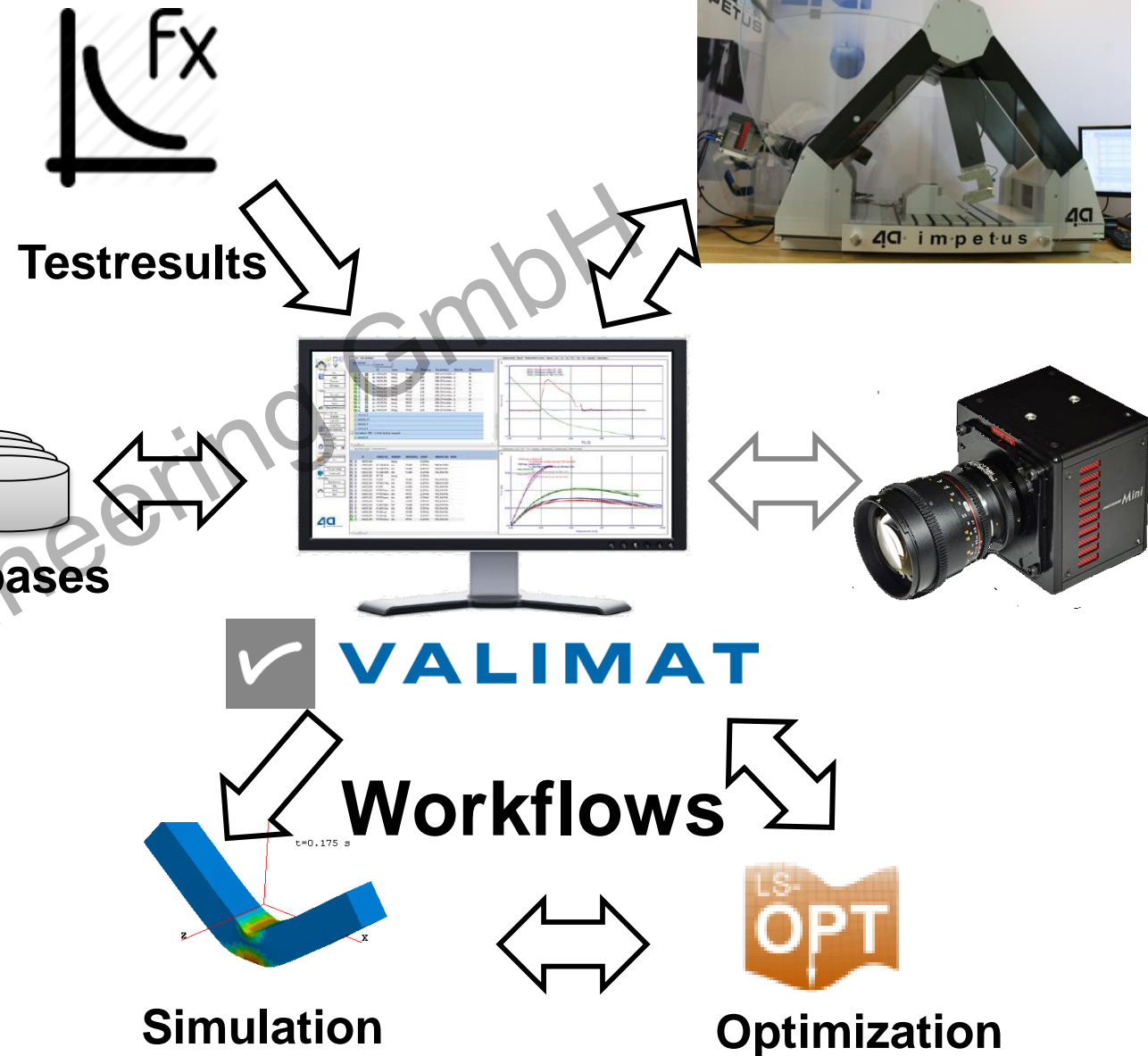
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From test to material card

