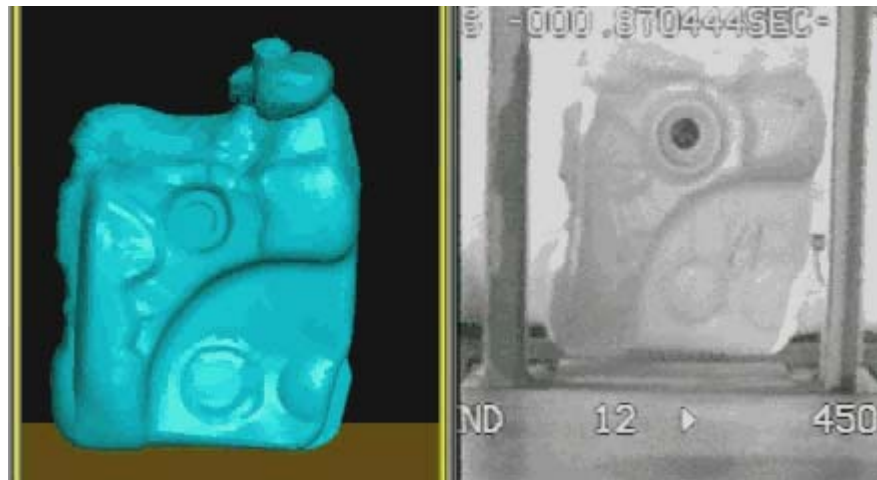


# Einfluss der Materialmodellierung von thermoplastischen Kunststoffen auf Ergebnisse von numerischen Falltests



## ■ Motivation

- Was ist das besondere an einer Falltestsimulation?
- Erfahrungen aus der Praxis → Fallstricke

## ■ Materialverhalten von Kunststoffen – BASF ULTRASIM™

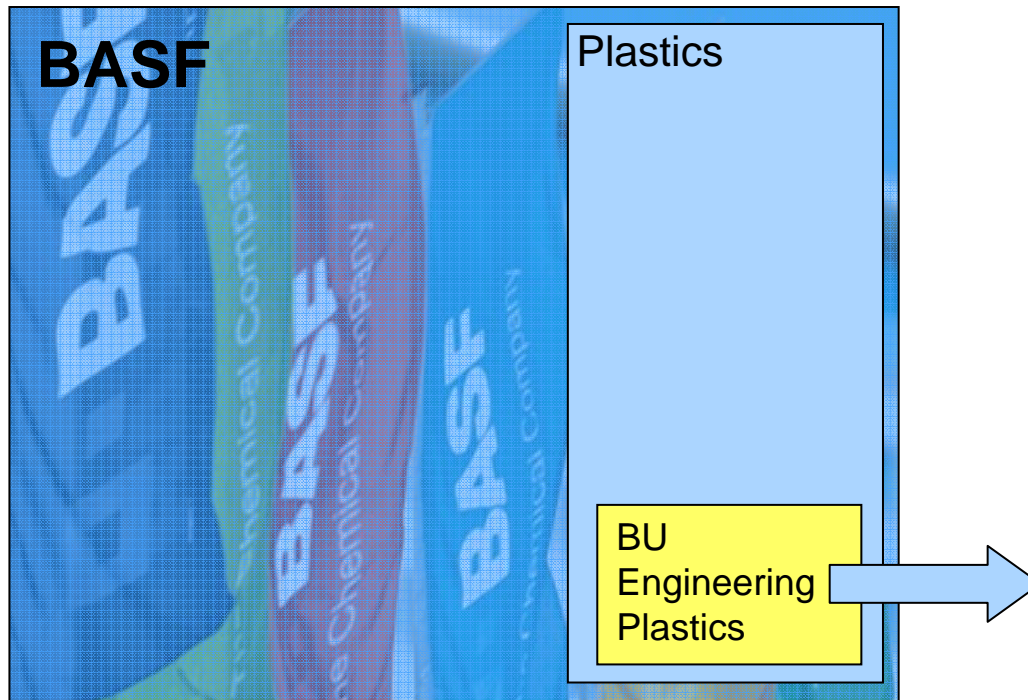
- Faserorientierung
- Dehnratenabhängigkeit
- Asymmetrie in Zug-Druck
- Anisotropie
- Versagensmodellierung

## ■ Ausgewählte Beispiele

## ■ Diskussion

# BASF and CAE?

## BASF – The Chemical Company



### ***Thermoplastic Materials*** + Customer Support:

- 
- Application Development Services
  - Material Modelling
  - Mechanical Analyses
  - Filling Analyses
- 
- 

**CAE**

## ■ Was ist das besondere an einer Falltestsimulation?

- Kinematisch anspruchsvoll

- Kontaktabbildung, Postprocessing

## ● Simplifikationen sind erschwert!

- Verbindungsmodellierung (Schrauben, Kleben, ...)

## ● Abbildung von Material und Versagen ist eine zentrale Aufgabe

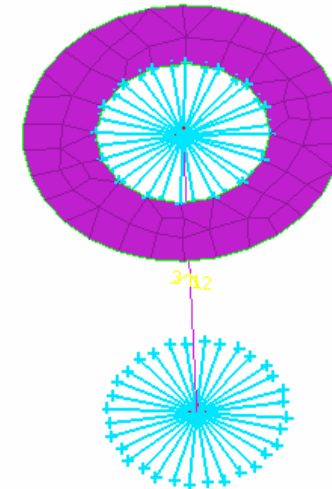
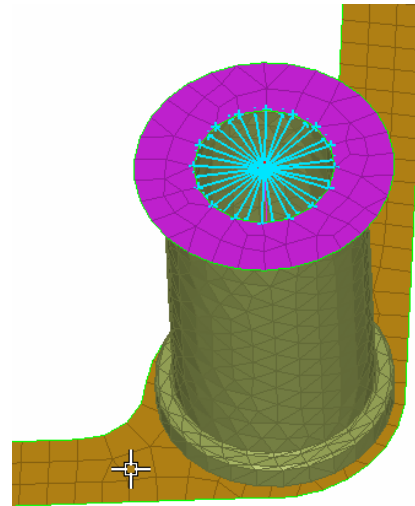
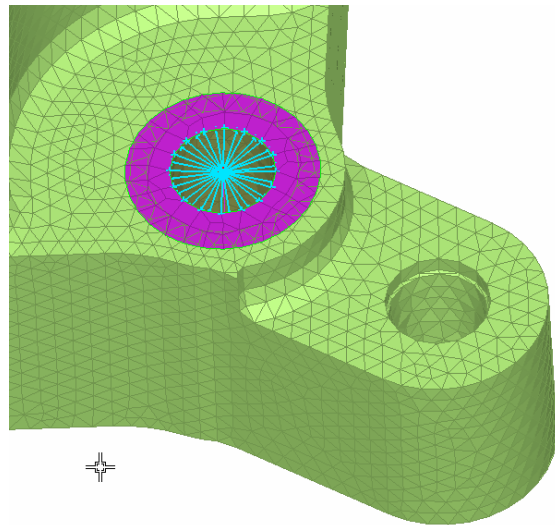
- Nichtlinearitäten, Anisotropie, ...

## ● Lokale Größen dominieren

- Netzfeinheit und Netzgüte

- - Resultat Absenkung → Steifigkeit → globale Größe
  - Resultat Versagen → Failure-Wert → lokale Größe

# Vereinfachung Schraube

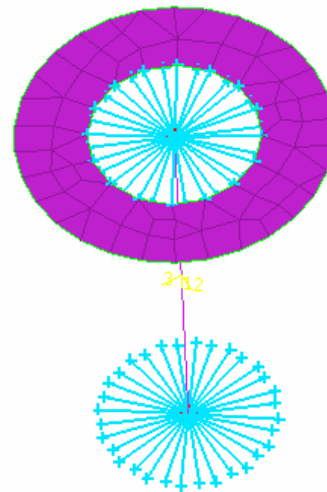
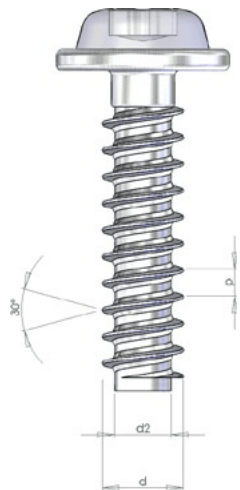
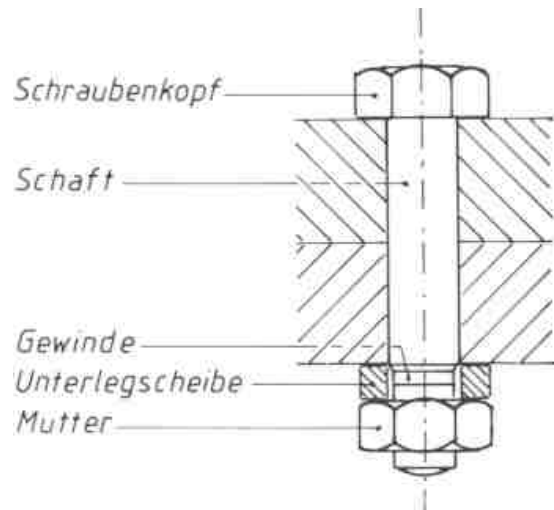


Schraube ist geometrisch nicht vorhanden!

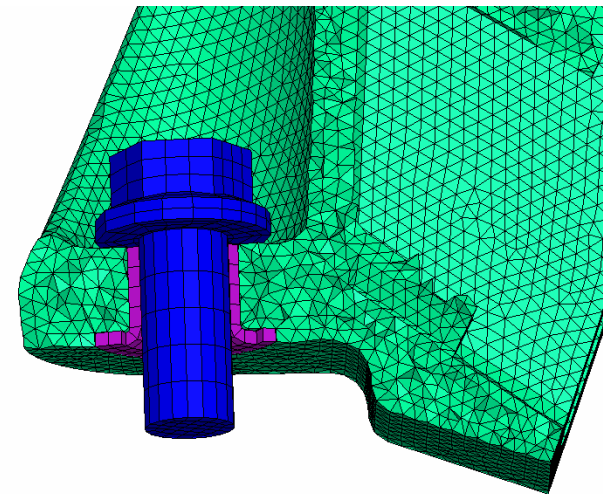
Probleme:

- Krafteinleitung
- was passiert nach dem Versagen?

# Vereinfachung Schraube



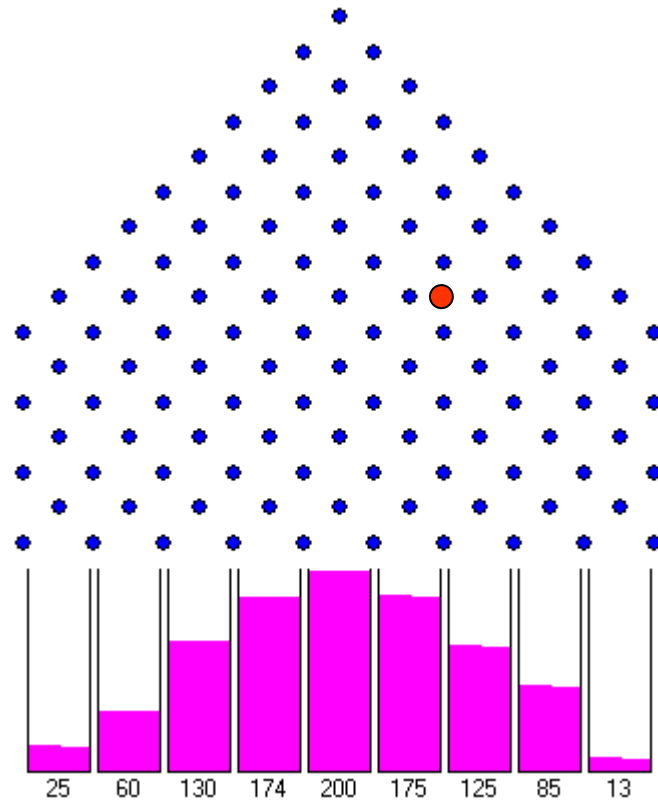
vereinfacht



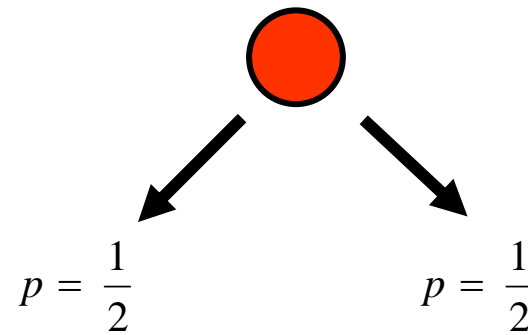
geometrisch korrekt

Gefahr: Bifurkation durch nichtphysikalisches Verhalten  
Lösung schlägt einen anderen Pfad ein!

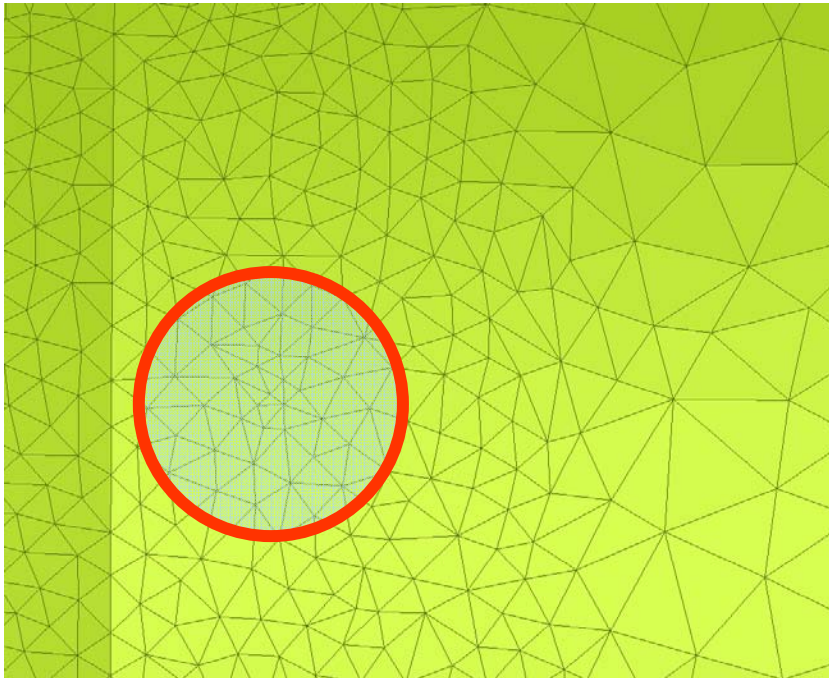
# Galton Brett Pfadabhängigkeit



Bifurkation (Gabelung)





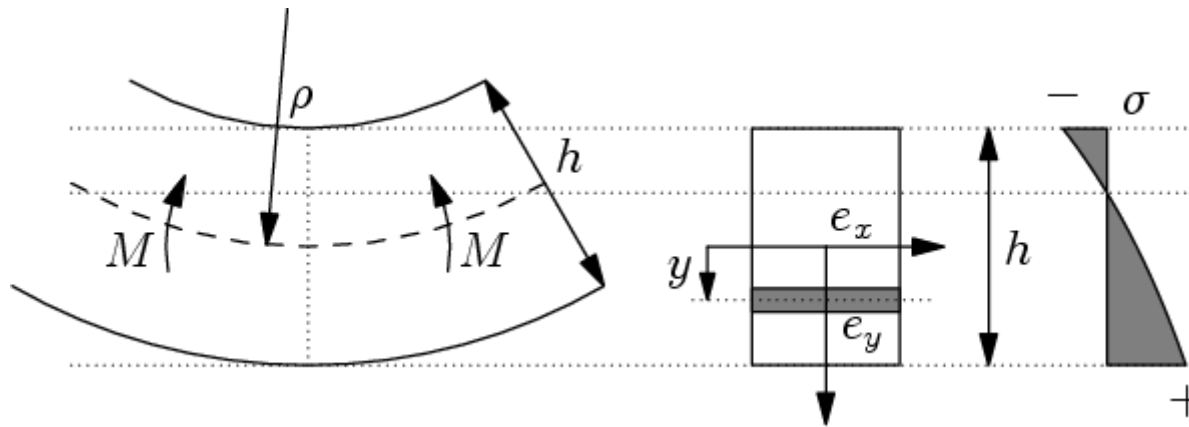


Resultat Absenkung → Steifigkeit →  
globale Größe  
Resultat Versagen → Failure-Wert →  
lokale Größe

- Numerischer Einfluss schlechter Elemente kann dominieren
- Solidelemente → Netzchecks im Inneren beachten!

