



TRR285

Efficient Gradient-Enhancement of Ductile Damage for Implicit Time Integration



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LS-Dyna Forum22 – C2 @Room II**

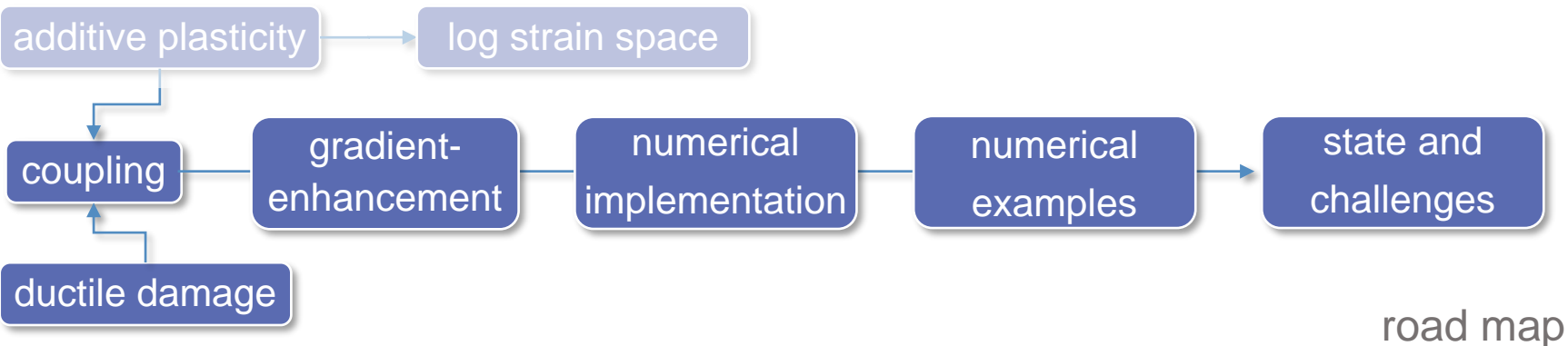
11.10.2022; 16:35-16:55

Material modelling for mechanical joining of sheet metal

-  materials: dual-phase steel HCT590X; aluminium alloy EN AW-6014
-  locally severe plastic deformations (acc. plastic strains > 2)
 - finite plasticity in the logarithmic strain space (“ln-space”)

Miehe et al., 2001/2002;
 JF et al., 2022 (IJSS)
-  modelling of process-induced damage: “damage is not failure”
 - phenomenological ductile continuum damage model

Tekkaya et al., 2020
-  fully coupled plasticity-damage
 - damage localisation
 - regularisation with gradient-enhancement to ensure mesh-independence
 - transfer to LS-Dyna using weakly staggered thermomechanical coupling



road map

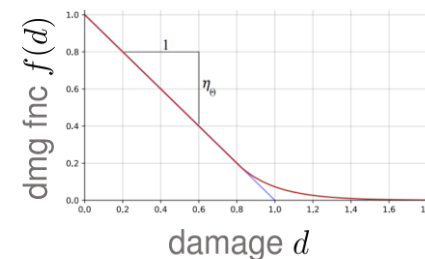
Damage and degradation

damage variable

$$d = [0 \dots \infty)$$

damage function

$$f_i = \begin{cases} 1 - \eta_i d, & \text{if } f_i > 0.01 \\ 0.001 + (0.01 - 0.001) \exp\left(\frac{1 - 0.01 - \eta_i d}{0.01 - 0.001}\right), & \text{else} \end{cases} = [1 \dots 0.001)$$



Ductile damage

ductile damage driven by plasticity: $d^{loc}(H^{p,acc})$
with undamaged acc. plastic strain

$$\dot{H}^{p,acc} = \sqrt{\frac{2}{3}} \dot{\gamma}^{pd} \geq 0$$

nonlinear damage accumulation:

$$d^{loc} = \left[\frac{H^{p,acc} - \varepsilon_{init}^p}{\varepsilon_{fail}^p - \varepsilon_{init}^p} \right]^{n_d}$$