VALIMAT™

Advantage

- Handling of bigdata
- Complex models
- Good correlation to simulation



Efficient dynamic testing

3 POINT BENDING TENSION BENDING COMPRESSION PUNCTURE TENSION

Plastic
Foam
Composite
Aluminum
Metals

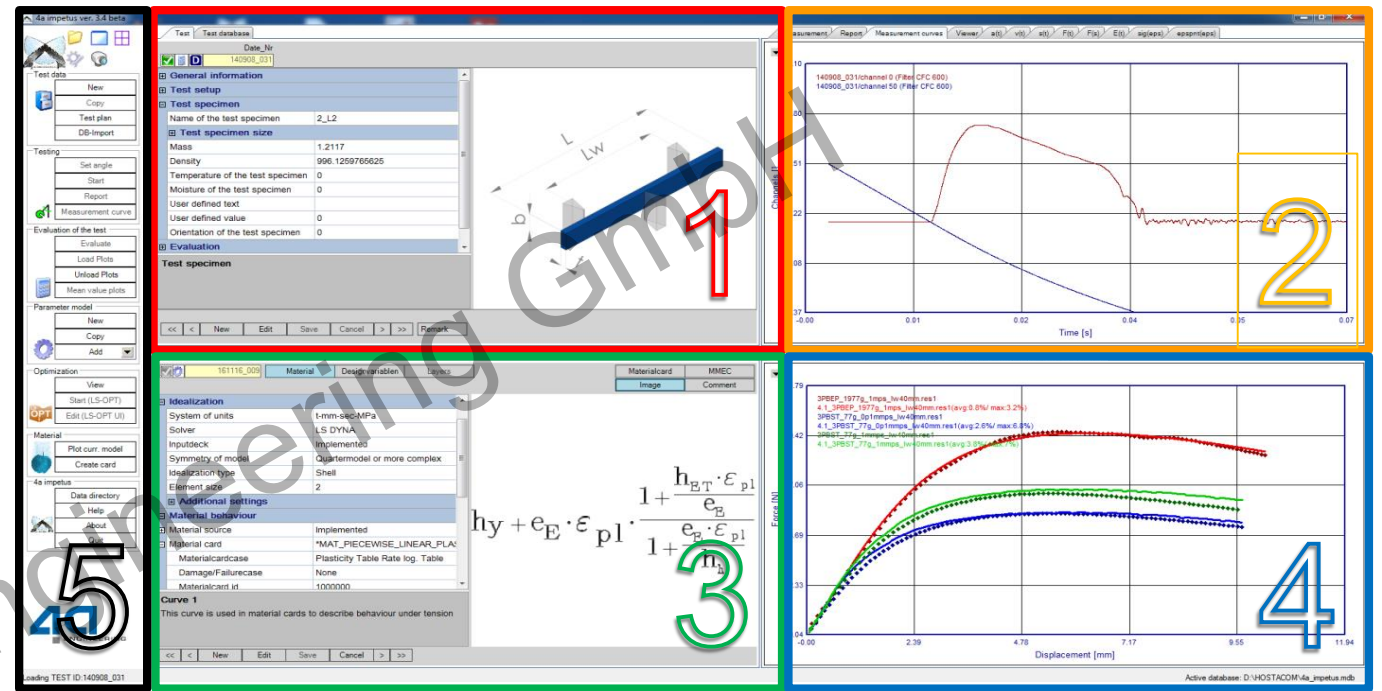
typical thickness
(1 - 4 mm)
(20 - 50 mm)
(1 - 4 mm)
(1 - 2.5 mm)
(0.5 - 1.5 mm)

automated FE-model generation
© by 4a engineering GmbH
VALIMAT

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5.551e-17
-1.320e-01
-2.640e-01
-3.960e-01
-5.280e-01
-6.600e-01