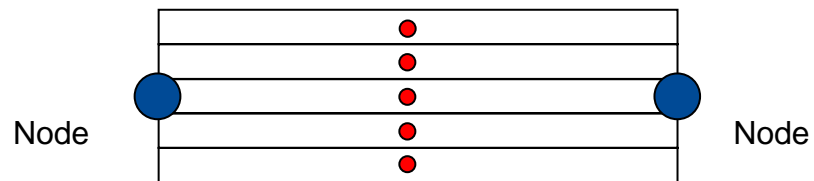


# Netzeinfluss - Netzfeinheit

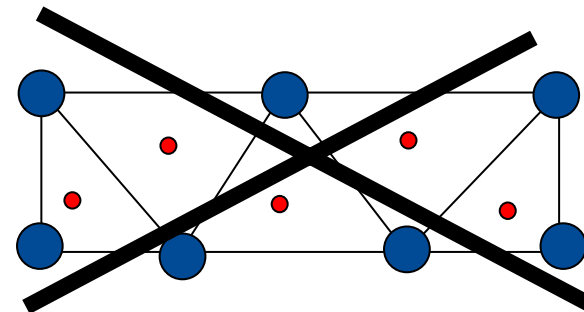


Schale unter Biegung

Shell-Element

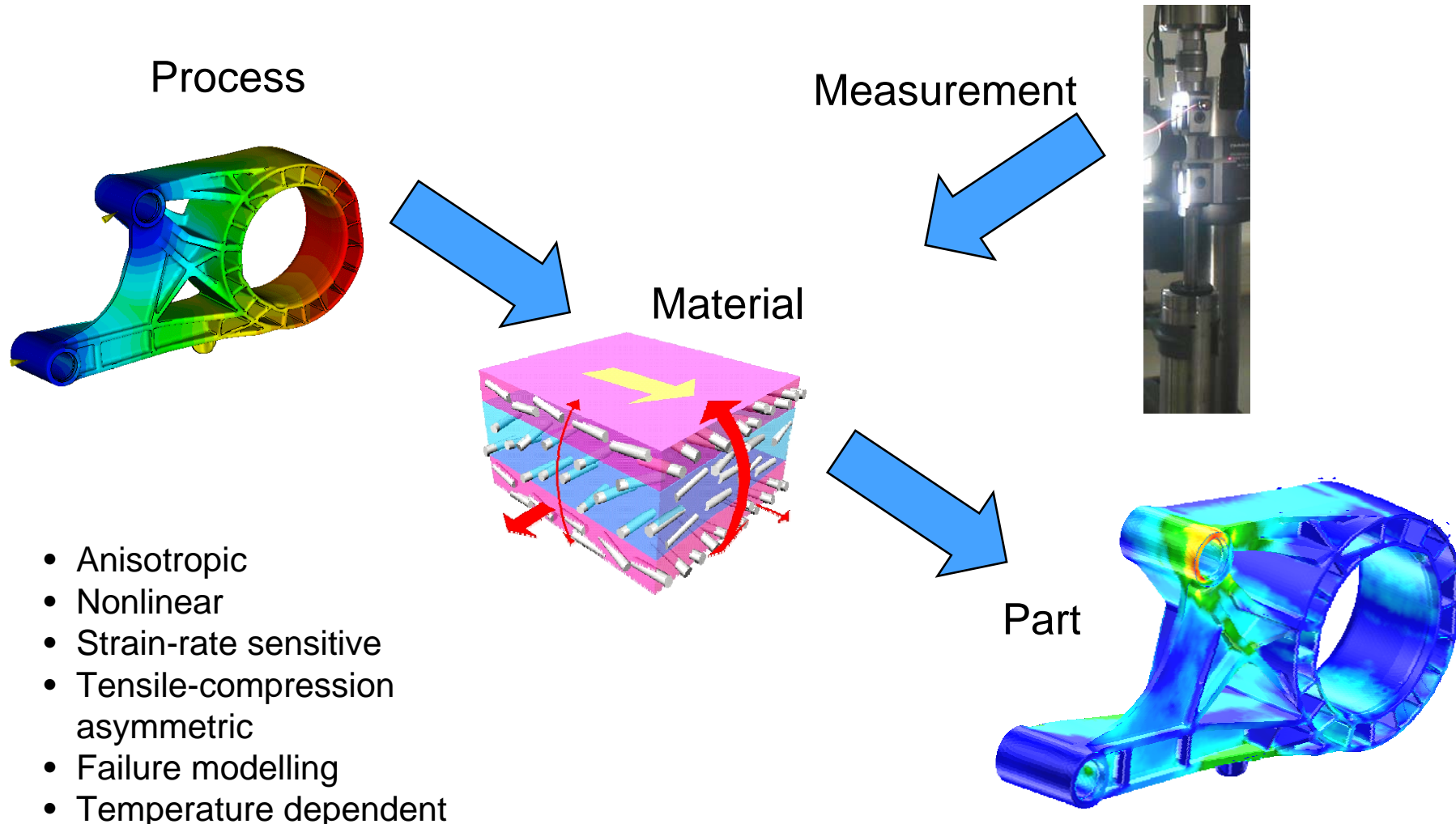


Solid-Element



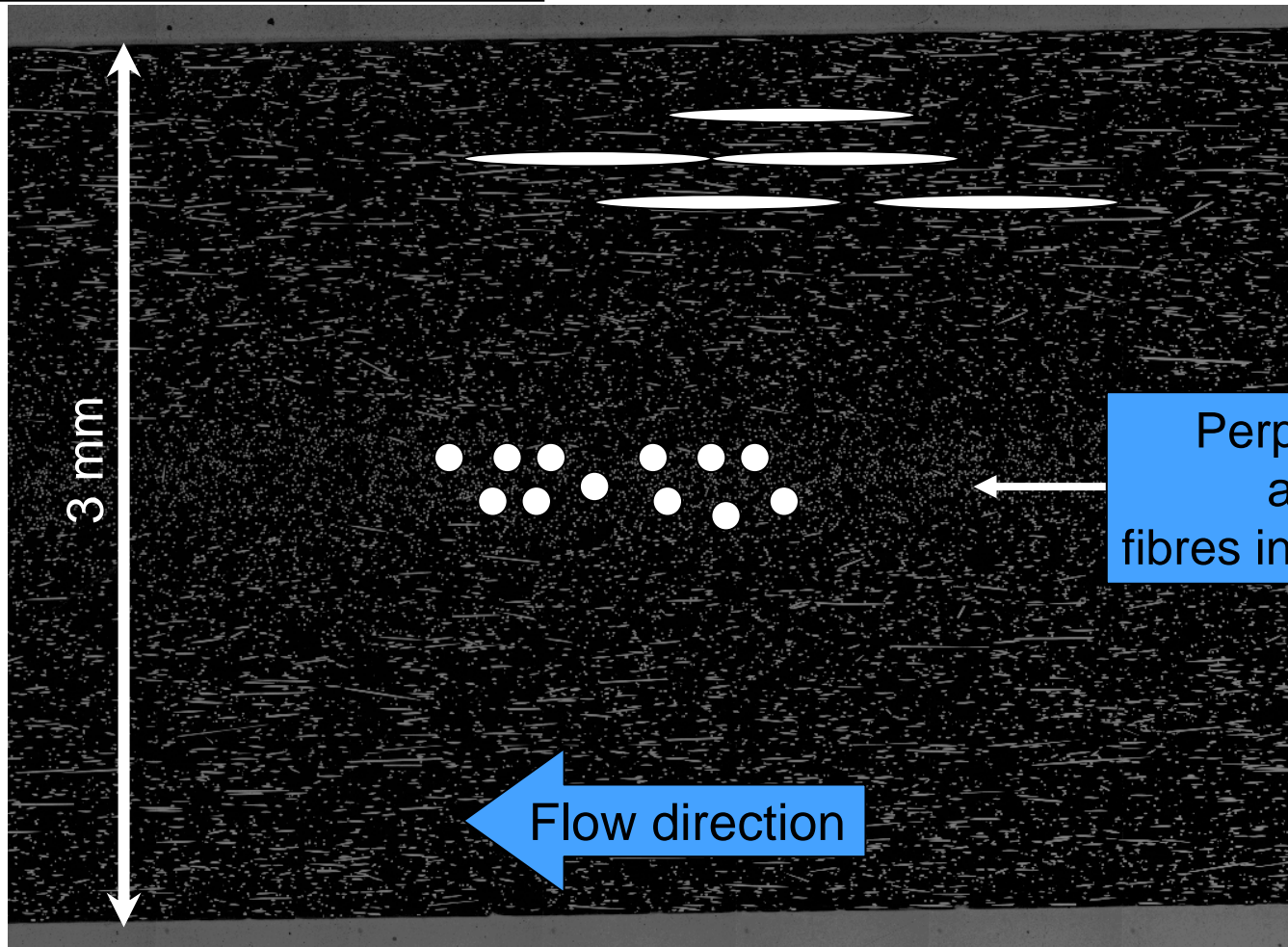
● Integration Point

# Integrative Simulation ULTRASIM™ for short fiber reinforced thermoplastics



# Cross section PA GF30

Flow aligned fibres near tool walls

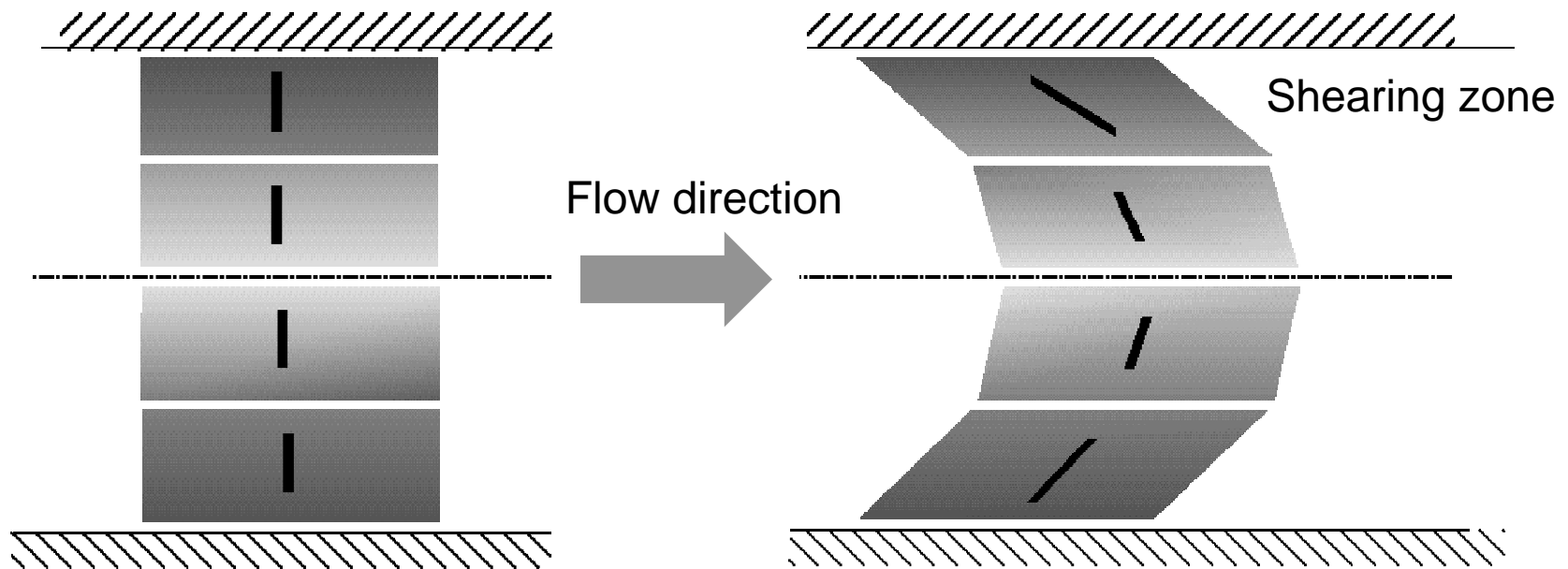


Perpendicular aligned fibres in middle layer

Flow direction

# Evolution of Fiber Orientation in Mould Filling Process

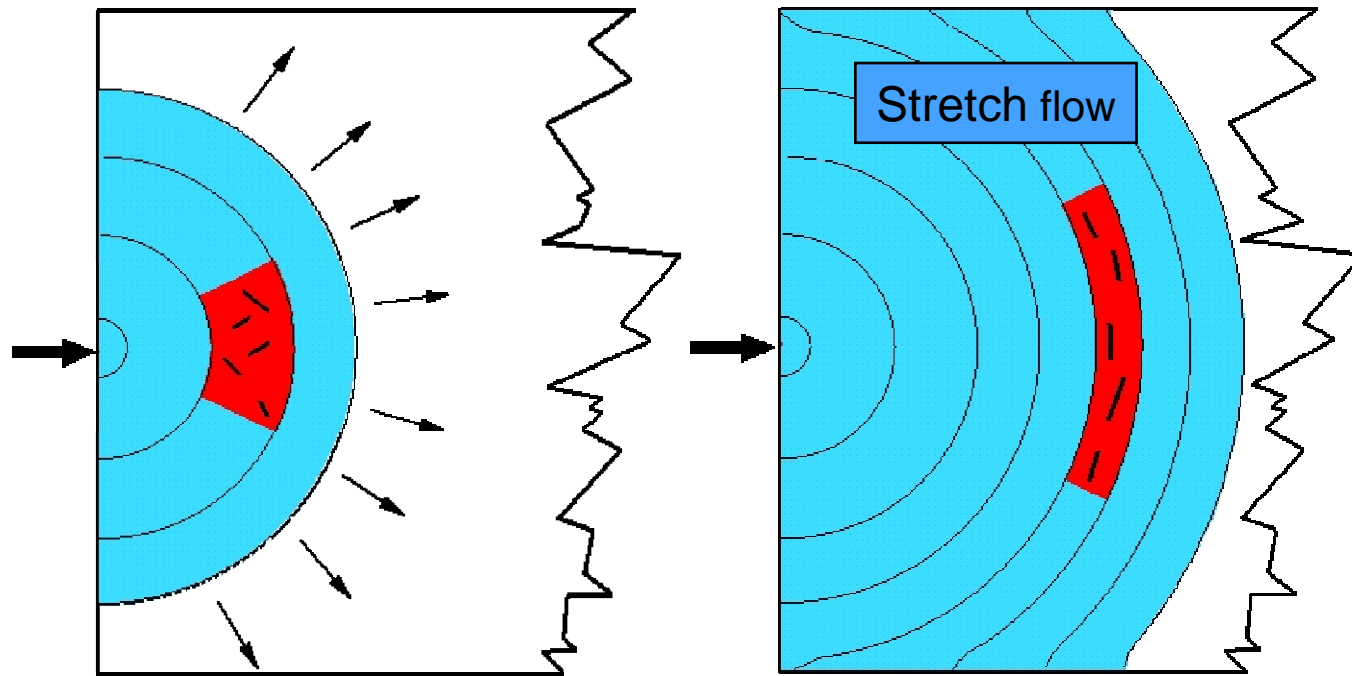
Cross sectional view



Due to shearing in the boundary layers  
the fibers are oriented in flow direction