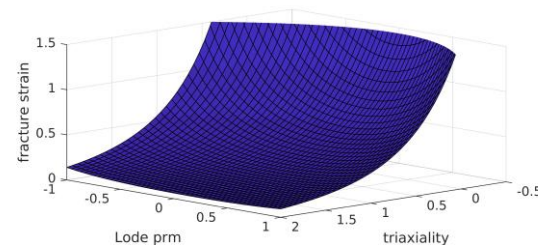
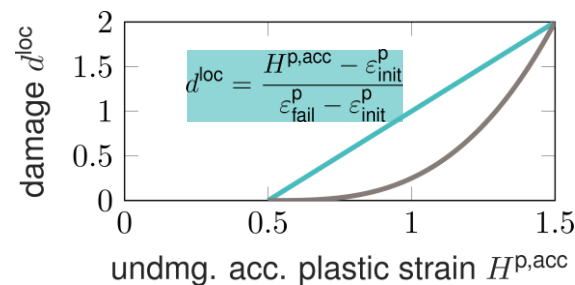
"truly" local damage

$\varepsilon_{(\bullet)}^p$: plastic strain

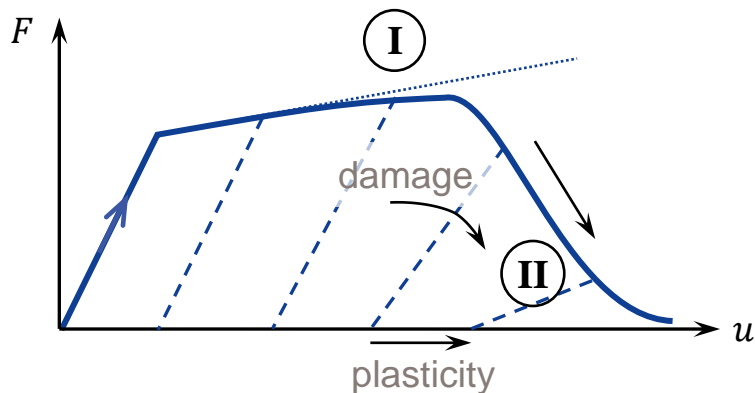
init: damage initiation

fail: failure

n_d : damage exponent

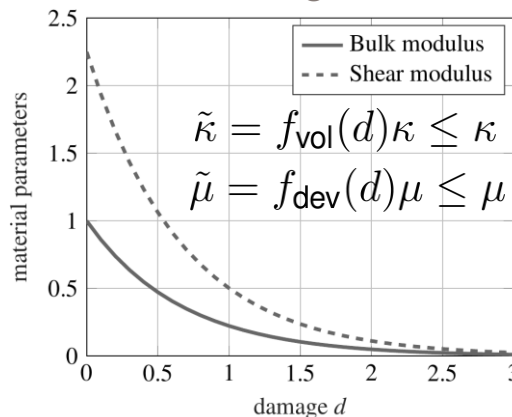


Modified Mohr-Coulomb failure surface



elasticity

material degradation



plasticity ← → damage

concept of effective stress

stress:

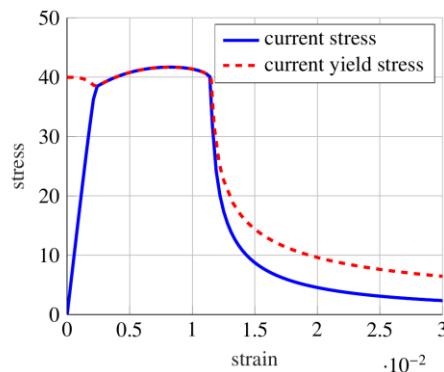
$$\tilde{\sigma}_{flow} = f_p(d)\sigma_{flow} \leq \sigma_{flow}$$

plastic strain tensor:

$$\dot{\mathbf{H}}^{pd} = \dot{\gamma}^{pd} \mathbf{n} = \dot{\mathbf{H}}^p$$

plastic hardening variable:

$$\dot{\alpha} = f_p(d)\dot{\gamma}^{pd}$$



$$\Psi^{plastic} = \Psi^{elastic} + \Psi^{hard}$$

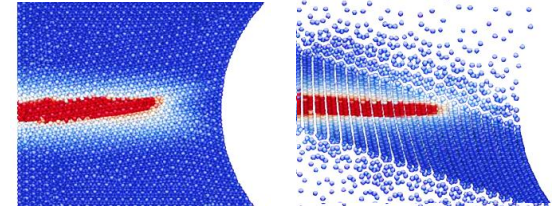
$$\Psi^{locPD} = f_i * \Psi^{elastic} + \Psi^{hard}$$

free energy

Why regularisation?