GUI - the graphic user interface is divided into five parts:



basic menu (left margin, (5))

window top left (1) → test; data base

window top right (2) → measurements; info; measurement results

window bottom left (3) → model parameter; optimization settings

window bottom right (4) → optimization; results of the optimization

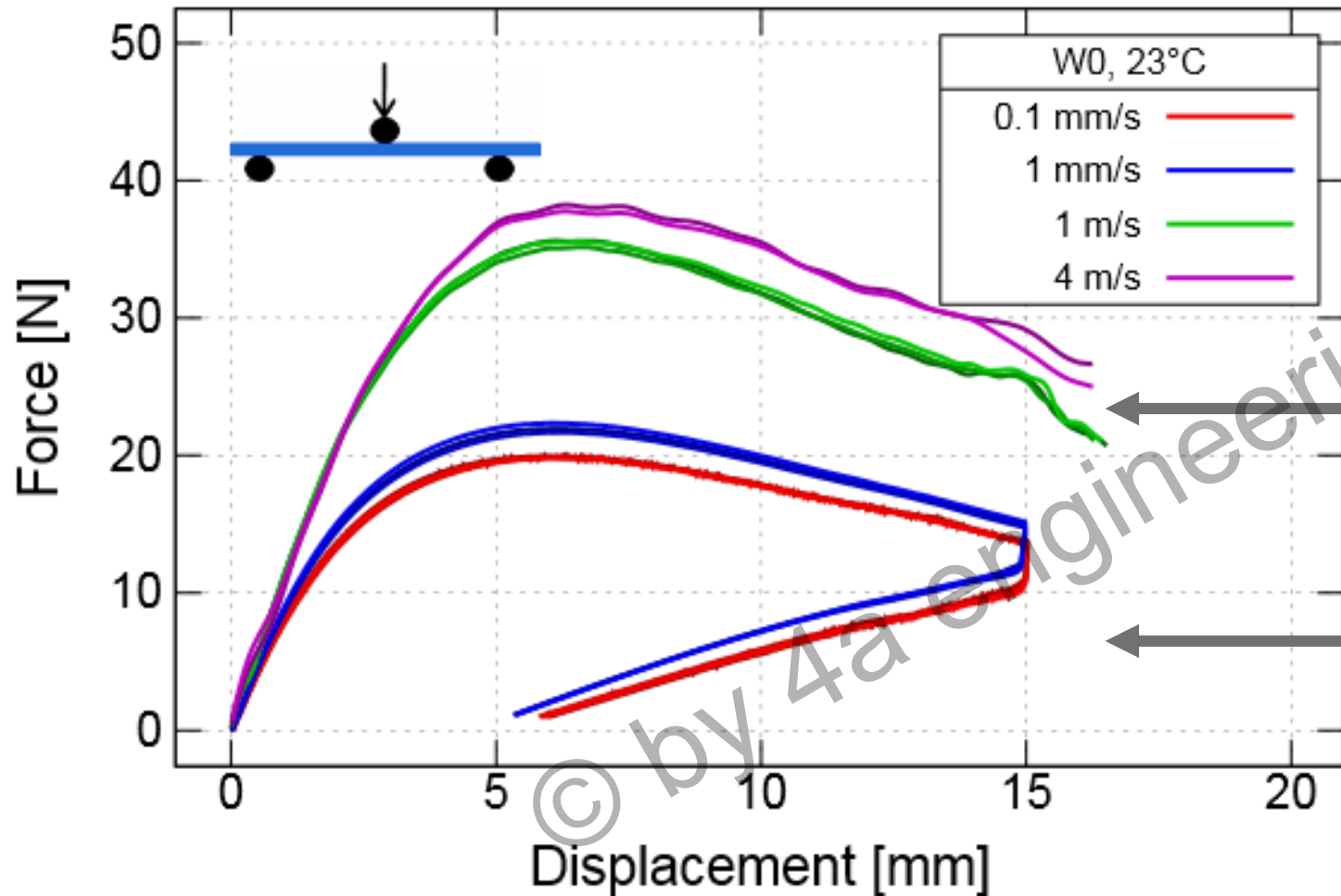
the basic menu describes the principal process from the test to the completed material model and allows a simple and fast access of the most important functions.