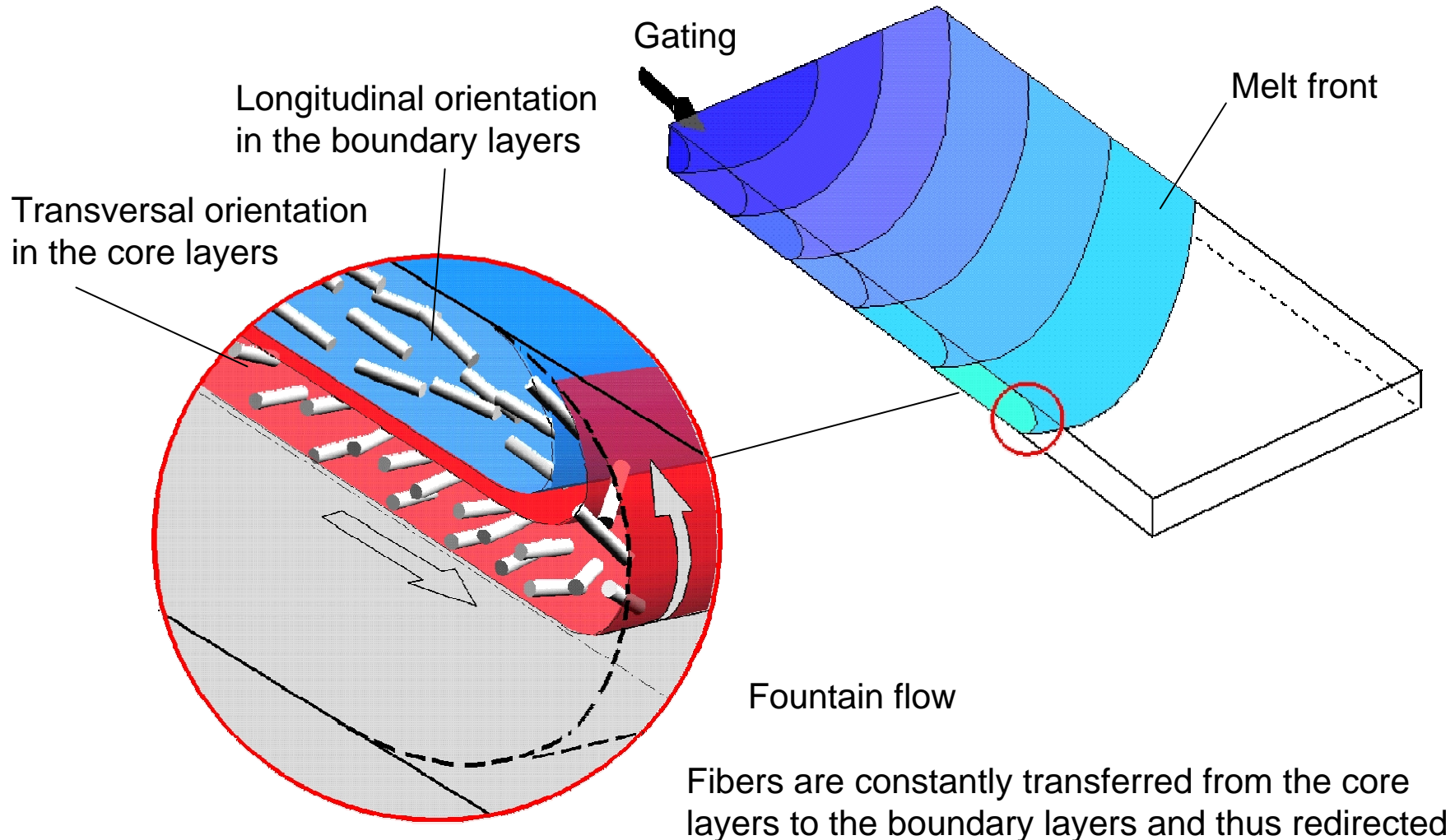
# Evolution of Fiber Orientation in Mould Filling Process

Upper view



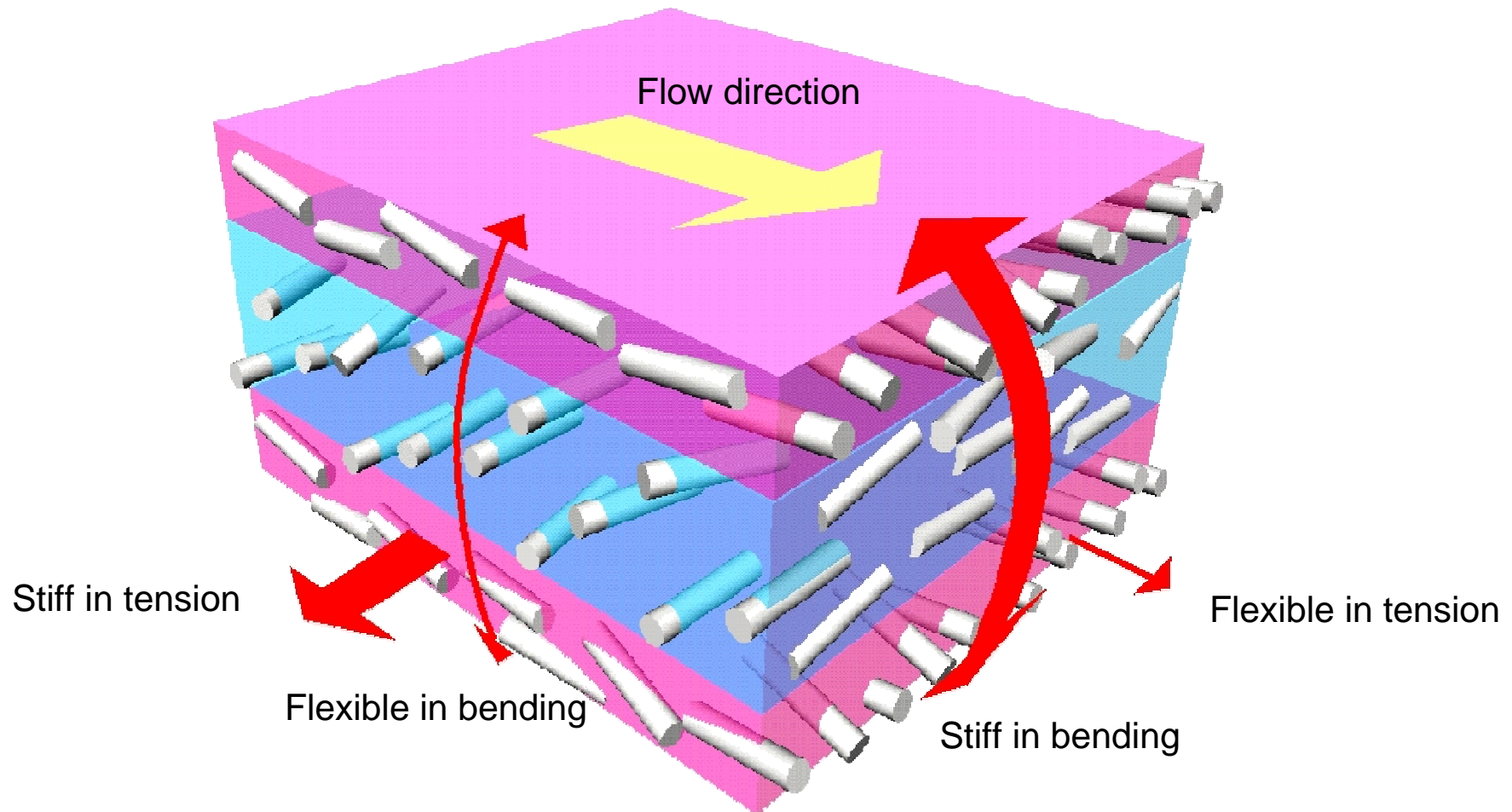
Fibers are being oriented in stretching direction

# Evolution of Fiber Orientation in Mould Filling Process





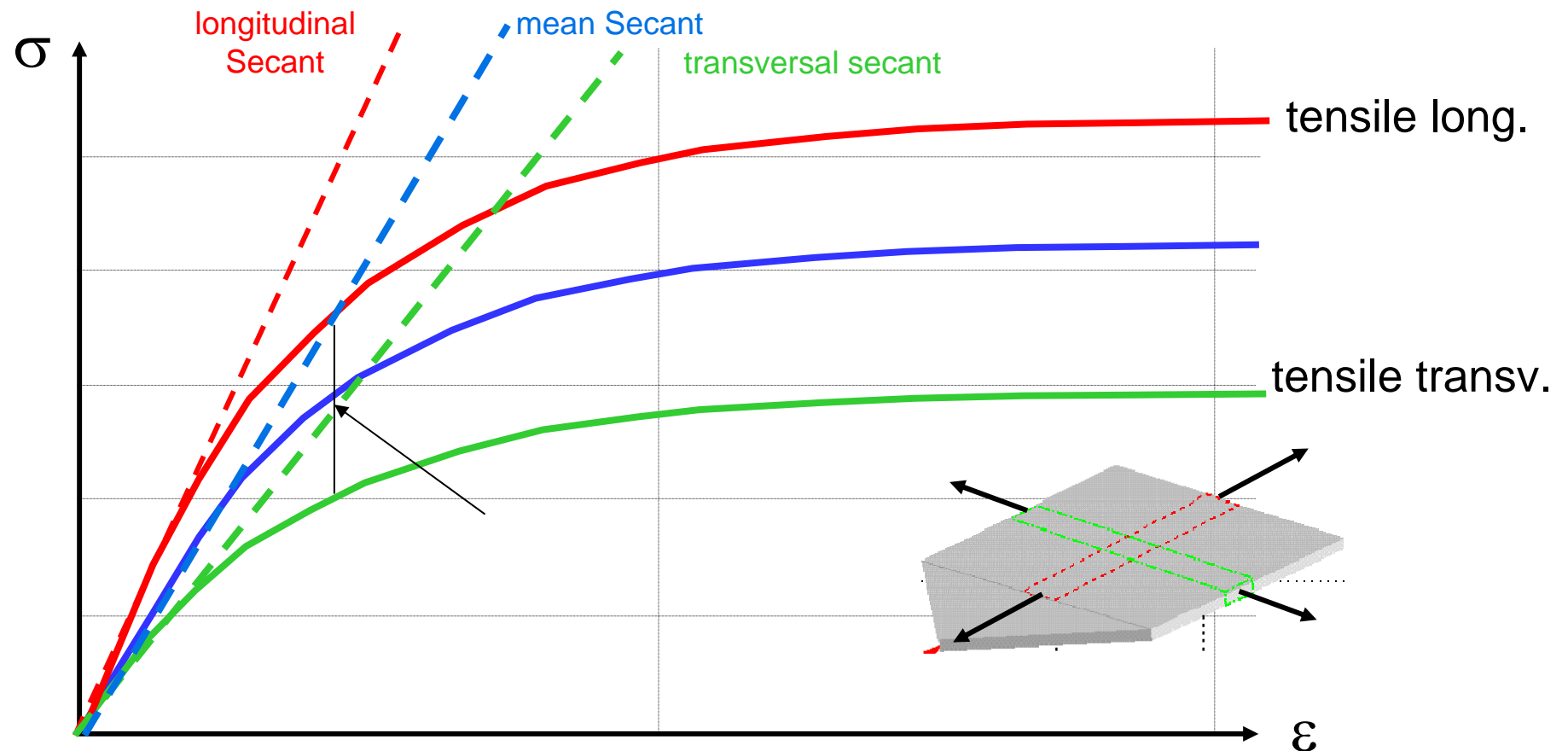
# Mechanical behaviour of anisotropic layered shells





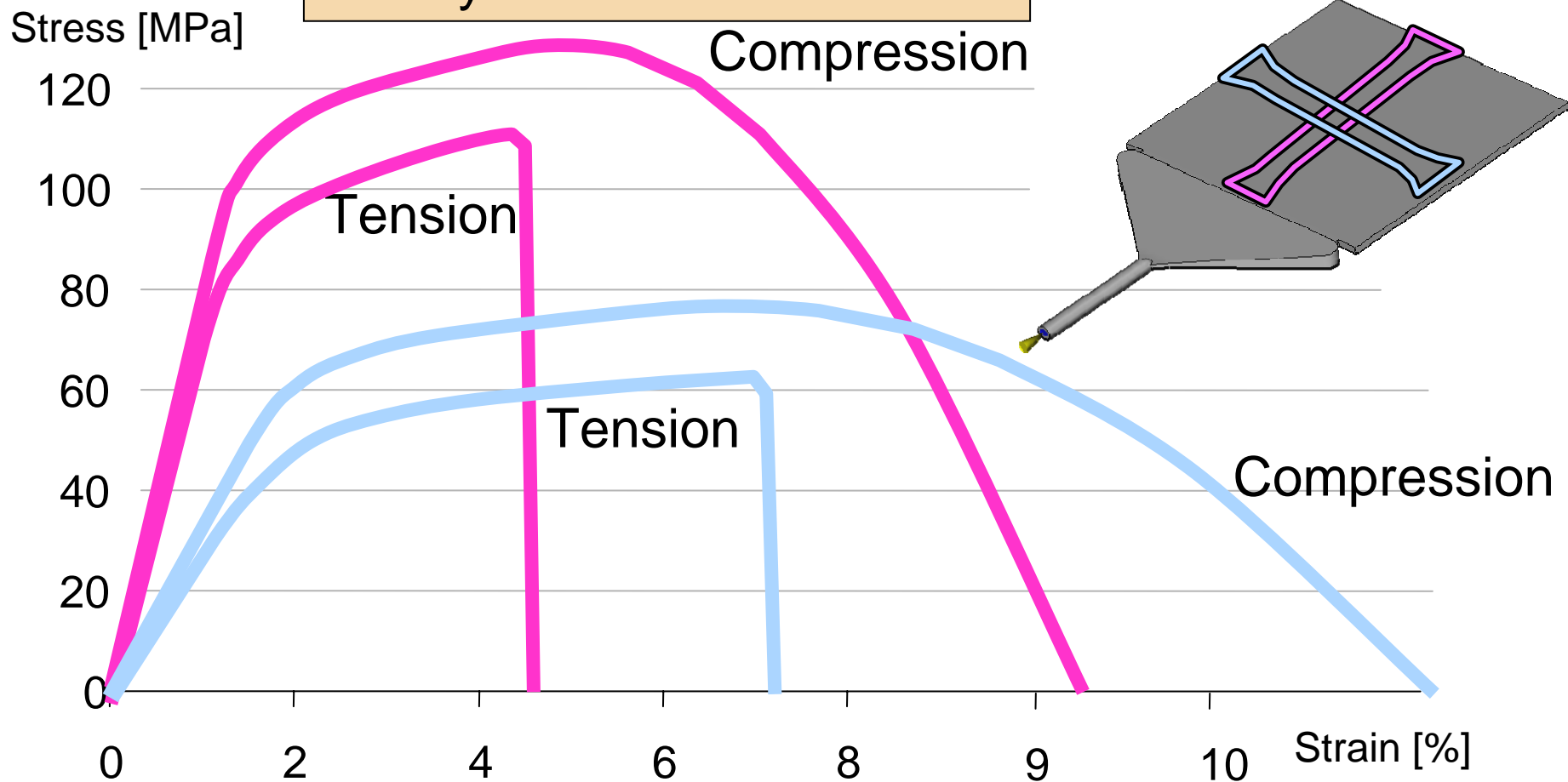
# Motivation for Anisotropic Material Modelling