Local damage models

- mathematically ill-posed
- mesh-dependent (mesh size/orientation/...)



Zhang&Lorentz&Besson, 2018

Why gradient-enhancement?

- more efficient than non-local integral model
- more flexible than viscous regularisation

Nahrnann&Matzenmiller, 2021
Niazi et al., 2013

Gradient-enhancement of free energy

$$\Psi = \Psi^{\text{loc}}(\mathbf{H}, \mathbf{H}^p, \alpha, d) + \Psi^{\text{nloc}}(d, \bar{d})$$

$$\text{with } \Psi^{\text{nloc}} = c/2 \|\nabla_{\mathbf{x}} \bar{d}\|^2 + \beta/2 [\bar{d} - d]^2$$

\bar{d} : non-local damage variable
 d : local damage variable
 c : regularisation parameter
 β : penalty parameter

Dimitrijevic&Hackl 2011;
Kiefer et al. 2018;
Langenfeld&Mosler 2019;
Brepols et al. 2020

Partial Differential Equations (PDEs)

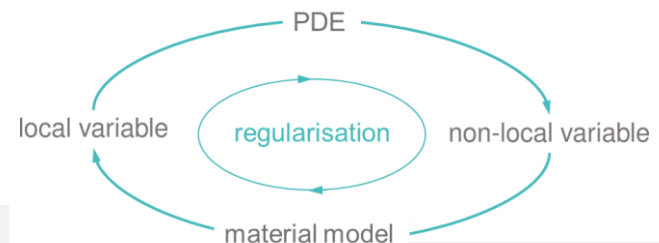
balance of linear momentum:

$$\nabla_{\mathbf{x}} \cdot [\mathbf{F} \cdot \mathbf{S}] = \mathbf{0}$$

regularisation

$$\nabla_{\mathbf{x}} \cdot [c \nabla_{\mathbf{x}} \bar{d}] - \beta [\bar{d} - d] = 0$$

Seupel et al., 2018
Ostwald et al., 2019

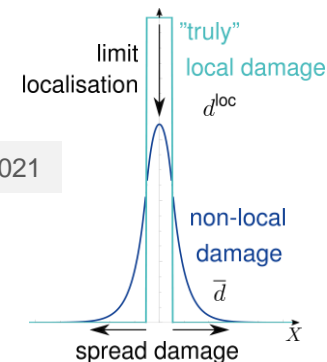


Friedlein et al. (PAMM21)

What variable to regularise? Many more options. Interested? Just ask.

- weakly staggered thermomechanical coupling
- delayed non-local variable \bar{d}_n
- explicit time integration → directly applicable
- implicit time integration → step size dependency
- mimic change of non-local variable $\bar{d}_{n+1} = \bar{d}_n / d_n^{\text{loc}} \cdot d_{n+1}^{\text{loc}}$

Nahrnann&Matzenmiller, 2021



Friedlein et al., 2021 (PAMM)

umat4x

UMAT with ITERM=1

$d_{n+1}^{\text{loc}} \leftarrow$ local damage model

$K_{\text{NL}} = \bar{d}_n / d_n^{\text{loc}}$

$\bar{d}_{n+1} = K_{\text{NL}} \cdot d_{n+1}^{\text{loc}}$

$d_{n+1} = \max(\underbrace{\max(d_n, \bar{d}_n)}_{d \geq 0}, \bar{d}_{n+1})$
spread

$f(d_{n+1}) \rightarrow$ material behaviour

Non-local integral model:
Tvergaard&Needleman,
1995;
Andrade et al., 2011

hsv(d_{n+1}^{loc})

thumat1x

thermal solver
with source term
and IHVE=1

$$l^2 \Delta_X \bar{d}_n - [\bar{d}_n - d_n^{\text{loc}}] = 0$$

hsvm(d_n^{loc})

temp(\bar{d}_n)

IHVE=1: map mechanical history

thermal step ideally done after/before each mechanical step

PDE for regularisation

$$l^2 \Delta_X \bar{d}_n - [\bar{d}_n - d_n^{\text{loc}}] = 0$$

linear \rightarrow single Newton-Raphson iteration $\bar{d}_n^h = M^{-1} \cdot R_d$

