Beyond FEM: The Element-Free Galerkin Method

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About me

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- M. Sc. in Computational Mechanics (COMMAS) at University of Stuttgart
- Ph. D. at Institute of Applied Mechanics (civil engineering)
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Outline

Introduction

- Element-Free Galerkin (EFG) Method
- EFG Usage in LS-DYNA
- Application Example
- Summary



Introduction

- LS-DYNA The Multiphysics Solver using a one-code strategy
 - Efficient multi-physics
 - Multi-stage problems
 - Massively parallel







Numerical method are needed to solve space and time-dependent partial differential equations,
 e. g. the momentum balance in structural mechanics

 $\rho \ddot{\mathbf{u}} = \operatorname{div} \mathbf{T}(\mathbf{u})$

- In general, numerical methods are based on space- and time-discretization schemes
 - Space discretization accounts for spatial changes
 - Time discretisation accounts for temporal changes
- Spatial discretisation methods, e. g.,
 - Finite-Element Method (FEM)
 - Smoothed Particle Hydrodynamics (SPH)
 - Element-Free Galerkin (EFG) Method
- Time discretization methods, explicit or implicit, e. g.
 - Central Difference Method
 - Newmark Scheme



- Finite-Element Analysis (FEA) fails at large element distortions
 - → Use of particle-based (mesh-free) spatial discretization methods for continua
 - Smoothed Particle Hydrodynamics (SPH)
 - Element-Free Galerkin (EFG) Method
 - Smooth Petrov Galerkin (SPG) Method

 $d_{\rm int} > d_{\rm crit}$

- EFG is a continuum- and particle-based spatial discretization method
- Discrete particle method (DEM) versus continuum-based particle method (CBPM)



Finite-Element Analysis



Element-Free Galerkin

In DEM, discrete particles interact via contact laws

 $0 < d_{\rm int} \leq d_{\rm crit}$

 $d_{\rm int} \leq 0$

Domain of interest

In CBPM, particles serve as computational points for field variables inside of a continuum

- Basic EFG concept
 - Decomposition of the domain of interest into material particles and a support domain similar to SPH
 - Polynoms to approximate field variables similar to shape functions in FEM
 - Usage of background mesh to integrate the weak forms

$$\rho \ddot{\mathbf{u}} = \operatorname{div} \mathbf{T}(\mathbf{u}) \qquad \qquad \int_{\Omega_e} \rho \ddot{\mathbf{u}} \cdot \delta \mathbf{u} \, \mathrm{d}\Omega + \int_{\Omega_e} \operatorname{grad} \, \delta \mathbf{u} \cdot \mathbf{T} \, \mathrm{d}\Omega - \int_{\partial\Omega_e} \delta \mathbf{u} \cdot \mathbf{t} \, \mathrm{d}a = 0$$

Approximating polynoms are constructed from monomials with their parameters minimized inside support domain through Moving Least Squares (MLS)

$$\begin{split} u^{h}(\mathbf{x}) &= \mathbf{H}^{T}(\mathbf{x}) \ \mathbf{b}(\mathbf{x}) = \sum_{i=1}^{n} H_{i}(\mathbf{x}) b_{i}(\mathbf{x}) \\ \text{with } \mathbf{b}(\mathbf{x}) & \text{coefficient vector} \\ \mathbf{H}^{T}(\mathbf{x}) & \text{vector of monomials, i. e. } \mathbf{H}^{T}(\mathbf{x}) = [1, x, x^{2}, ..., x^{n}]^{T} \end{split}$$



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- Remarks on the background-mesh integration
 - Advantages
 - Definition of the physical domain
 - Usage of various contact types
 - Application of **boundary conditions**
 - Volume integration via "stress points"
 - Disadvantages
 - Mesh distortion issue
 - Difficult failure analysis





current configuration

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Remarks on the support domain, i. e. EFG Kernel Function