Anisotropy due to fiber orientation



# Fiber reinforced Polymer, Stress-Strain

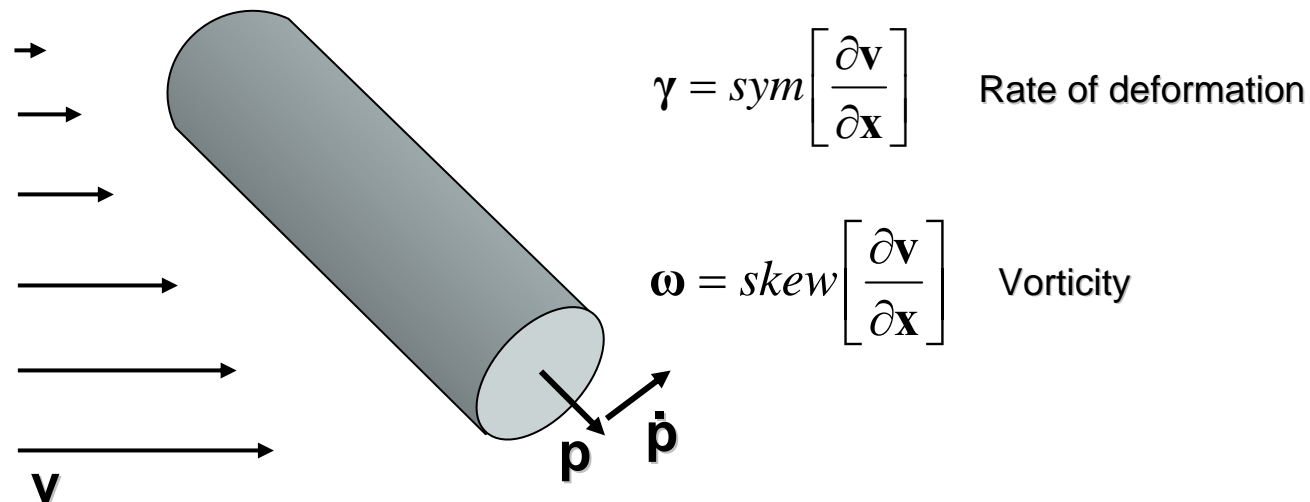
influence: fiber orientation  
and hydrostatic stress state



# Evolution of fiber orientation

Jefferey 1922

$$\dot{\mathbf{p}} = -\boldsymbol{\omega} \cdot \mathbf{p} + \lambda (\boldsymbol{\gamma} \cdot \mathbf{p} - (\mathbf{p} \cdot \boldsymbol{\gamma} \cdot \mathbf{p}) \mathbf{p}) - \frac{D_r}{\psi} \frac{\partial \psi}{\partial \mathbf{p}} \quad ; \quad \lambda = \frac{(l/d)^2 - 1}{(l/d)^2 + 1}$$



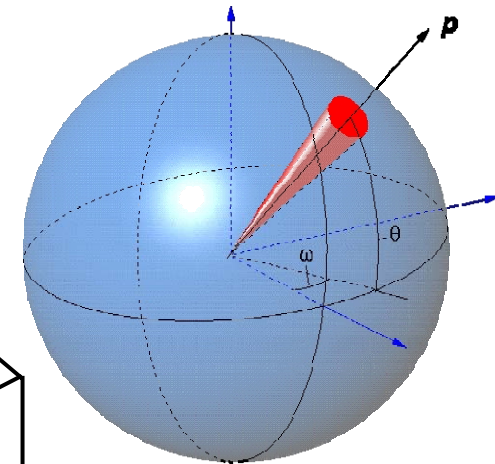
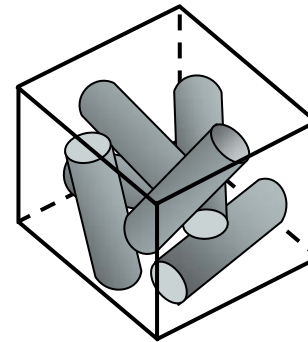
# Orientation distribution function

Orientation tensors

$$\mathbf{a} = \int \mathbf{p} \otimes \mathbf{p} \psi(\mathbf{p}) d\omega$$

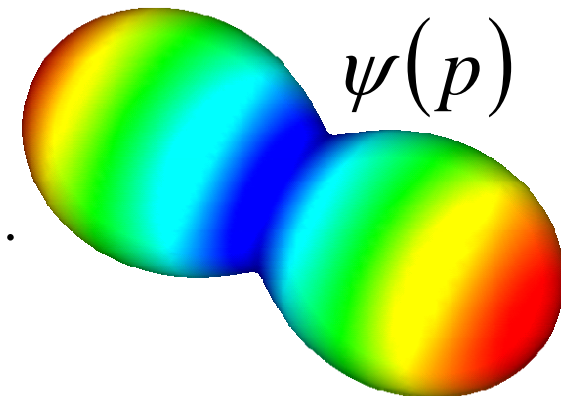
$$\mathbf{a}^4 = \int_{\omega} \mathbf{p} \otimes \mathbf{p} \otimes \mathbf{p} \otimes \mathbf{p} \psi(\mathbf{p}) d\omega$$

(Tucker 1987)



Taylor expansion of ODF

$$\begin{aligned} \psi(\mathbf{p}) = & \frac{1}{4\pi} + \frac{15}{8\pi} + dev(\mathbf{a}) : dev(\mathbf{p} \otimes \mathbf{p}) \\ & + \frac{315}{32\pi} dev(\mathbf{a}^4) :: dev(\mathbf{p} \otimes \mathbf{p} \otimes \mathbf{p} \otimes \mathbf{p}) + \dots \end{aligned}$$



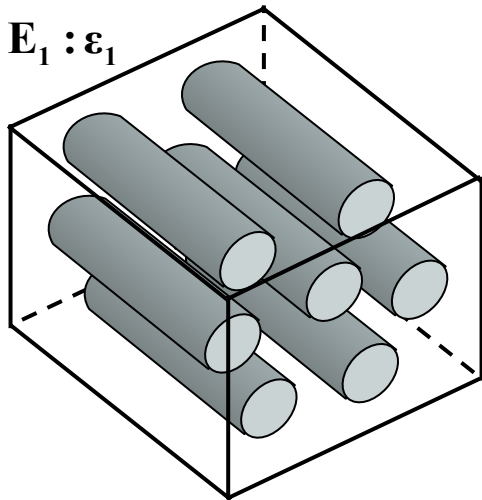
# Homogenization of fibers and polymer

## Mean Field Theory

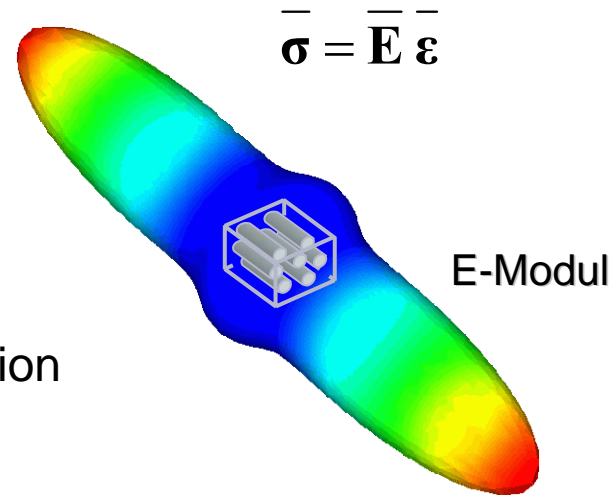
(Mori and Tanaka, Tandon and Weng)

$$\sigma_0 = \mathbf{E}_0 : \varepsilon_0$$

$$\sigma_1 = \mathbf{E}_1 : \varepsilon_1$$



Homogenization



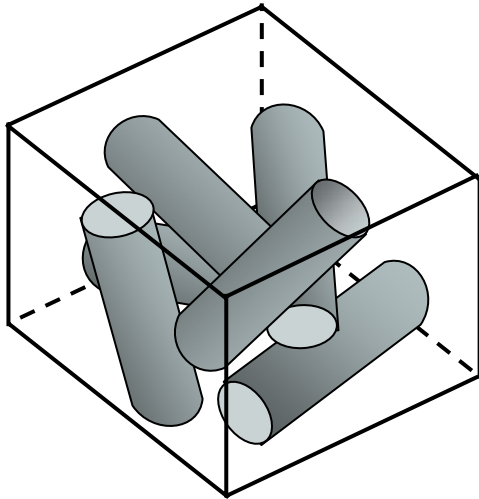
$$\bar{\sigma} = \bar{\mathbf{E}} \bar{\varepsilon}$$

$$\bar{\mathbf{E}} = \left[ c_1 \mathbf{E}_1 : \mathbf{B}^\varepsilon + (1 - c_1) \mathbf{E}_0 \right] : \left[ c_1 \mathbf{B}^\varepsilon + (1 - c_1) \mathbf{I} \right]^{-1}$$

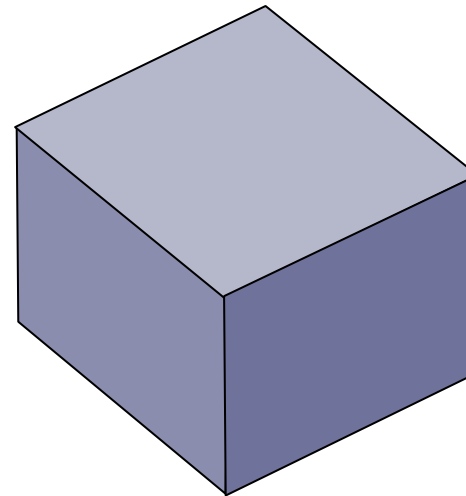
$$\mathbf{B}^\varepsilon = \left( \mathbf{I} + \mathcal{E}_{(I, \omega)} : \left[ \mathbf{E}_0^{-1} : \mathbf{E}_1 - \mathbf{I} \right] \right)^{-1} \quad \mathcal{E}_{(I, \omega)} : \text{Eshelby Tensor}$$

# Material modelling for composite materials

**Micro Scale**



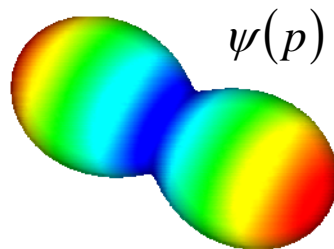
**Macro Scale**



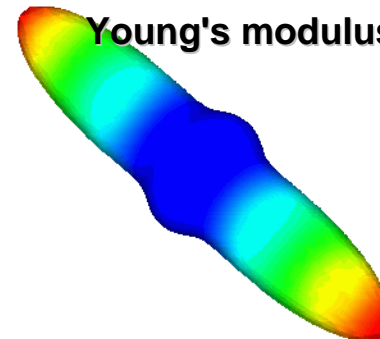
Homogenization:



**Orientation distribution function**

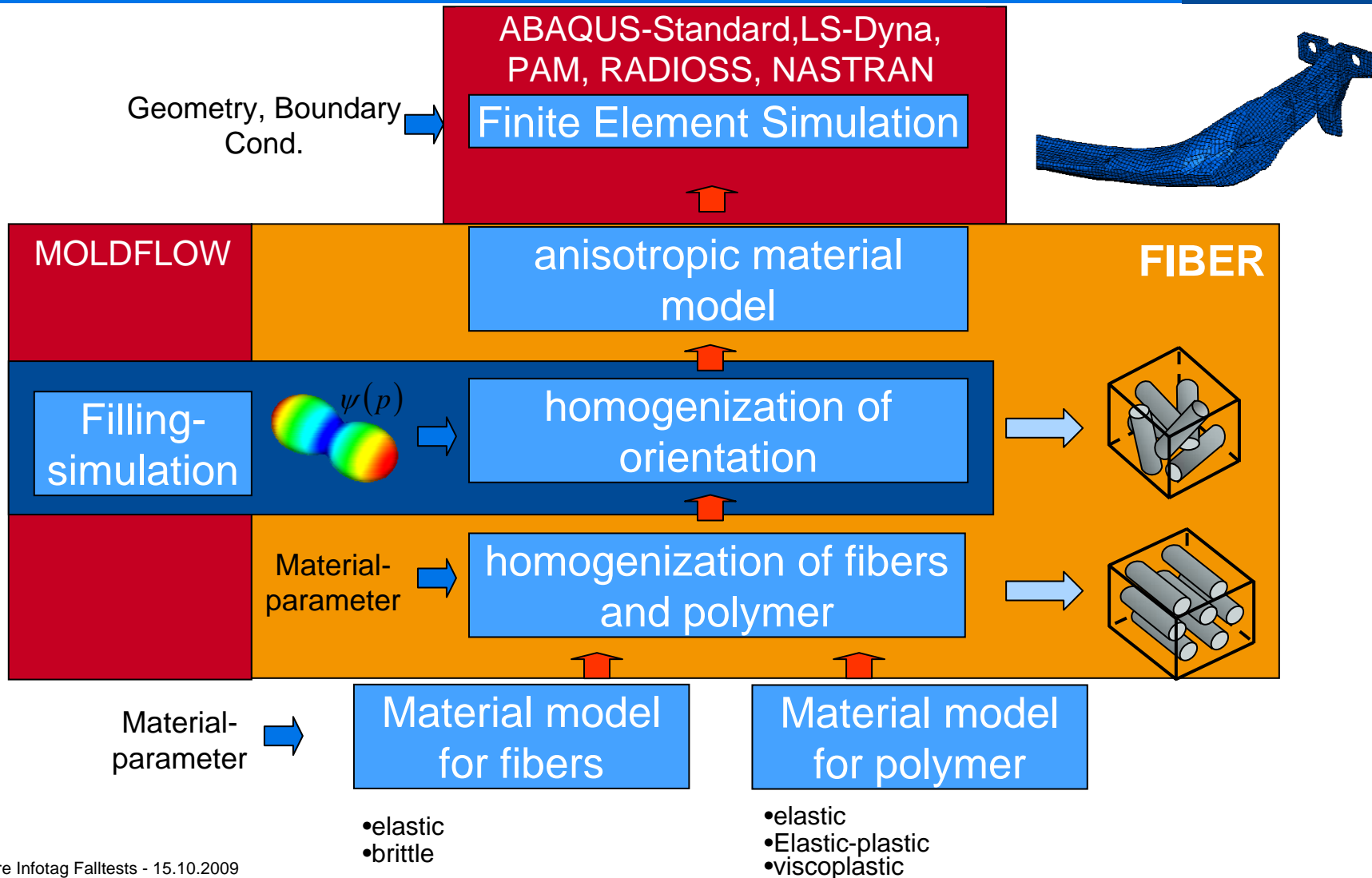


**Young's modulus**



# Integrative Simulation ULTRASIM™

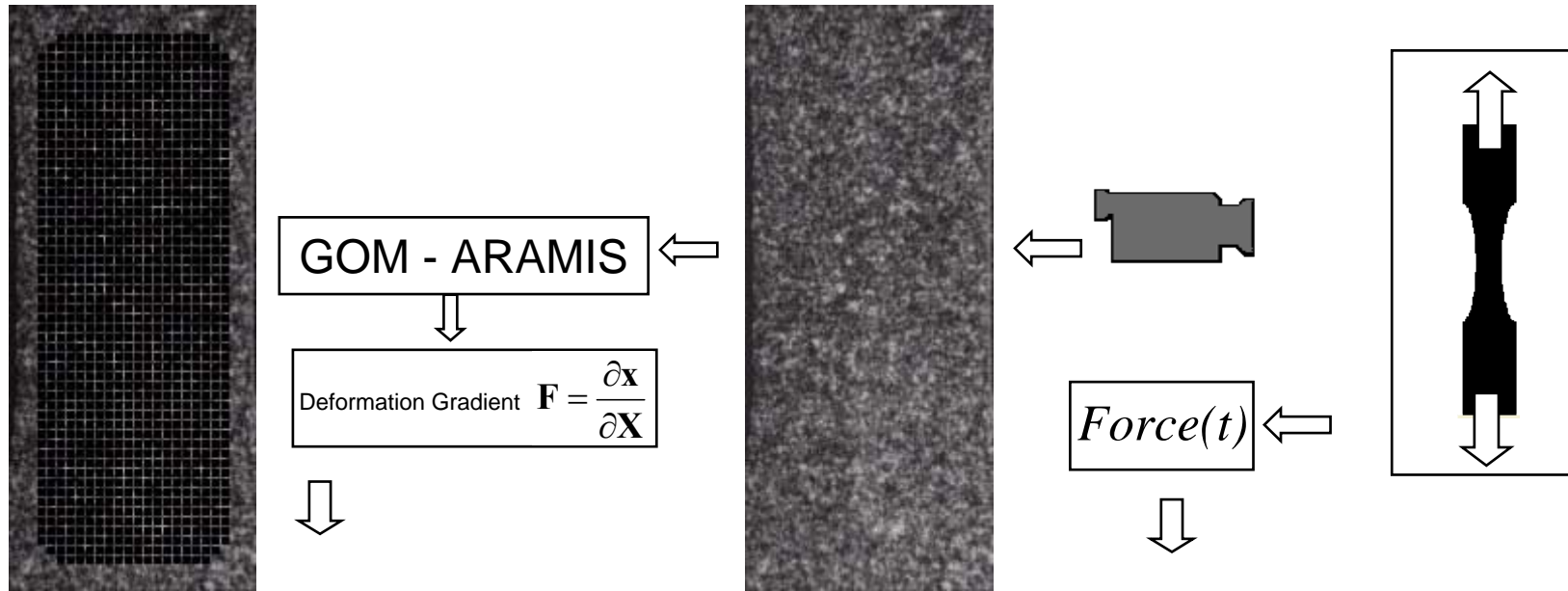
## Data flow structure





# Material Measurements

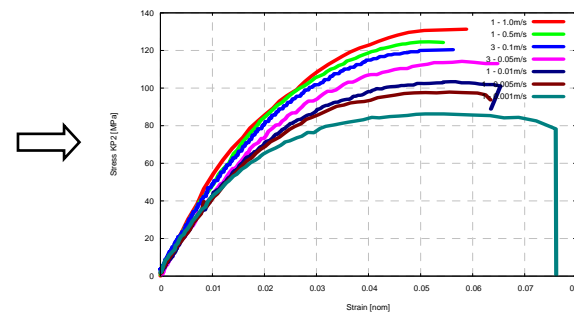
## Data Flow



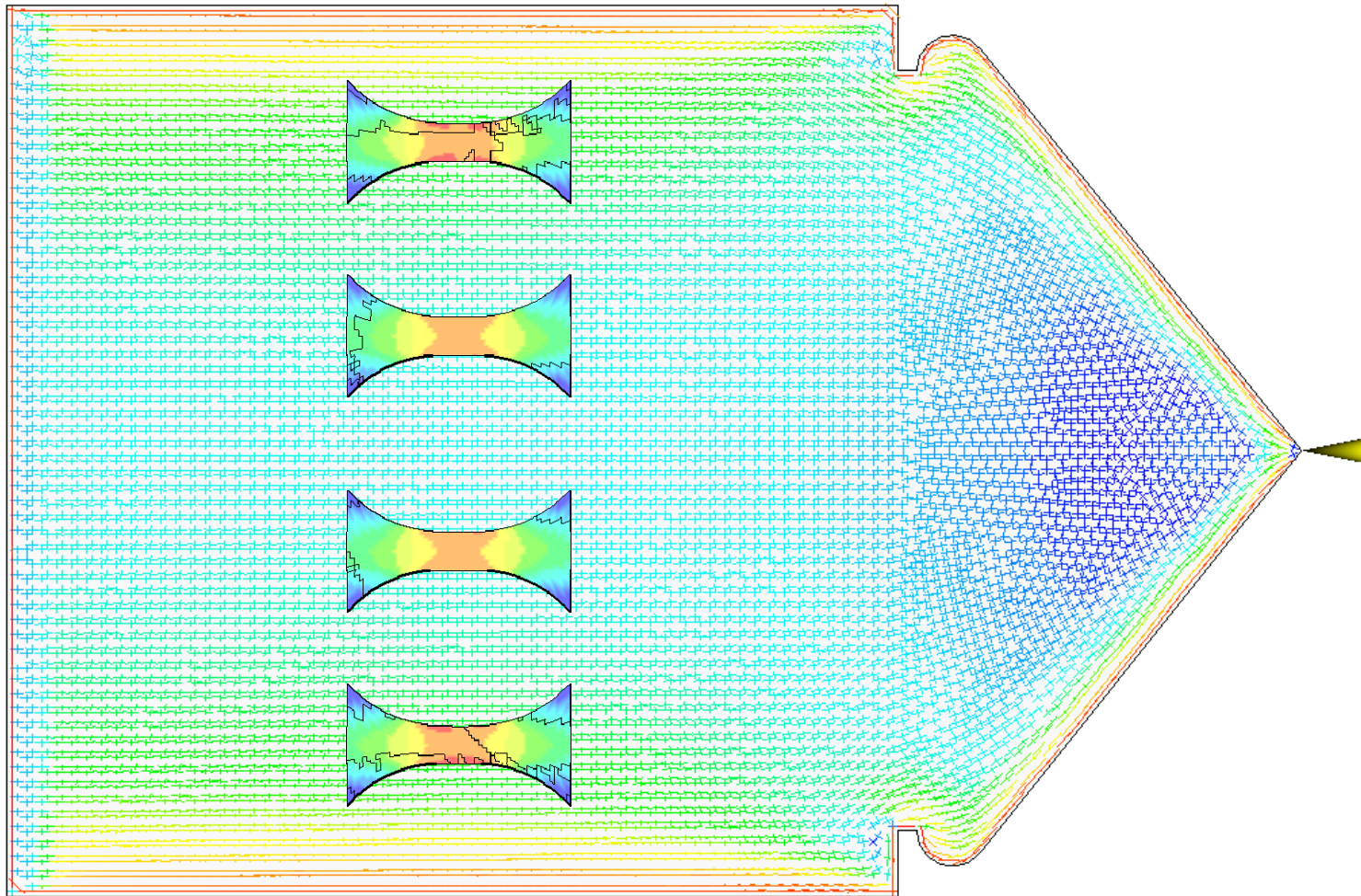
**BASF Software**

$\mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}} \rightarrow$  Strain:  $\mathbf{E} = \frac{1}{2}(\mathbf{F}^T \mathbf{F} - \mathbf{G})$   
 $\mathbf{e} = \frac{1}{2}(\mathbf{g} - \mathbf{F}^{-T} \mathbf{F}^{-1})$

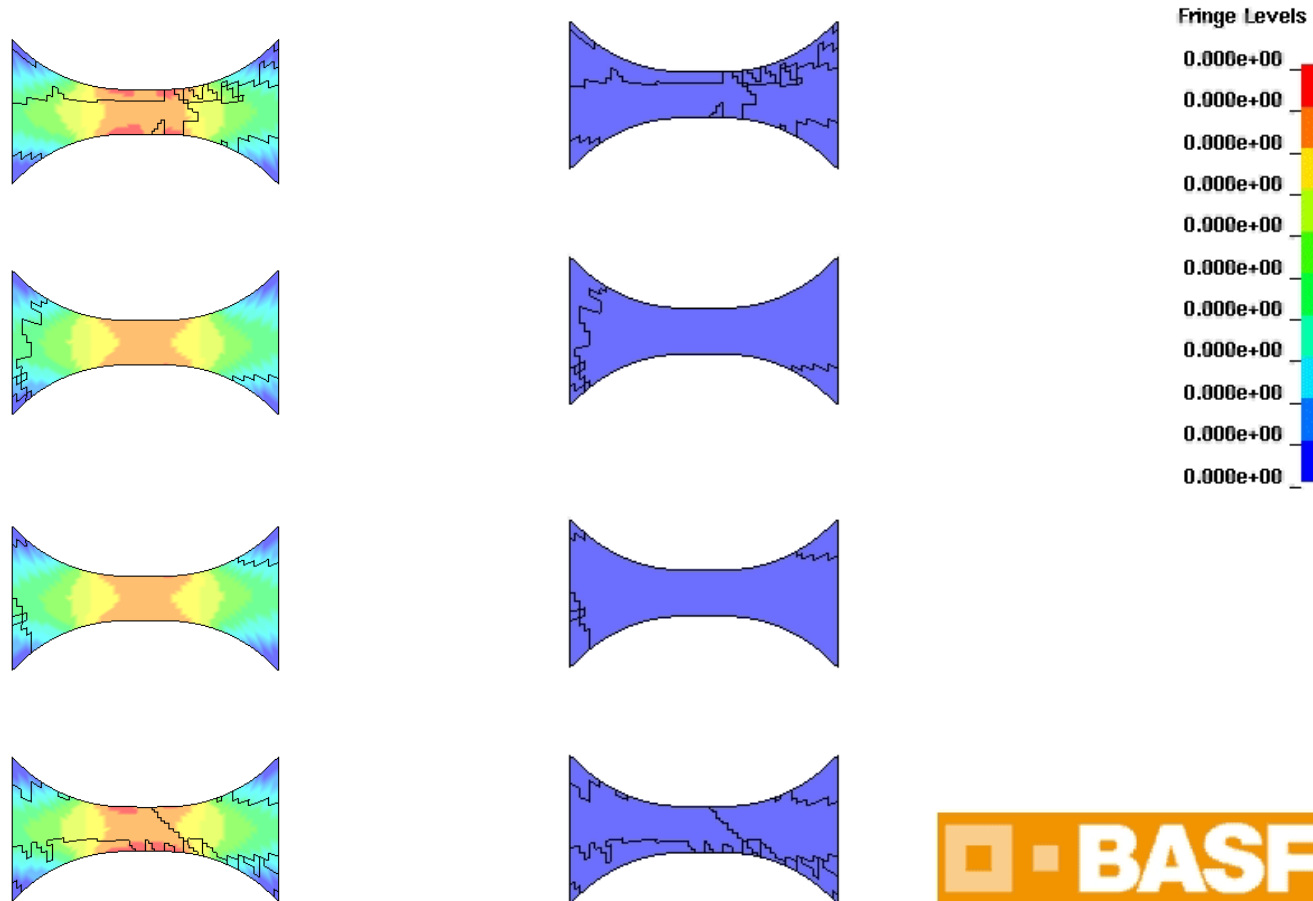
$S^{11} = \frac{Force(t)}{A_0}$  Stress:  $\boldsymbol{\sigma} = \frac{1}{J} \mathbf{F} \mathbf{S} \mathbf{F}^T$



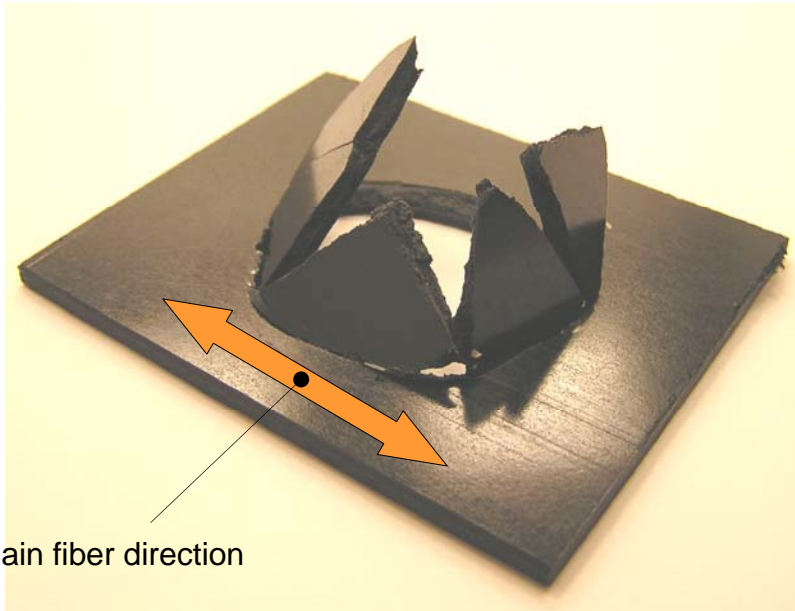
# Average Fiber orientation and Failure variable