- Plenty of direct implemented **LS-Dyna** material models (*also Abaqus, PamCrash*)

Material card	
Materialcardcase	*MAT_ELASTIC (*MAT_001)
Damage/Failurecase	*MAT_PIECEWISE_LINEAR_PLASTICITY (*MAT_024)
Materialcard id	*MAT_PLASTICITY_COMPRESSION_TENSION (*MAT_124)
Density	*MAT_SAMP-1 (*MAT_187)
Plasticity	*MAT_FU_CHANG_FOAM (*MAT_083)
Function (Hardening, Elastic curve)	*MAT_COMPOSITE_DAMAGE (*MAT_022)
Strain rate dependency	*MAT_ENHANCED_COMPOSITE_DAMAGE (*MAT_054)
Micromec	*MAT_LAMINATED_COMPOSITE_FABRIC (*MAT_058)
Fracture	*MAT_RATE_SENSITIVE_COMPOSITE_FABRIC (*MAT_158)
Postfracture	*MAT_LAMINATED_FRACTURE_DAIMLER_PINHO (*MAT_261)
	*MAT_LAMINATED_FRACTURE_DAIMLER_CAMANHO (*MAT_262)
Loadcases	*MAT_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_157)
Results	*MAT_MICROMECH (*MAT_215)
	*MAT_MICROMECH (*MAT_215)+Carbon

- Whole number** of LS-Dyna material models is available through **userdefined material cards**

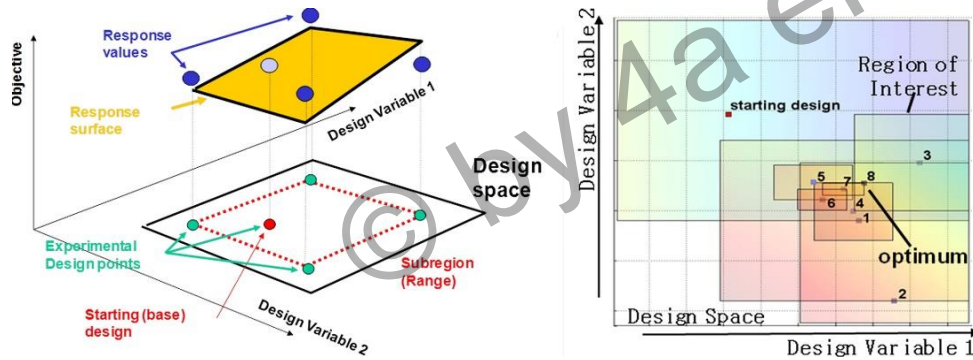
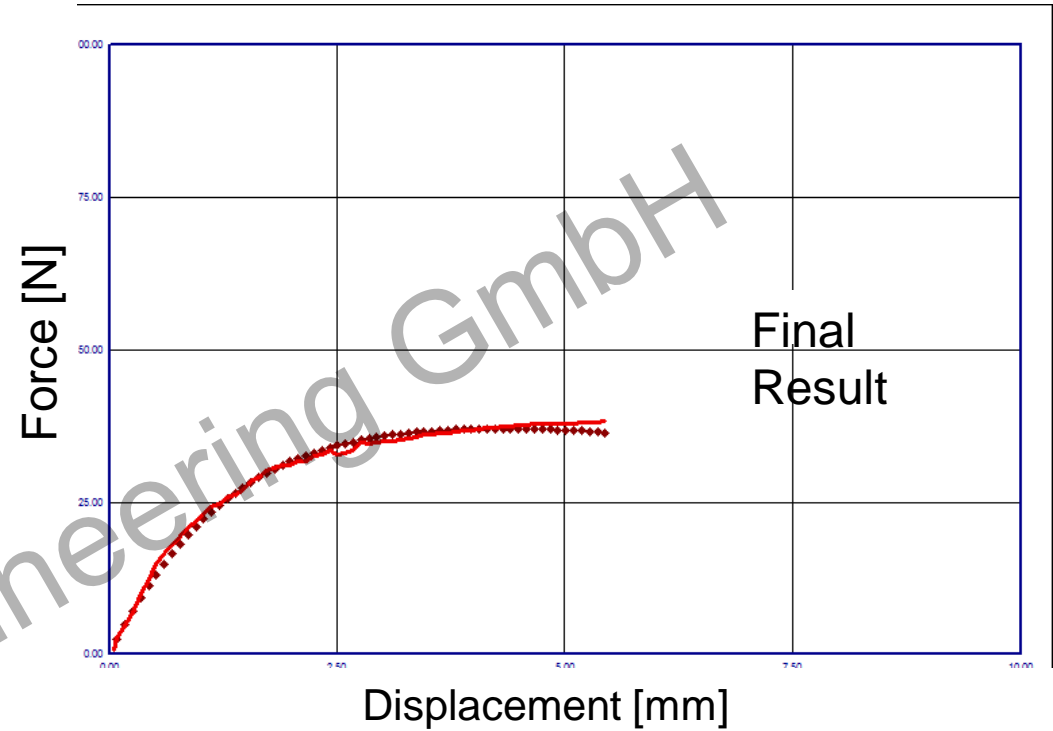
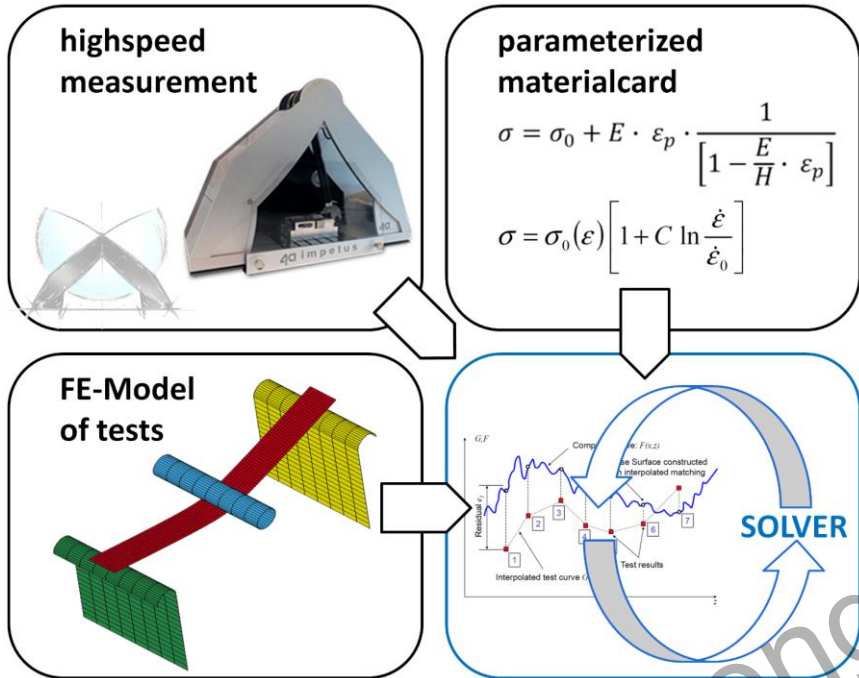
Efficient dynamic testing