\rightarrow gradient-enhancement by post-processing scheme

umat4x

UMAT

$d_{n+1}^{\text{loc}} \leftarrow$ local damage model

$$K_{\text{NL}} = \bar{d}_n / d_n^{\text{loc}}$$

$$\bar{d}_{n+1} = K_{\text{NL}} \cdot d_{n+1}^{\text{loc}}$$

$$d_{n+1} = \max(\underbrace{\max(d_n, \bar{d}_n)}_{d \geq 0 \text{ spread}}, \bar{d}_{n+1})$$

$f(d_{n+1}) \rightarrow$ material behaviour

$hsv(d_{n+1}^{\text{loc}})$

post-processing

least square
minimisation

$$\bar{d}_n^h = M^{-1} \cdot R_d$$

implicit/explicit

$hsv(\bar{d}_n)$

- nonlinear damage evolution using midpoint rule
- quadratic accuracy
- suitable for implicit time integration with larger steps
- exact for damage exponent $n_d = 2$ with constant damage parameters

$$\Delta d^{loc} = \frac{n_d}{[\varepsilon_{fail}^p - \varepsilon_{init}^p]^{n_d}} [H_n^{p,acc} + 0.5\Delta H^{p,acc} - \varepsilon_{init}^p]^{n_d-1} \Delta H^{p,acc}$$

with $H^{p,acc}$: undmg. acc. plastic strain

ε_{init}^p : plastic strain at damage initiation

ε_{fail}^p : plastic strain at failure

n_d : damage exponent, e. g. =2

Implementation

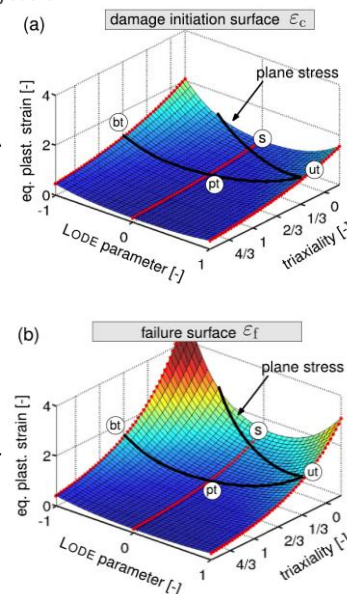
tensor-based → tensor toolbox for Fortran (ttb)

modular implementation

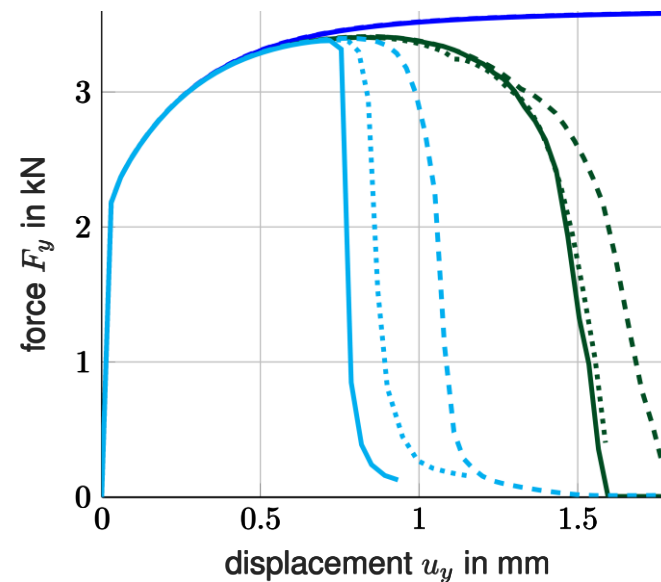
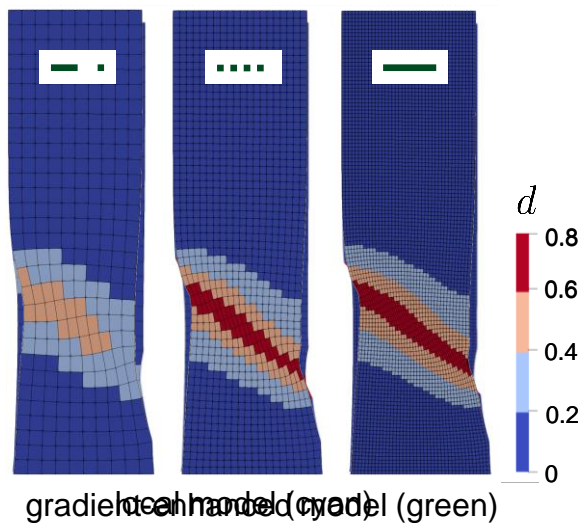
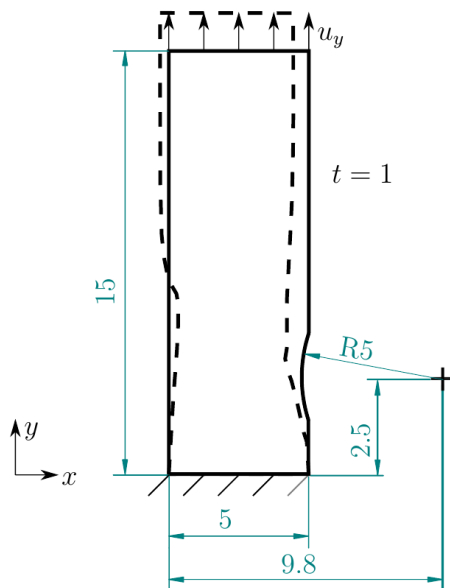
→ GitHub-user: jfriedlein