Lagrangean Kernel

- Support is defined in the initial configuration
- Support covers the same set of material points throughout time

Eulerian Kernel

- Support is defined in the current configuration
- Support covers different material points throughout time

Semi-Lagrangean Kernel

- Support is defined in the current configuration
- Support covers the same number of material points throughout time



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support domain



initial configuration

deformed configuration



EFG + Lagrangean Kernel



EFG + semi-Lagrangean Kernel



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EFG in LS-DYNA

- Implementation features
 - Explicit and implicit time integration
 - Thermal coupling
 - Adaptive and remeshing strategies
- Activating an EFG analysis in LS-DYNA
 - Create your FE model as usual
 - Replace *SECTION_SOLID by *SECTION_SOLID_EFG
 - LS-PrePost particle representation
 - **Go to FEM \rightarrow Model and Part** \rightarrow Appearance
 - Tick the check boxes Sphere" and Shrn
 - Click the EFG part
 - Modify particle visualization in Settings → General Settings







Keyword *SECTION_SOLID_EFG

*SECTION_SOLID_EFG									
\$	-+1	+2	+3	4	+5	+6	-+7	+8	
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- secid section identifier
- elform element type of background mesh: EQ.41: EFG solid (TET, HEX, PENT mesh) EQ.42: EFG solid (TET mesh)

(SMP & MPP, implicit and explicit analysis and thermal-mechanical coupling available from R5 on upwards)



Keyword *SECTION_SOLID_EFG

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dx, dy, dz normalised dilatation parameter in x, y and z direction, respectively, where 1.0 < dx, dy, dz < 1.6 are recommended \rightarrow the higher the slower the performance

	regular mesh	irregular mesh
Foam	1.0 ~ 1.2	1.0 ~ 1.2
Metal	1.2 ~ 1.4	1.0 ~ 1.2
Fluid or EOS	1.4 ~ 1.6	1.2 ~ 1.4



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Keyword *SECTION_SOLID_EFG

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ispline choice of kernel function

- EQ.0: Cubic spline function (rectangular support dx, dy, dz)
 - with linear base function (default)
- EQ.1: Quadratic spline function (rectangular support with dx, dy, dz)
- EQ.2: Cubic spline function (circular support),
 - where dx defines radius coefficient
- EQ.10: Cubic spline function with bilinear base function (rectangular support with dx, dy, dz)





Keyword *SECTION_SOLID_EFG

*SECTION_SOLID_EFG									
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idim Integration of the weak forms within the spatial domain

EQ. 1: Local boundary condition method

EQ. 2: Gauss integration (default)

EQ.-1: Stabilized EFG method (PENT and HEX background mesh only)

- One-point integration scheme + gradient type hourglass control
- Designed especially for foam and rubber materials
- Computational cost is between reduced integration FEM and full integration FEM
- EQ.-2: Fractured EFG method (TET background mesh and SMP only)



Keyword *SECTION_SOLID_EFG



- toldef Deformation tolerance for the activation of adaptive EFG Semi-Lagrangian and Eulerian kernel
- Apply pressure smoothing by adding slight compressibility to the material EQ. 0: No pressure smoothing (default)
 - EQ. 1: Moving-least squared pressure recovery (only for ELFFORM=42)
 - there is numerical instability in contact ("hard contact")
 - Implicit analysis has convergence problem





- Mesh-adaptivity/Remeshing in LS-DYNA
 - Basically follows the remeshing keywords as in FEA (check out our forming class for more informations)
 - However, with some extensions merely regarding EFG

*Part									
\$	+1	+2	-+3	+4	-+5	-+6	+7	+8	
\$#	pid	secid	mid	eosid	hgid	grav	adpopt	tmid	
	1	1	1				2		

adpopt activate remeshing

- LT.0: adaptive remeshing for 2-D solids, adpopt gives the load curve ID that defines the element size as a function of time
- EQ.0: adaptive remeshing is inactive for this part ID (default)
- EQ.1: h-adaptive for 3-D shells.
- EQ.2: adaptive remeshing for 2-D solids, 3-D tetrahedrons and 3-D EFG
- EQ.3: axisymmetric r-adaptive remeshing for 3-D solid
- EQ.9: passive h-adaptive for 3-D shells. The elements in this part will not be split unless their neighboring elements in other parts need to be split more than one level.