# Failure variable



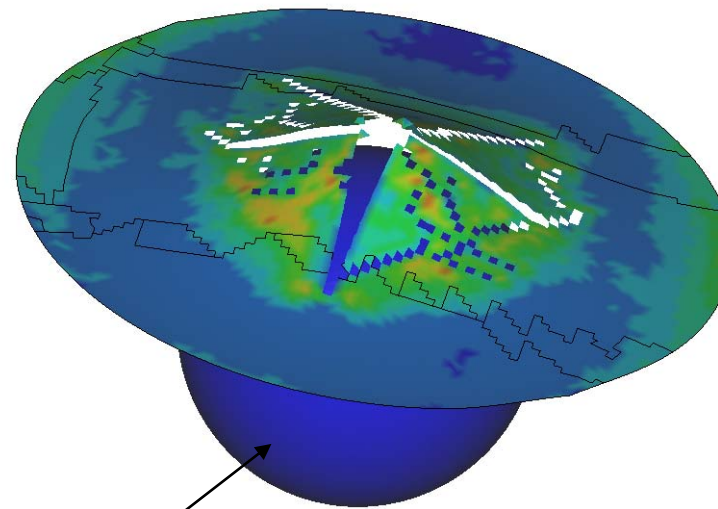
# Penetration Experiment



Main fiber direction

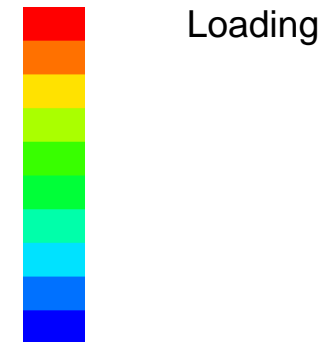
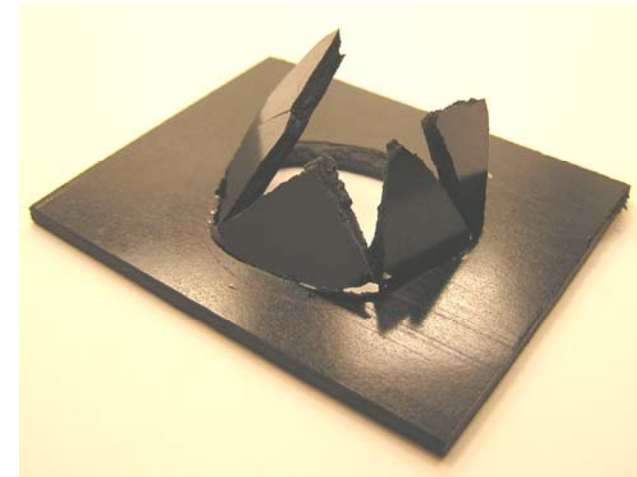
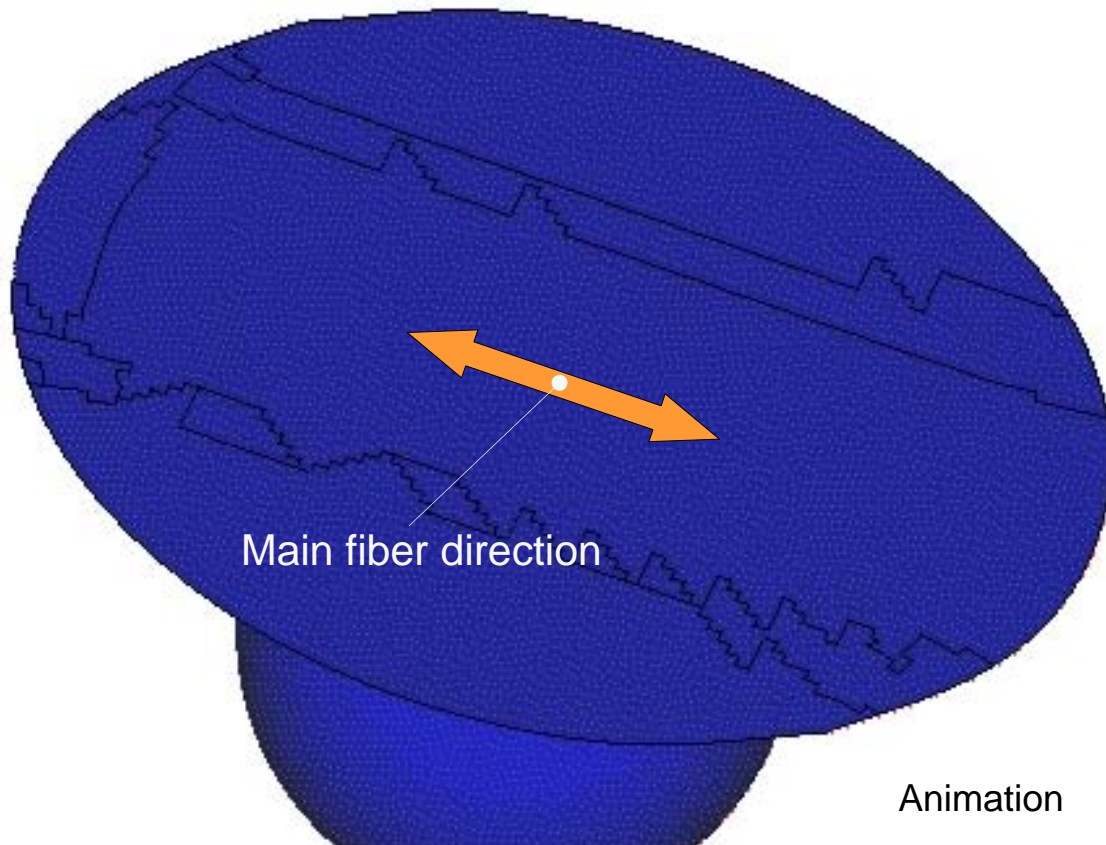
Biaxial Stress

Fixed by axisymmetric die



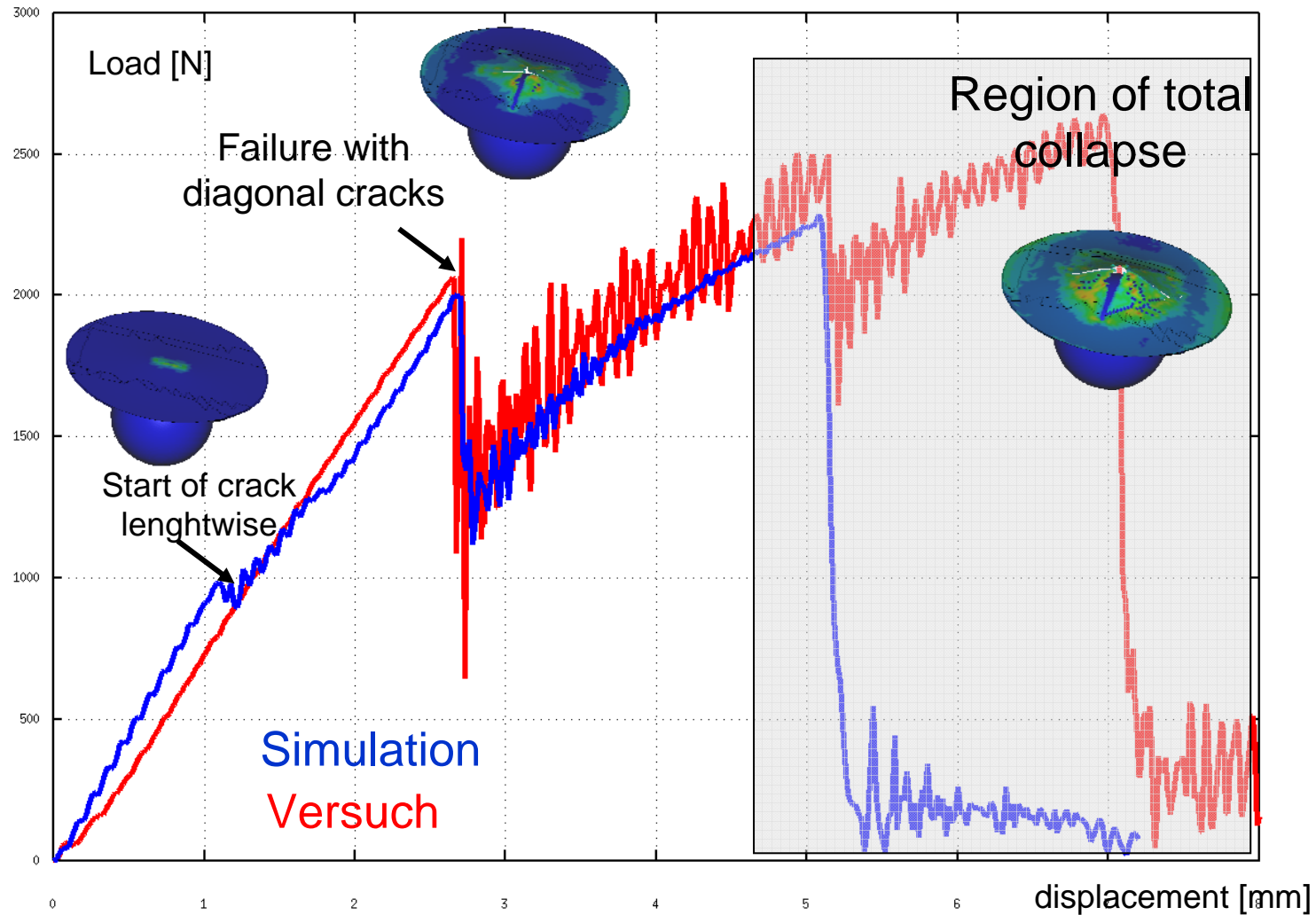
punch

# Simulation of penetration experiment





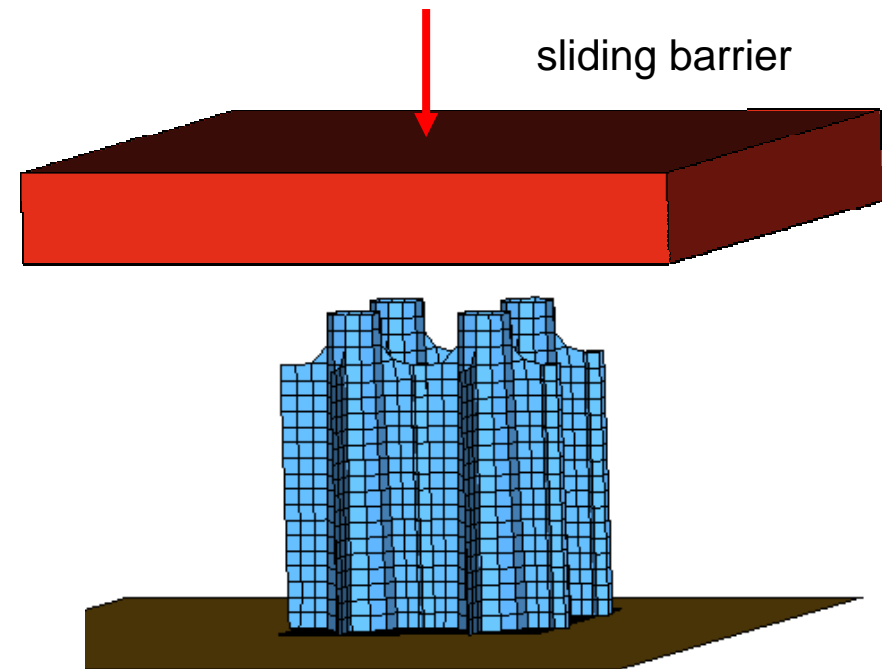
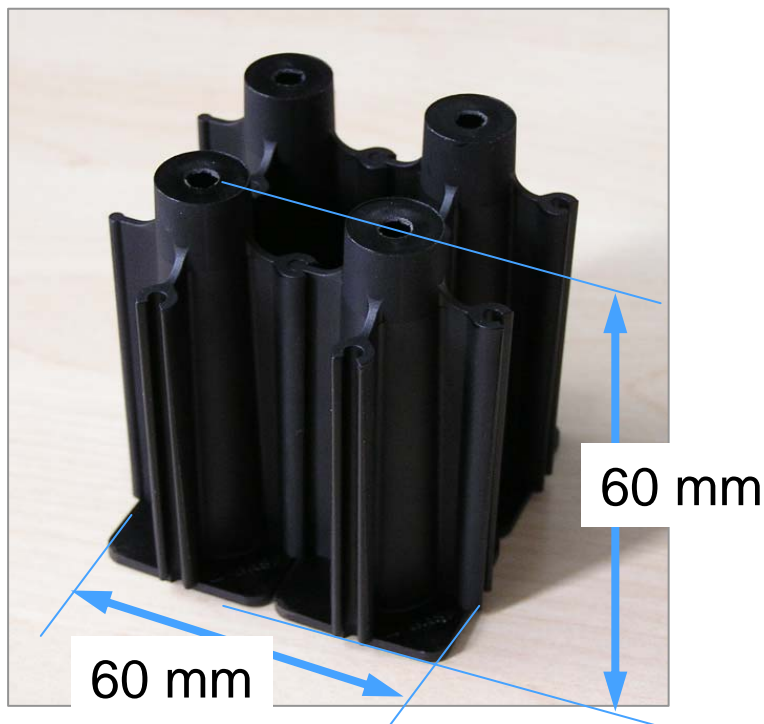
# Simulation of penetration experiment



# Test Specimen for compression load

Specimen is designed for controlled collapse

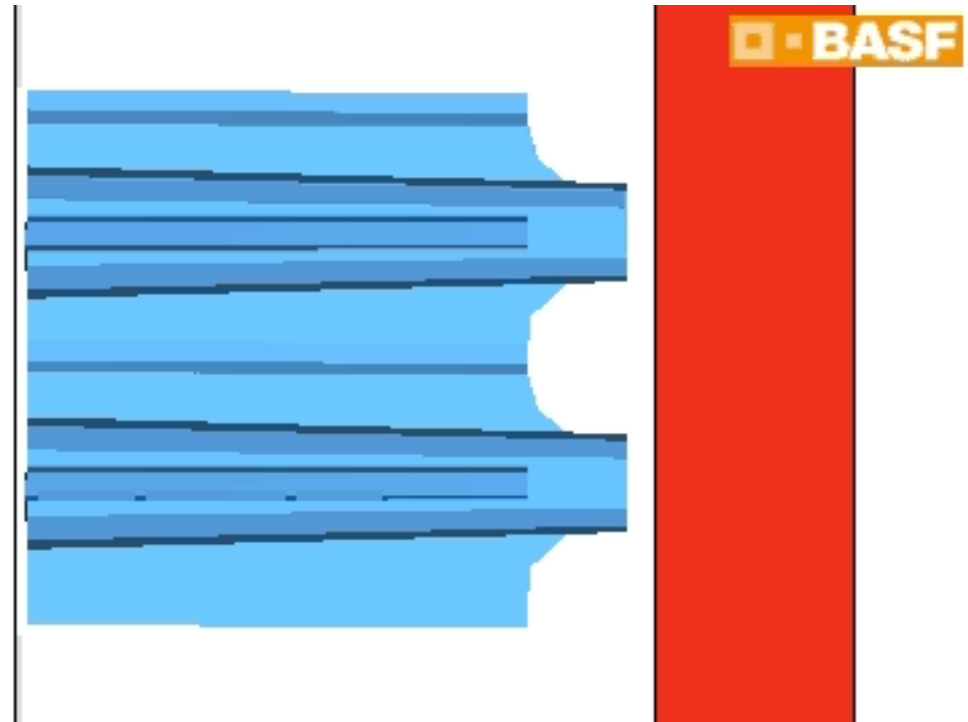
Material: B3WG6 CR (PA6 GF30%)