<https://adtzlr.github.io/ttb/>



Nahrnann&Matzenmiller, 2021



Seupel et al., 2018

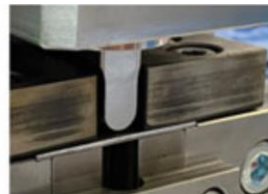
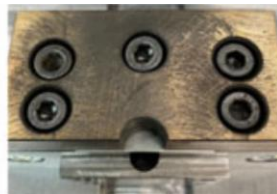
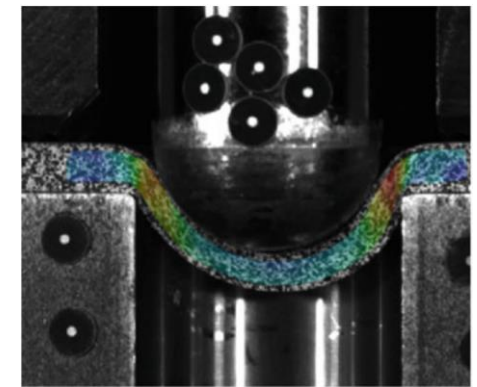
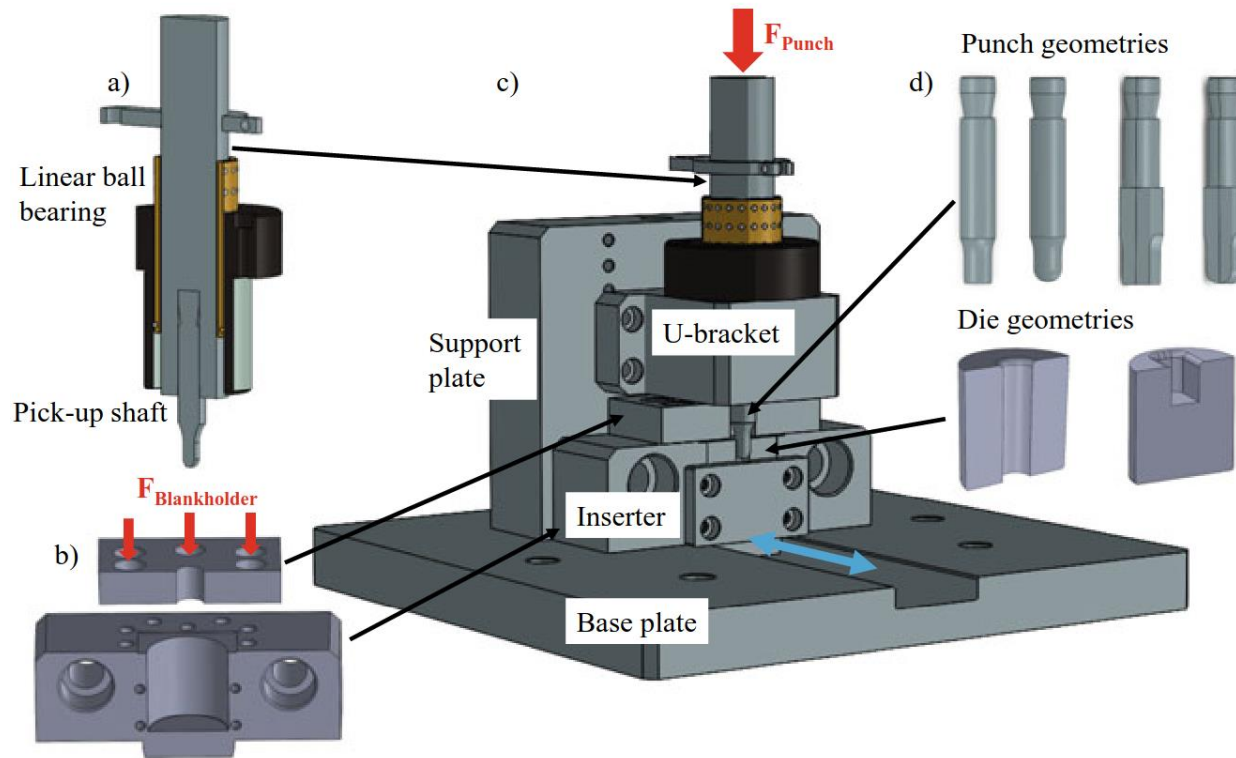
gradient-damage