- Mesh-adaptivity/Remeshing in LS-DYNA
 - Basic remeshing parameters apply from FEA also apply to EFG



adpfreg Time interval in which LS-DYNA checks the remeshing criteria, e.g. adpene

lcadp Time interval between remeshing criteria-checks over time via *DEFINE_CURVE (overwrites adpfreg)

- adpene For shells (h-adaptive):
 - GT.0: adaptivity takes place when the forming contact surfaces are approaching

LT.0: adaptivity takes place when the forming contact surfaces are penetrating

The refinement generally occurs before contact takes place and the refinement is based on the curvature of the tooling

For 3-D solids (r-adaptive):

GT.0: the mesh refinement is based on the curvature of the tooling



- Mesh-adaptivity/Remeshing in LS-DYNA
 - Similar to ***CONTROL_REMESHING** for FEA, however, with the additional card 2 and 3 for EFG exclusively



rmin/rmax Minimum/Maximum edge length for the surface mesh surrounding the parts which should be remeshed

ivtInternal variable transfer in adaptive EFGEQ.1: Moving Least square approximation with Kronecker-delta property (recommended in general case)EQ.-1: Moving Least square approximation without Kronecker-delta propertyEQ.2: Partition of unity approximation with Kronecker-delta propertyEQ.-2: Partition of unity approximation without Kronecker-delta propertyEQ.-3: Finite element approximation



Mesh-adaptivity/Remeshing in LS-DYNA

Additional to predefined adaptivity steps (see <a href="mailto:adaptive-ada





Mesh-adaptivity/Remeshing in LS-DYNA



mm Interactive adaptive remeshing with monotonic resizing EQ.1: The adaptive remeshing cannot coarsen a mesh the current implementation only supports ist = 1, 2, 3 and isr = 0

- iat<1,2,3> Tolerance for interactive adaptivity for ELFORM=42, e.g.
 - -iat1 shear strain
 - -iat2 max.-to-min. element edge ratio
 - -iat3 volume-change tolerance



Mesh-adaptivity/Remeshing in LS-DYNA

adpene=0, mm=0 rmin has no effect, rmax=1.25





adpene=0, mm=1 rmin has no effect, rmax=1.25









Overview



Bulk forming



Self-piercing rivet

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Overview





Modelling of a sheet-molding compound (with courtesy of JSOL)





- Process simulation requires
- Remeshing
- Thermal Coupling
- Beam-Fiber coupling



Modelling of a sheet-molding compound (with courtesy of JSOL)







- Modelling of a sheet-molding compound (with courtesy of JSOL)
 - Large deformations of the fiber-matrix compound via Element-Free Galerkin (EFG)
 - Fiber-matrix interaction via ***CONSTRAINED_BEAM_IN_SOLID** (CBIS)
 - Fiber-fibre interaction (fibre network) through ***CONTACT_AUTOMATIC_GENERAL**

fiber-matrix compound





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Modelling of a sheet-molding compound (with courtesy of JSOL)



Modelling of a sheet-molding compound



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Summary

- Available for explicit and implicit time-integration schemes
- **EFG** more **suitable for large deformations** compared to FEA, e. g.
 - Forging
 - Cutting
- **Remeshing** extents an even wider range of application but
 - Geometry is slightly changed
 - Contact force might be reduced
 - Part of the solution is lost due to variable transfer
 - → Trigger as few remeshing steps as possible!
- Thermal coupling possible
- However, in general, EFG is
 more computational expensive than FEA







Thank you for your attention!

LS-DYNA

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