# Plastic specimen under compression load

## Simulation and Experiment

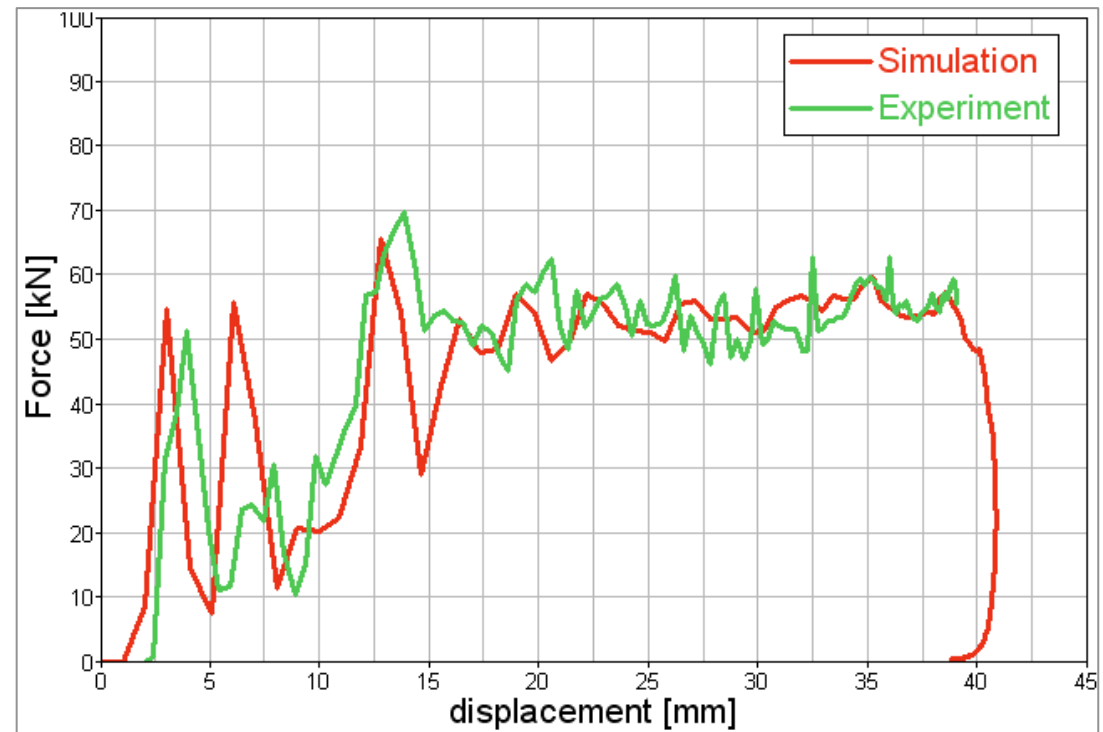


# Test-specimen under compression load

## Simulation and Experiment



60 mm

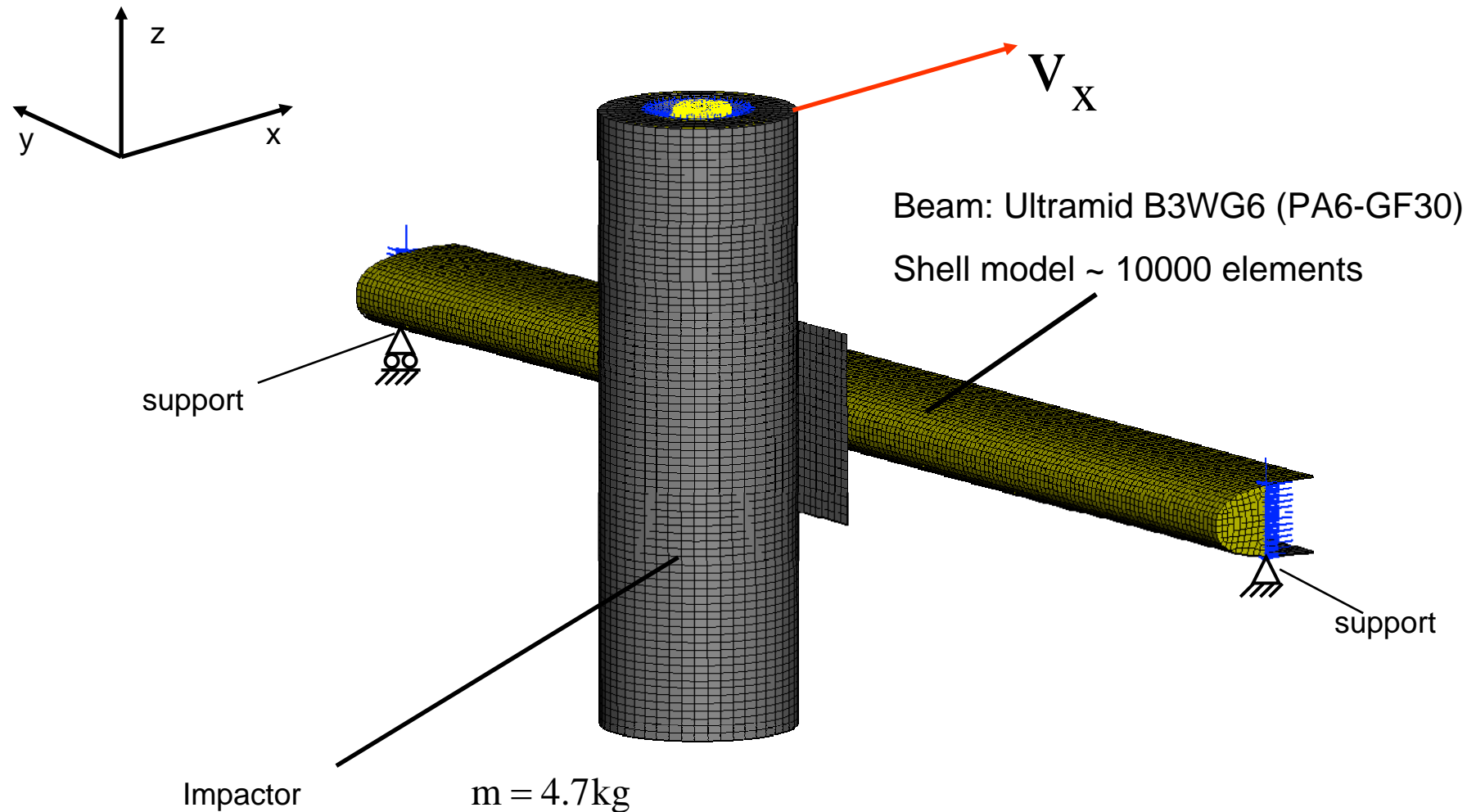


## Illustrated Example

# Importance of Fiber Orientation

Mechanical test set-up

Lower leg shot on supported beam



## Illustrated Example

# Importance of Fiber Orientation

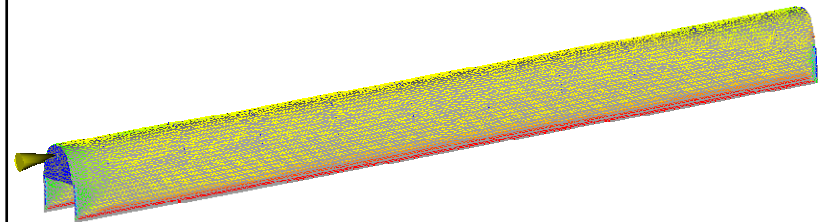
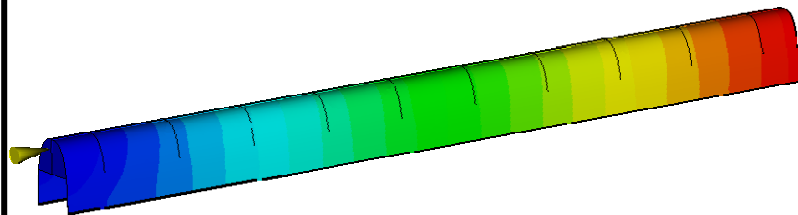
Filling pattern and fiber orientation  
Filling calculation with MOLDFLOW

**BASF**  
The Chemical Company

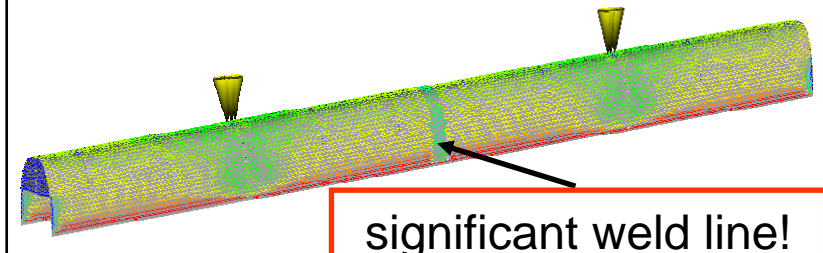
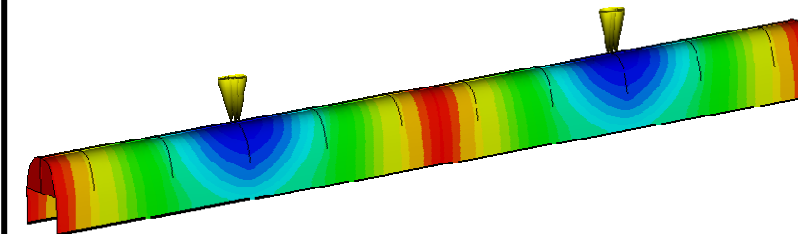
Filling pattern

Fiber orientation

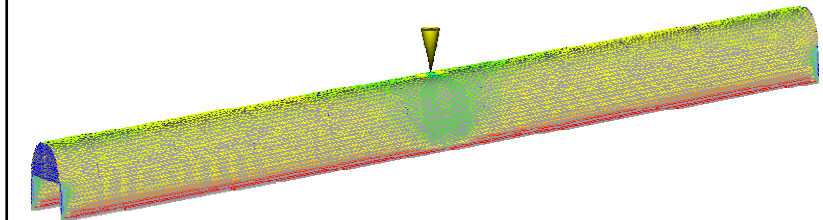
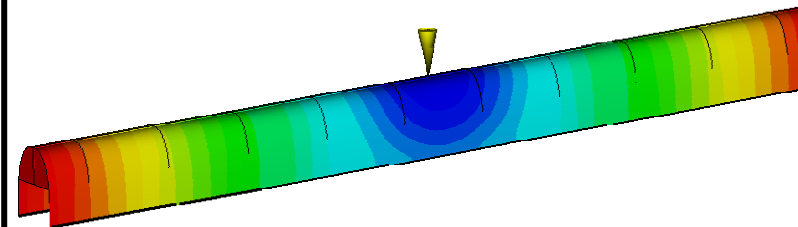
Case A



Case B

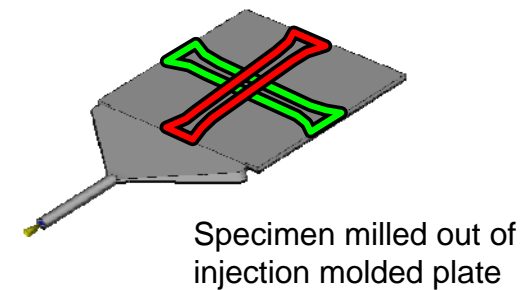
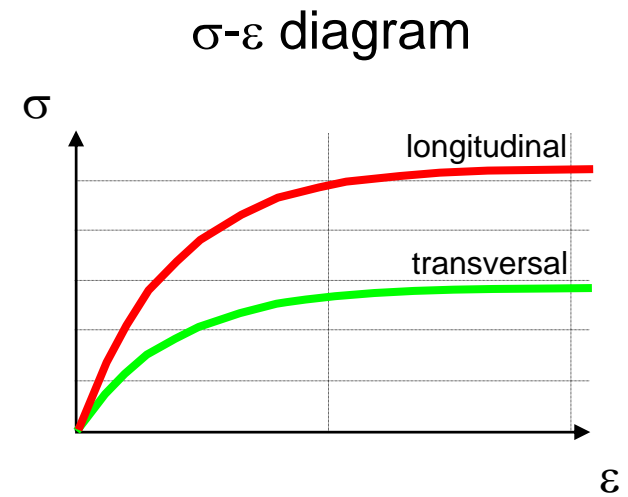
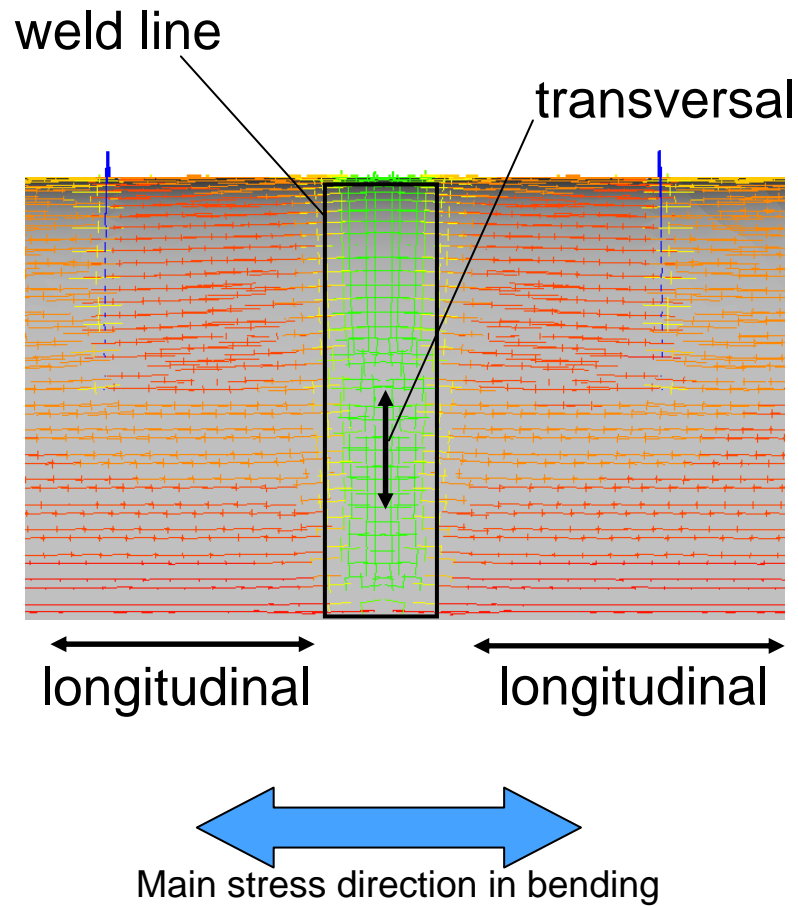


Case C



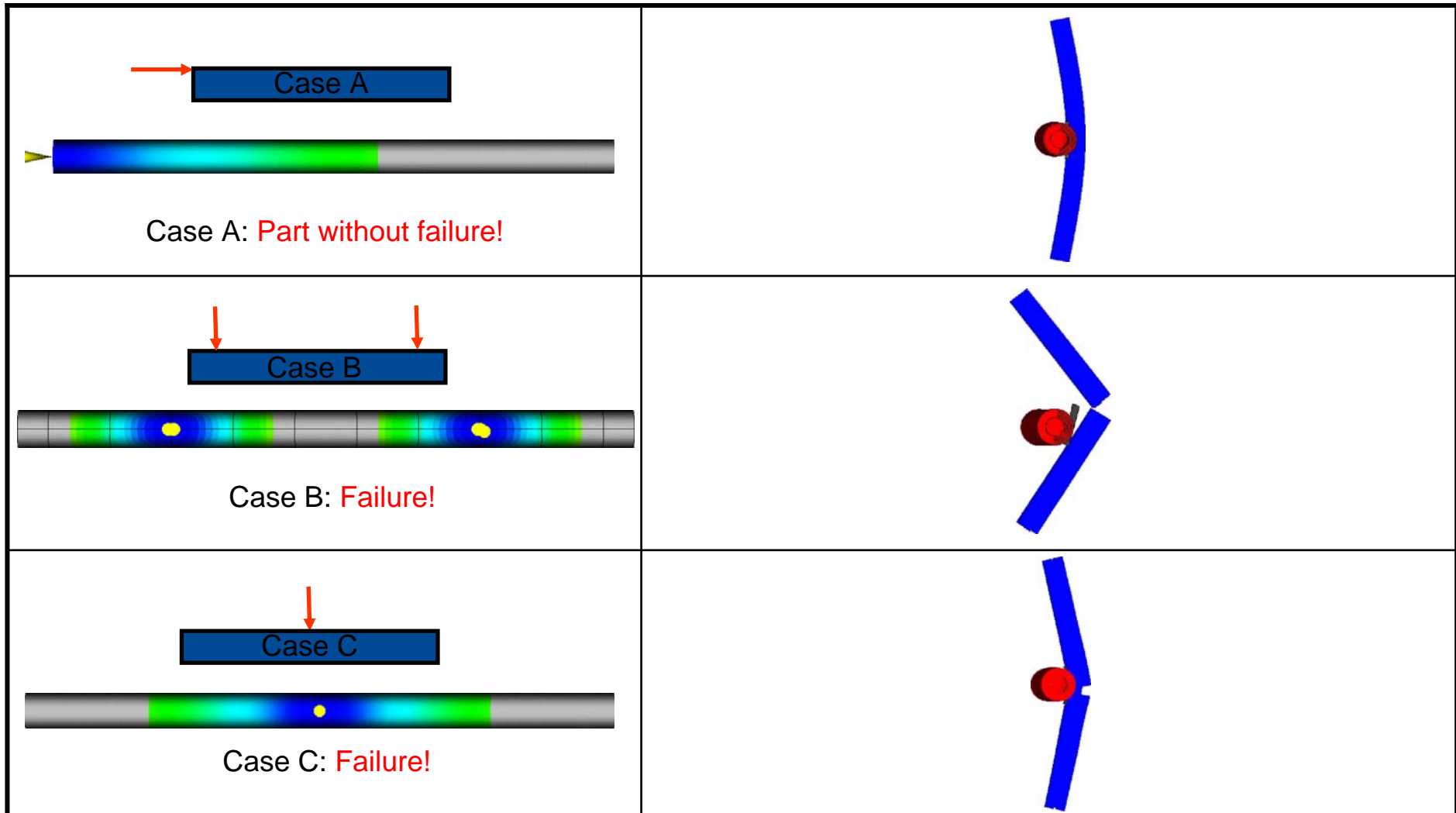
# Detail of fiber orientation in weld line