l/mm	1
pure plasticity	
steel HCT590X	Friedlein et al., 2021 (IDDRG21)
(identified from tensile tests)	

$$d^{\text{loc}} = \left[\frac{H^{\text{p,acc}} - 0.01}{0.4 - 0.01} \right]^2$$



comparison of local plasticity-damage and plasticity – gradient-damage on plane strain example



t



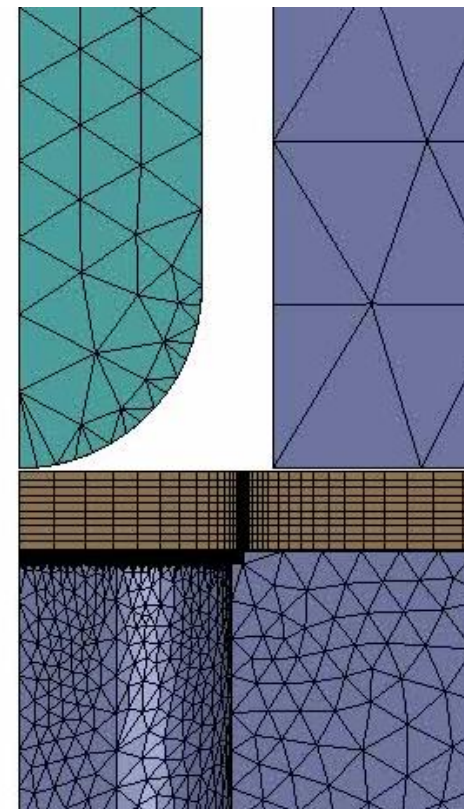
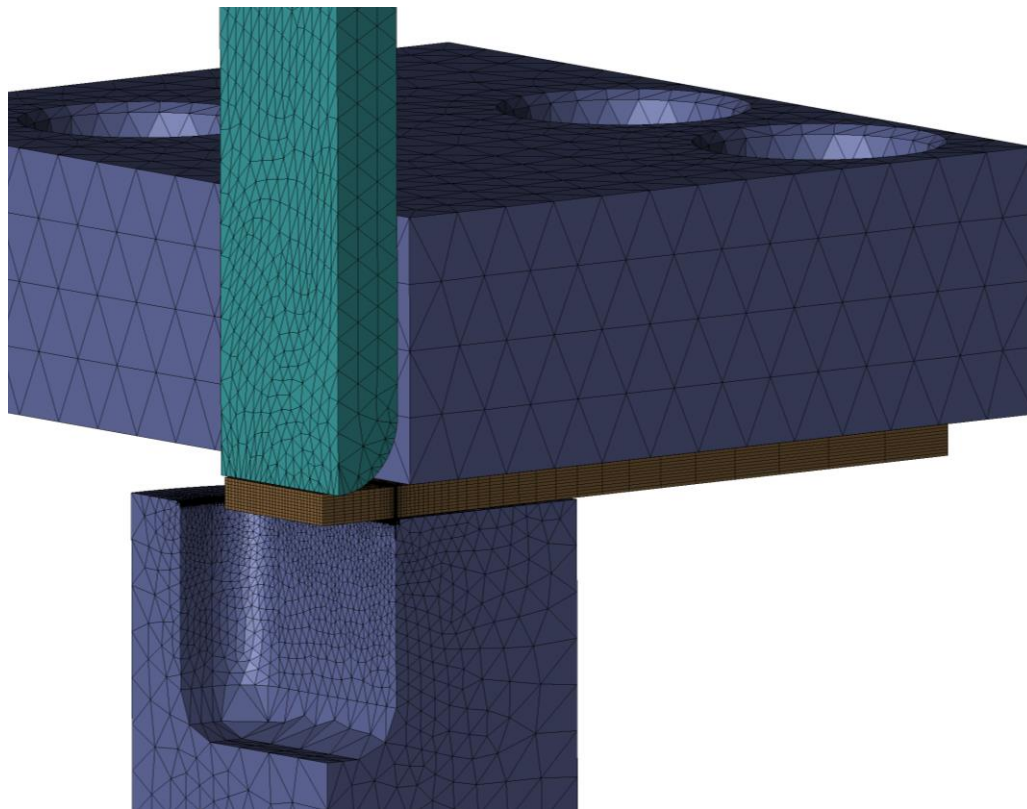
t + 0.69 s