IMPETUS

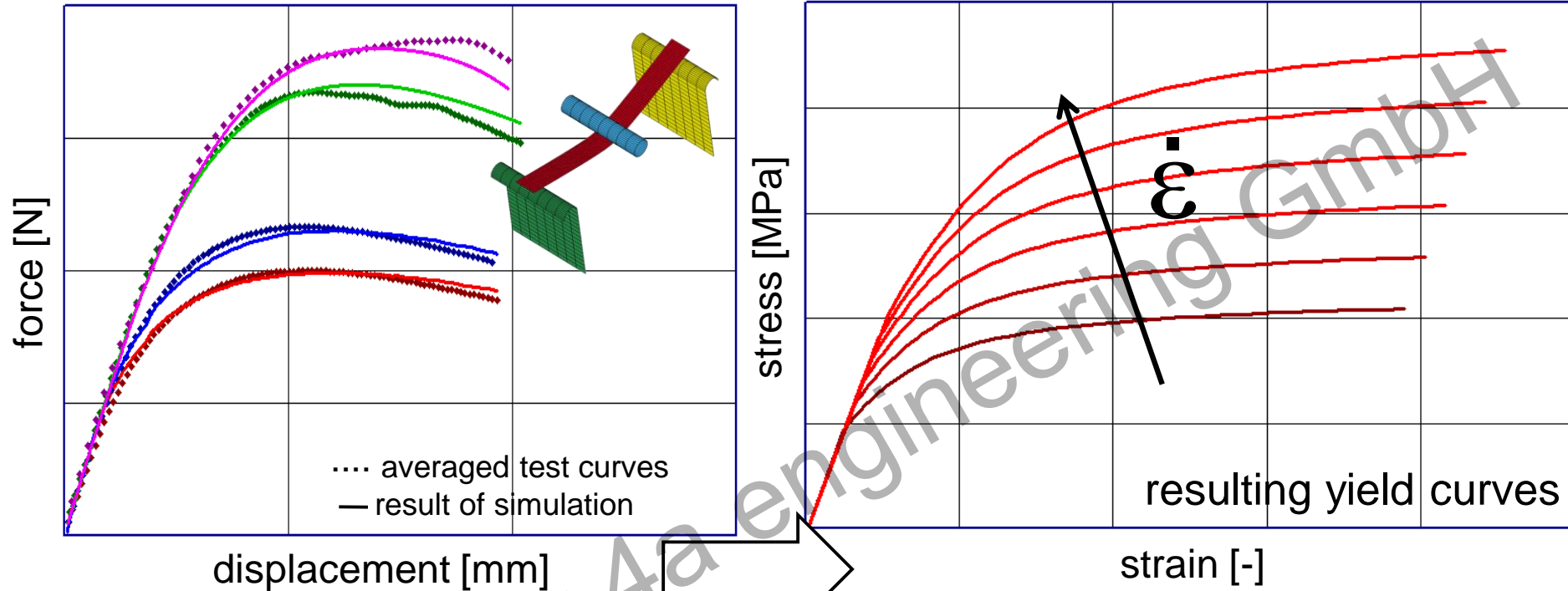
Universal static testing

Reverse engineering

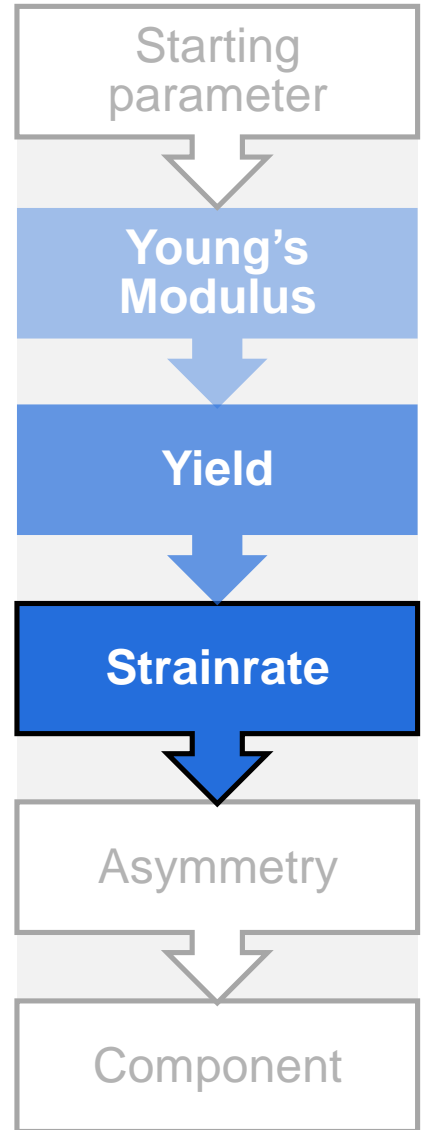
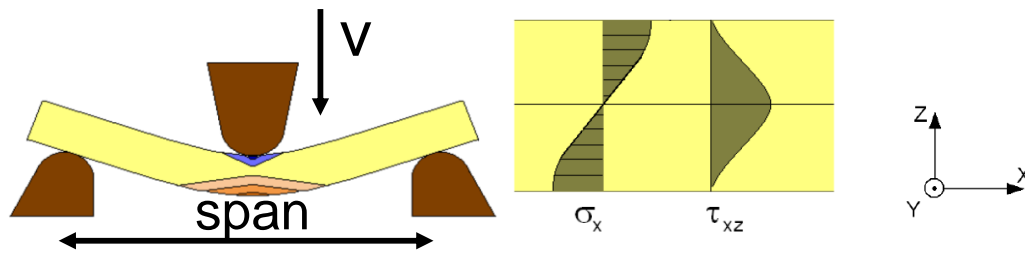