## Case B



# Illustrated Example Importance of Fiber Orientation

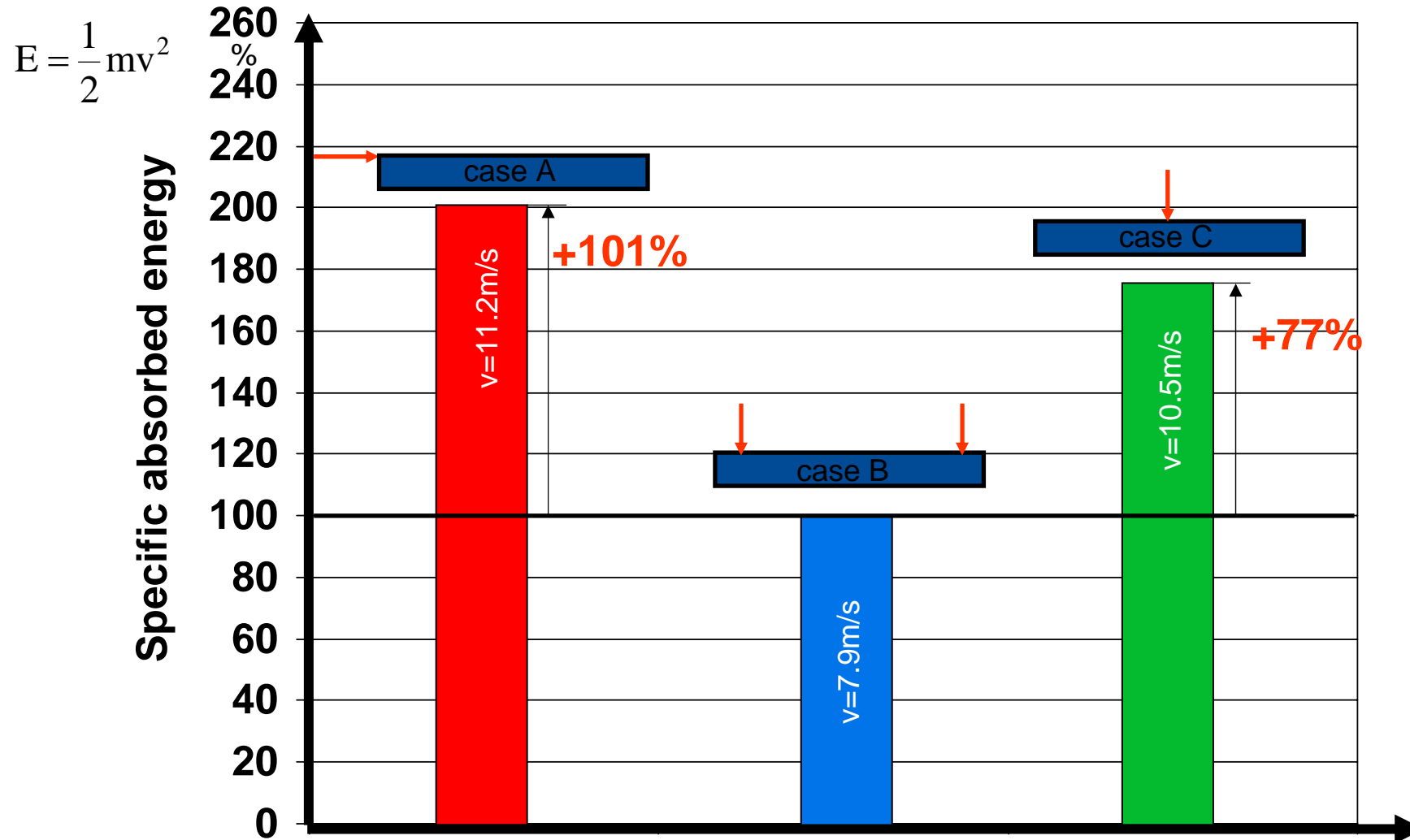
Results with  $v=11.2$  m/s



# Illustrated Example

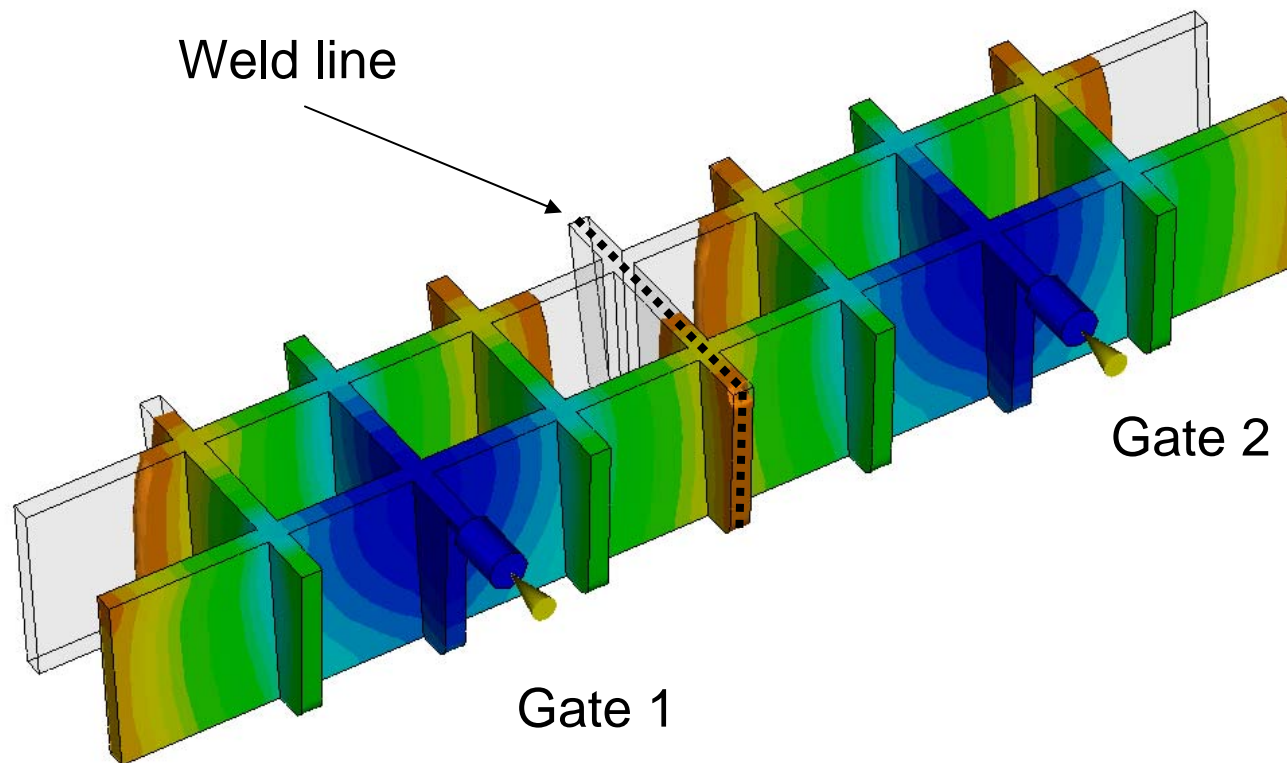
## Importance of Fiber Orientation

Comparison of absorbed energy

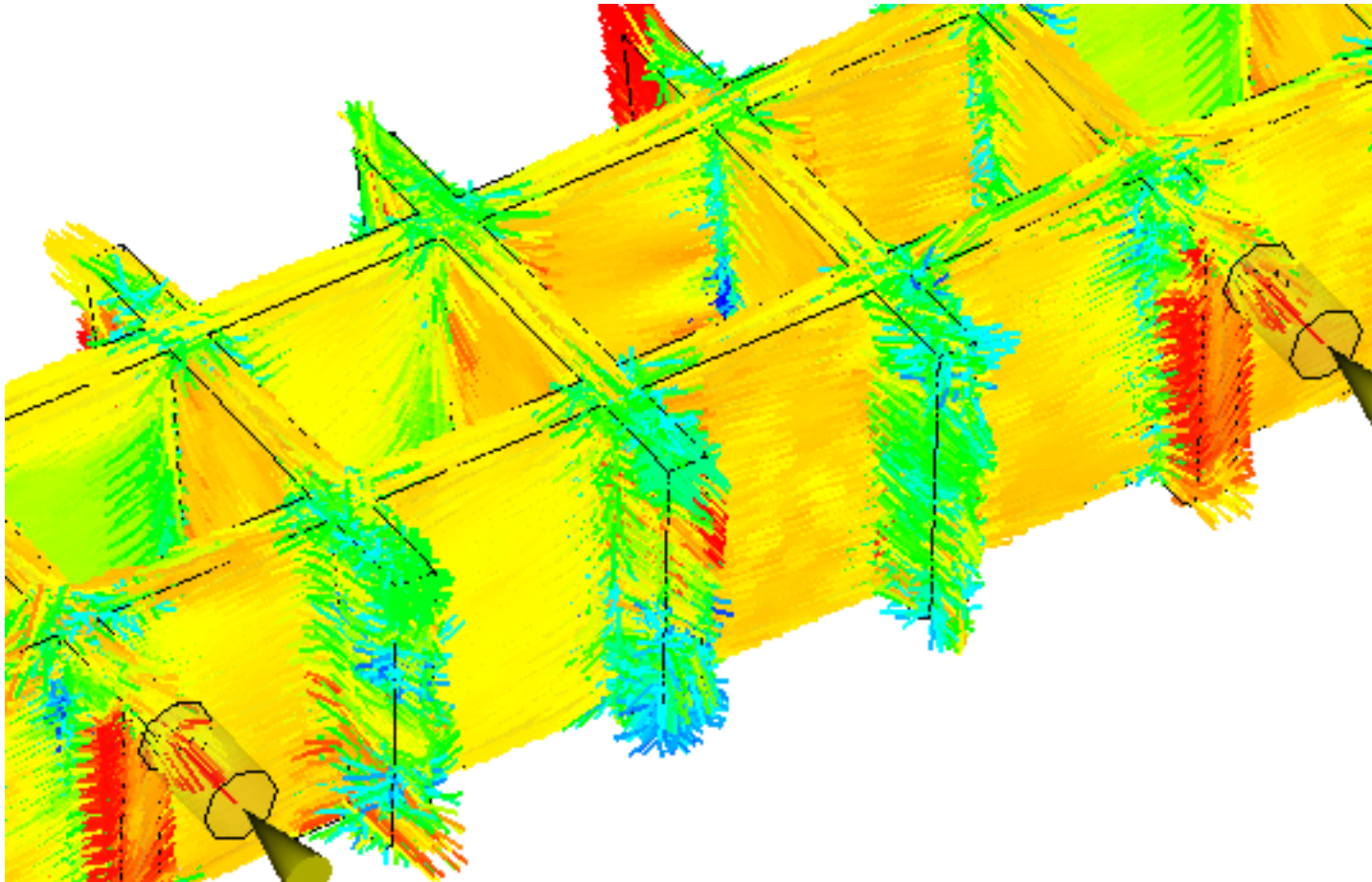




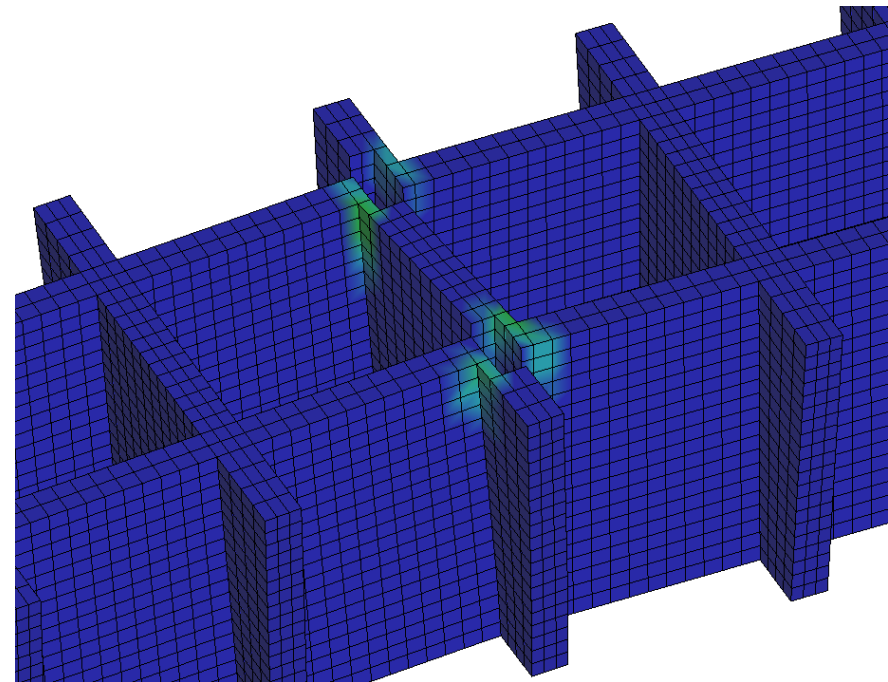
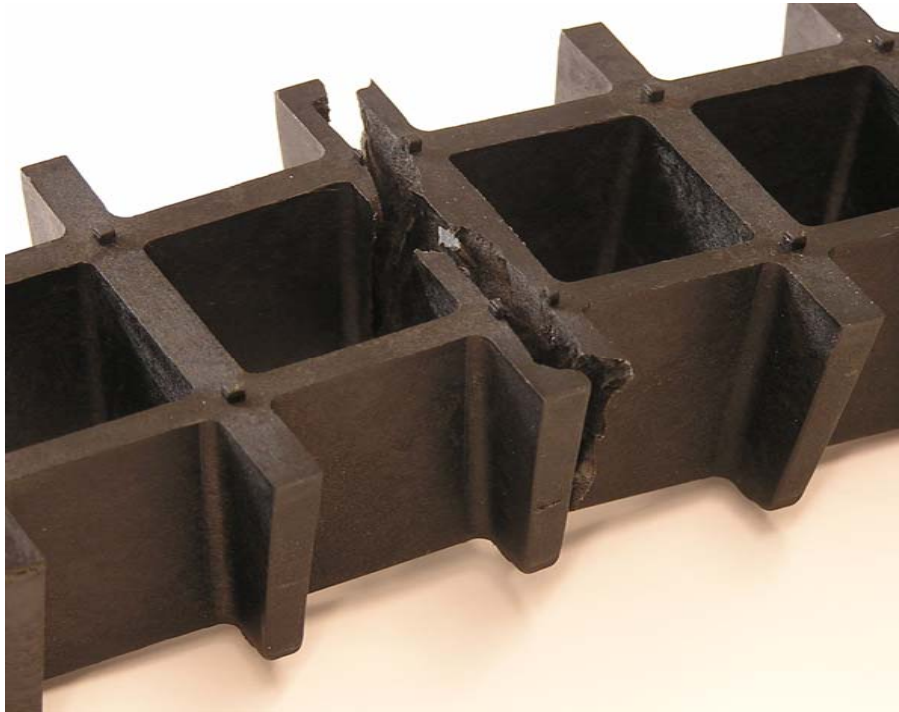
# Filling pattern and weld line



# Fiber orientation



# Failure in weld line - symmetric bending



- Simulation von Falltests stellt neue Herausforderungen
  - Kinematik → Kontakt
  - Abbildung von Verbindungen → Beispiel Schraube
  - Materialverhalten → ULTRASIM
  - Versagen → ULTRASIM
- Materialmodellierung mit BASF ULTRASIM™
- Bindenahteinfluss bei faserverstärkten Kunststoffen
- Beispiele

**Vielen Dank für Ihre Aufmerksamkeit!**

# Einfluss der Materialmodellierung von thermoplastischen Kunststoffen auf Ergebnisse von numerischen Falltests