t + 1.18 s

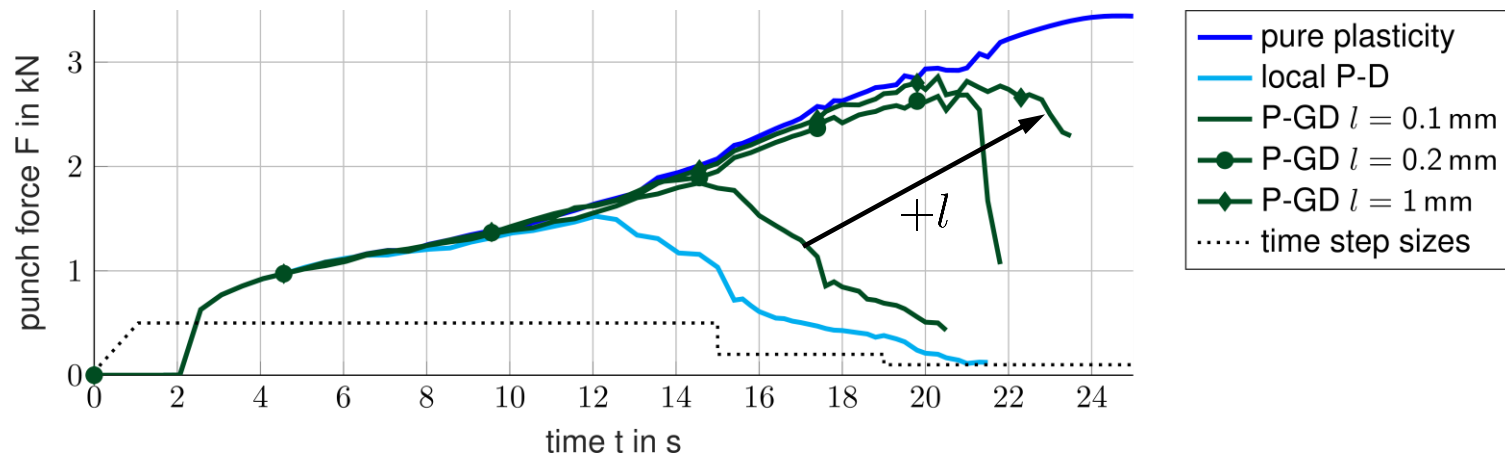
Böhnke et al. 2022 (NUMISHEET22)

experimental setup of the modified punch test



aluminium EN AW-6014 T4; sheet thickness 2 mm

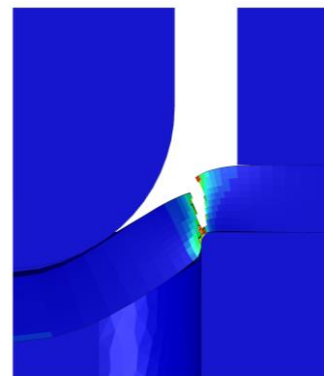
numerical setup of the modified punch test with a prismatic round punch