Source: Dynamic Material Characterization Using 4a impetus – PPS Conference 2015, Graz

From bending → *MAT_024



v [m/s]	span [mm]
0.0001	40
0.001	40
1	40
4	40



Intelligent reliable solutions for plastics, composites, metals, foams, ...



VALIMAT

- manage test results
(import, export, filter, evaluation)
- statistics
- automatic report
- material card generation
- material card validation

for all material types

from test to validated material cards



IMPETUS

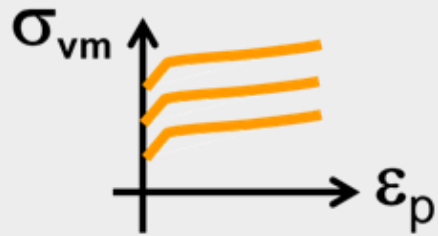
- single pendulum up to 4.5 m/s
- double pendulum up to 8 m/s
- standard test methods
- specialized test methods
- component testing
- advanced measurement

efficient dynamic testing

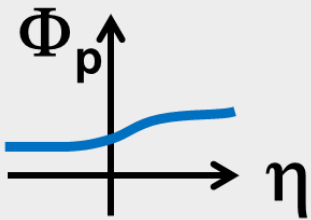
plastics and composites

Intelligent reliable solutions for plastics, composites, metals, foams, ...

✓ VALIMAT



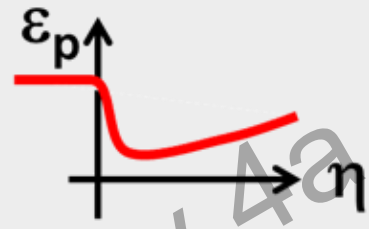
Hardening



Triaxiality



Anisotropic

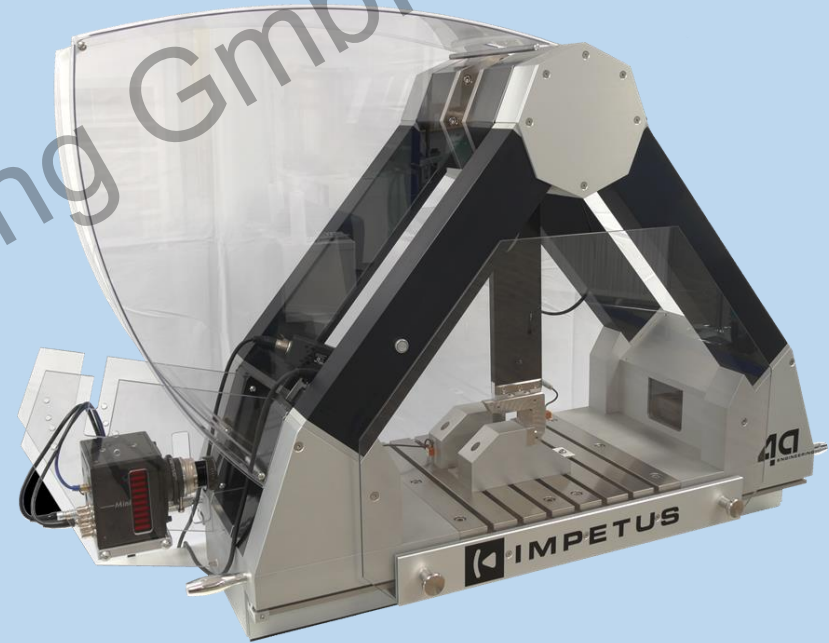


Damage/Failure

for all material types

from test to validated material cards

◀ IMPETUS



efficient dynamic testing

plastics and composites



IMPETUS

<http://impetus.4a.at>



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<http://valimat.4a.at>



YOUTUBE CHANNEL