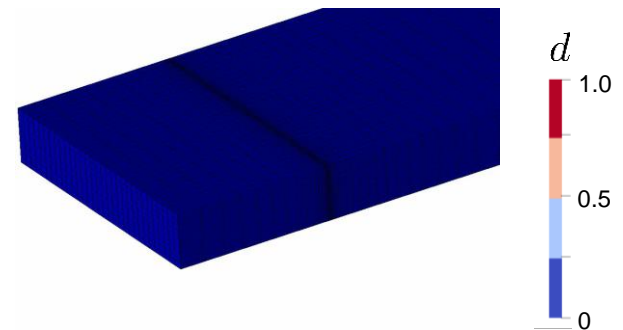
pure plasticity



local P-D



plasticity – gradient-damage $l = 0.1$ mm



numerical results for the modified punch test with a prismatic round punch

Solution strategy

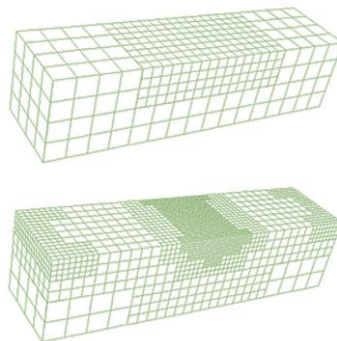
- ▀ monolithic
 - ▀ fully coupled
 - ▀ accurate
 - ▀ unlimited time steps
 - ▀ unsym. stiffness
 - ▀ usu. need for UEL

Kiefer et al. 2018
Brepols et al. 2020

- ▀ weakly staggered
 - ▀ approximate
 - ▀ limited time steps
 - ▀ efficient
 - ▀ flexible
 - ▀ existing solvers
 - ▀ existing ELFORMs
- possibility for post-processing scheme freeing thermal solver

Mesh

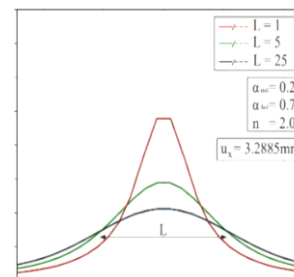
- ▀ regularisation requires fine mesh
- ▀ calls for mesh adaptivity
- ▀ regularisation copes well with changing mesh size
- ▀ gradient-enhancement can improve damage history transfer by inverse mapping



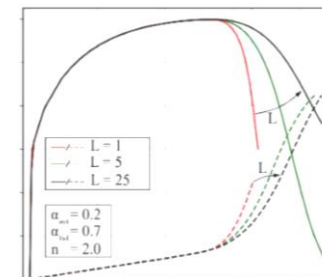
Parameter identification

- ▀ internal length
 - ▀ how to separate effects?
- ▀ challenging couplings
 - ▀ damage affects plasticity
 - ▀ damage affects stress state
 - ▀ gradient-damage affects local damage evolution
- ▀ how to use existing strategies without inverse FEM?
- ▀ regularisation of alternative variables

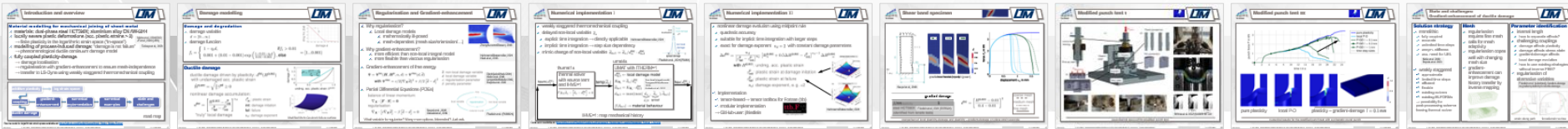
Friedlein et al. (submitted), Gradient-damage vs gradient-plasticity for ductile damage.



strain along path



force&strain vs time



Efficient Gradient-Enhancement of Ductile Damage for Implicit Time Integration

Thank you for your attention!

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